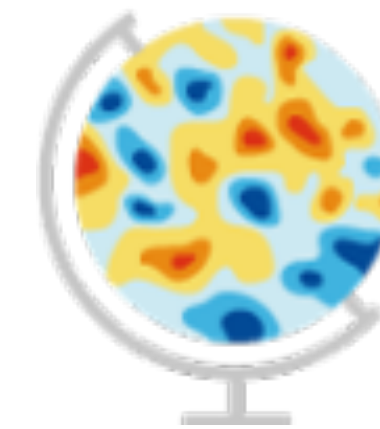


BAYESIAN END-TO-END CMB ANALYSIS FROM LFI TO HFI

Artem Basyrov, PhD student
Institute of Theoretical Astrophysics, University of Oslo

COLLABORATION

- BeyondPlanck
- Cosmoglobe
- LiteBIRD

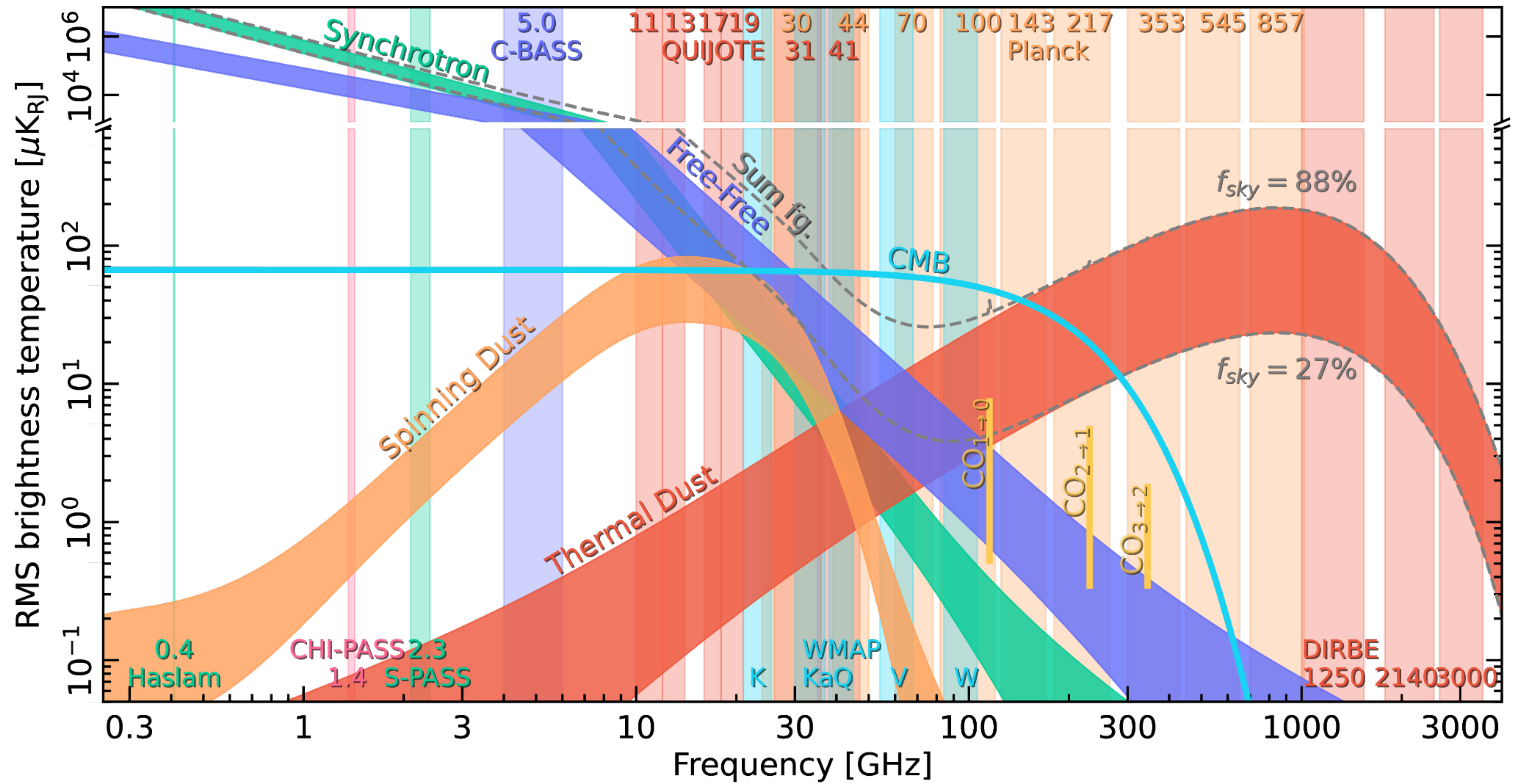


Cosmoglobe



IDEA

- Joint analysis of several data sets together to avoid ‘blind spots’ (scanning strategies) and degeneracies (component separation)
- Integrated approach from the properties of the instrument to the sky model (and from the sky model to the instrument uncertainties)
- More technically: creating a modular algorithm suitable to be used for any future experiments
- More technically: a hands free pipeline from the TOD level to the maps and cosmological parameters without preprocessing and human intervention in-between



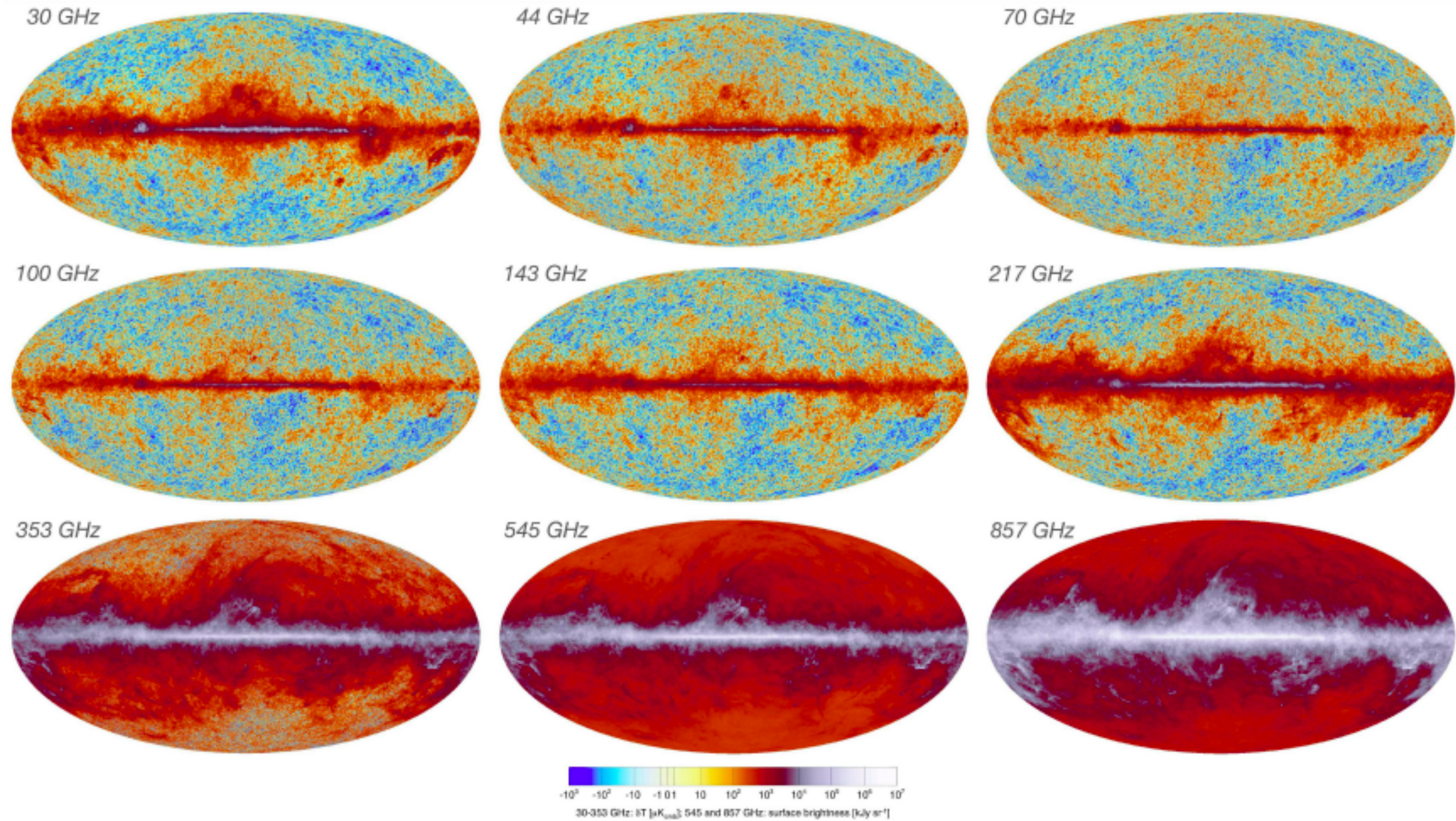
THE SKY MODEL

Different experiments augment each other

THE SKY MODEL*

$$\begin{aligned}
 s = & a_{\text{CMB}} \frac{x^2 e^x}{(e^x - 1)^2} & x = h\nu/kT_0 \\
 & + a_s \left(\frac{\nu}{\nu_{0,s}} \right)^{\beta_s} \\
 & + a_{\text{ff}} \left(\frac{\nu}{\nu_{0,\text{ff}}} \right)^{-2} \frac{g_{\text{ff}}(\nu; T_e)}{g_{\text{ff}}(\nu_{0,\text{ff}}; T_e)} \\
 & + a_{\text{ame}} \left(\frac{\nu}{\nu_{0,\text{ame}}} \right)^{-2} \frac{f_{\text{ame}}(\nu \cdot \frac{30\text{GHz}}{\nu_p})}{f_{\text{ame}}(\nu_{0,\text{ame}} \cdot \frac{30\text{GHz}}{\nu_p})} \\
 & + a_d \left(\frac{\nu}{\nu_{0,d}} \right)^{\beta_d+1} \frac{e^{h\nu_{0,d}/k_B T_d} - 1}{e^{h\nu/k_B T_d} - 1} \\
 & + \sum_{j=1}^{N_{\text{src}}} a_{j,\text{src}} \left(\frac{\nu}{\nu_{0,\text{src}}} \right)^{\alpha_{j,\text{src}}-2}
 \end{aligned}$$

- Cosmic Microwave Background
- Synchrotron emission
- Free-free emission
- Anomalous Microwave (spinning dust) emission
- Dust emission
- Point source (stars, galaxies) emission



We can reconstruct the sky model using the maps from different frequencies

HOW TO CALCULATE THE RESIDUAL?

$$r_j = (d_j - n_j^{\text{corr}} - s_j^{1\text{Hz}}) / g_j - s_j^{\text{sky}} - s_j^{\text{orb}} - s_j^{\text{fsl}} - s_j^{\text{leak}}$$

- Ideally the residual should be pure normal noise, meaning only the white noise remains in the system
- However, in a system as complex as Planck satellite there are many sources of 'noise'

r_j - residual TOD

d_j - raw TOD (actual data)

n_j^{corr} - correlated noise

$s_j^{1\text{Hz}}$ - electronic 1Hz spike correction

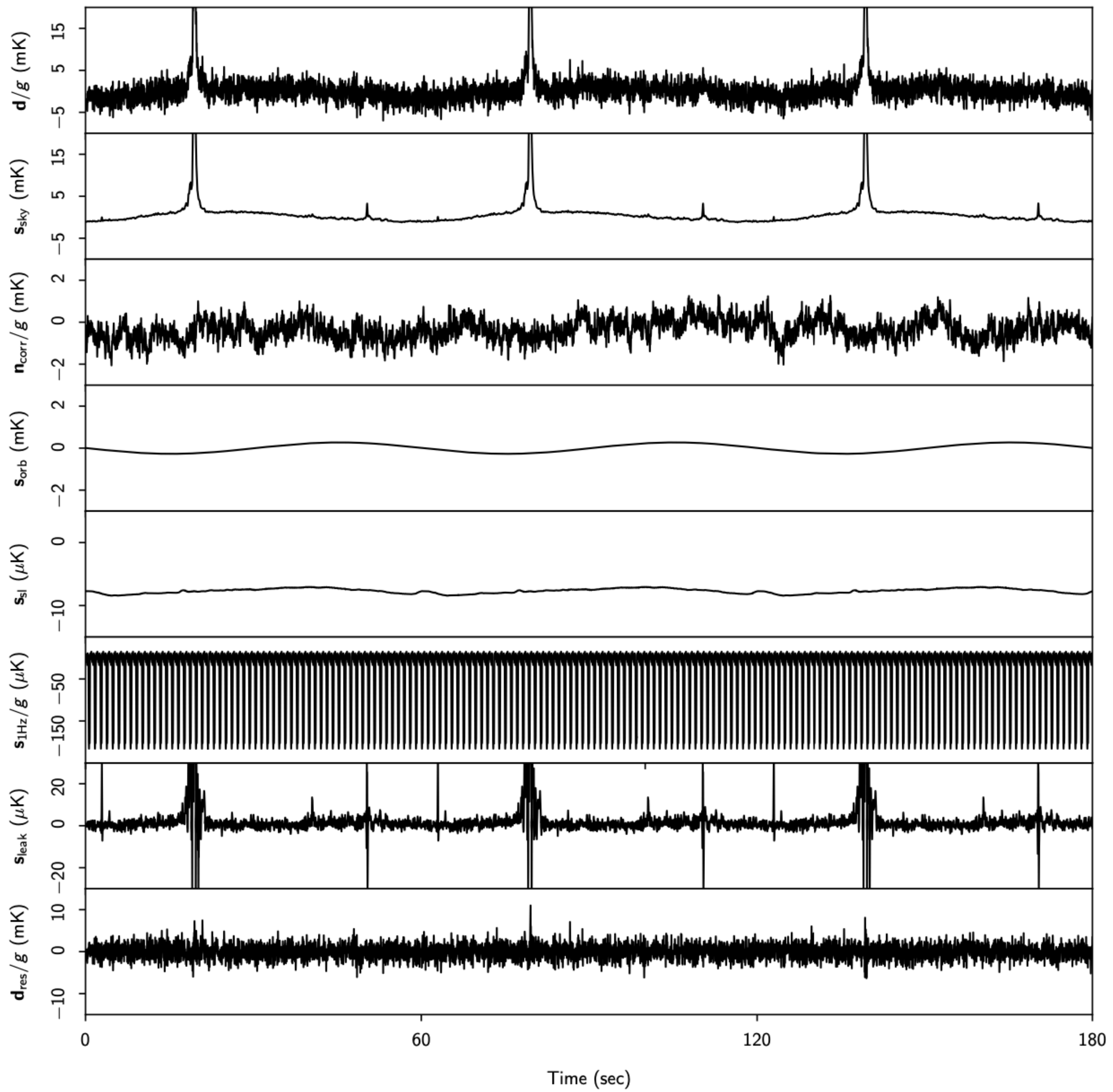
g_j - instrumental gain

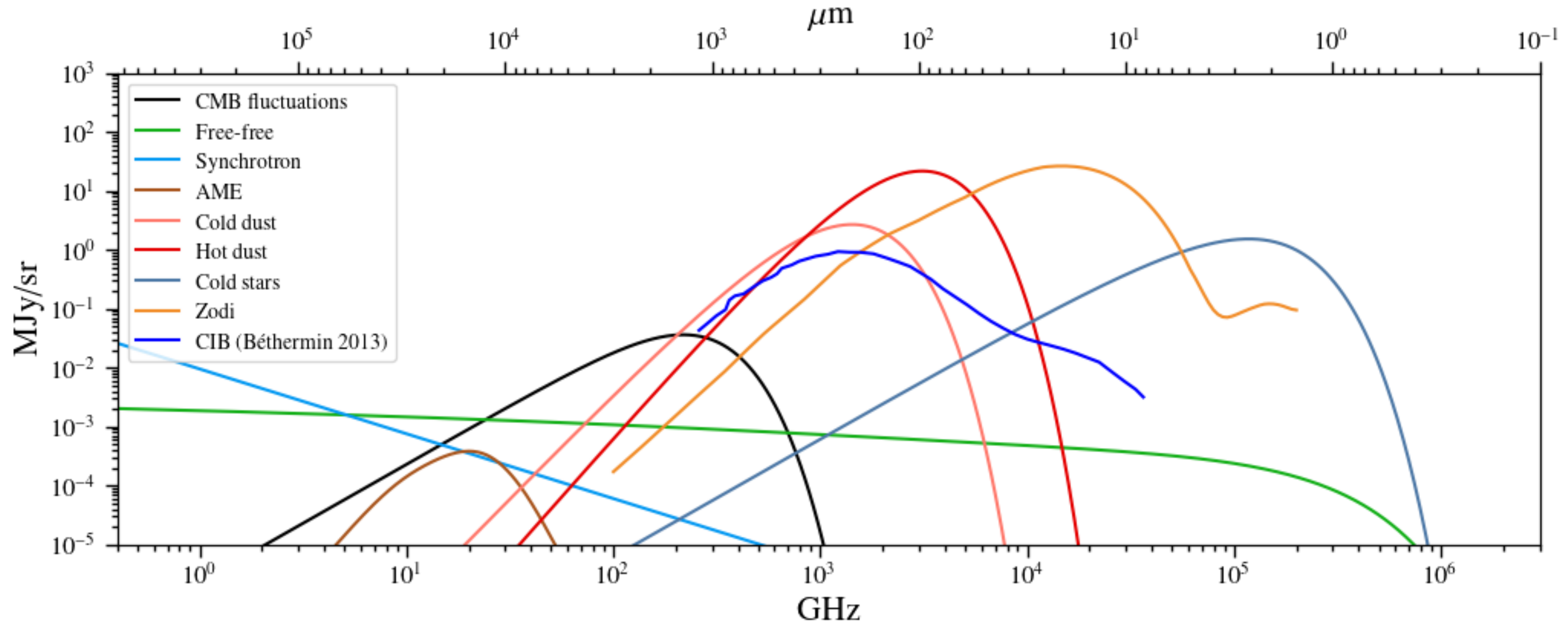
s_j^{sky} - sky signal

s_j^{orb} - orbital CMB dipole signal

s_j^{fsl} - far sidelobes correction

s_j^{leak} - bandpass and beam leakage correction





ADDING MORE COMPONENTS!

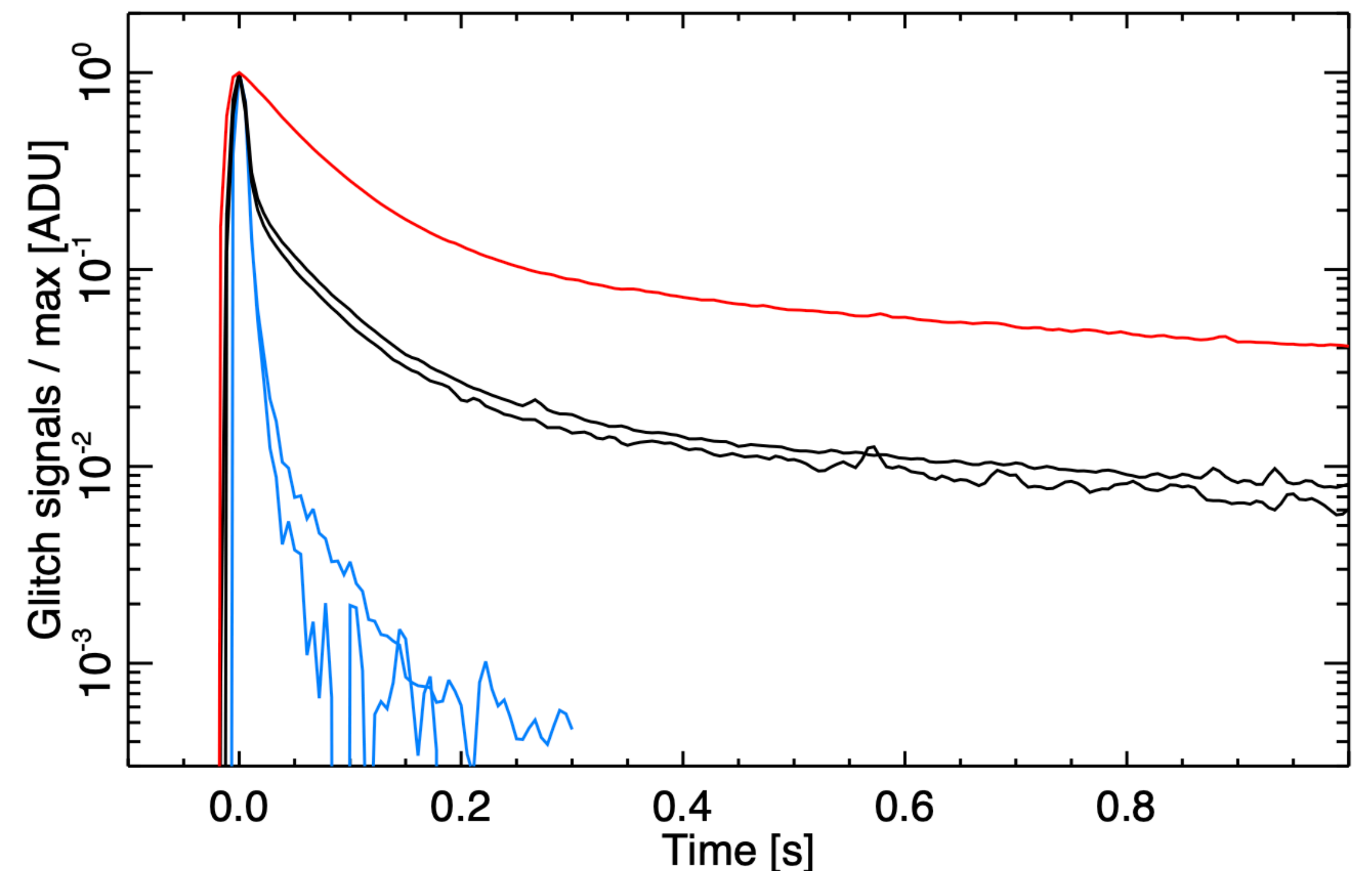
Interesting side-project going on is adding DIRBE, FIRAS, IRIS and other high frequency maps, which allows to solve the degeneracies

PLANCK HFI

- The **analogue-to-digital conversion (ADC)** in the HFI was drifting with time, and has both linear (similar to LFI) and non-linear effects, which require correction
- HFI cooler was actively trying to compensate **temperature variations** through out the whole mission (unlike passive cooler for LFI), which creates extra source of instrumental noise.
- **Cosmic rays** created extra signal depending on which part of the detector they would hit
- Since HFI was using a different detector technology (radiometers on LFI vs bolometers on HFI), and required higher angular sensitivity while measuring higher frequencies compared to LFI, the **bolometer transfer function** plays an important role in the deconvolution of data

COSMIC RAY

- **The blue line** shows an example for short glitches due to a direct impact on a thermometer
- **The black line** - for long glitches due to an impact on the support structure of a bolometer's absorber
- **The red line** - for slow glitches, the origin of which is a mystery not known to humankind



TRANSFER FUNCTION

- Describes a reaction of a bolometer to measuring a signal through the series of filters

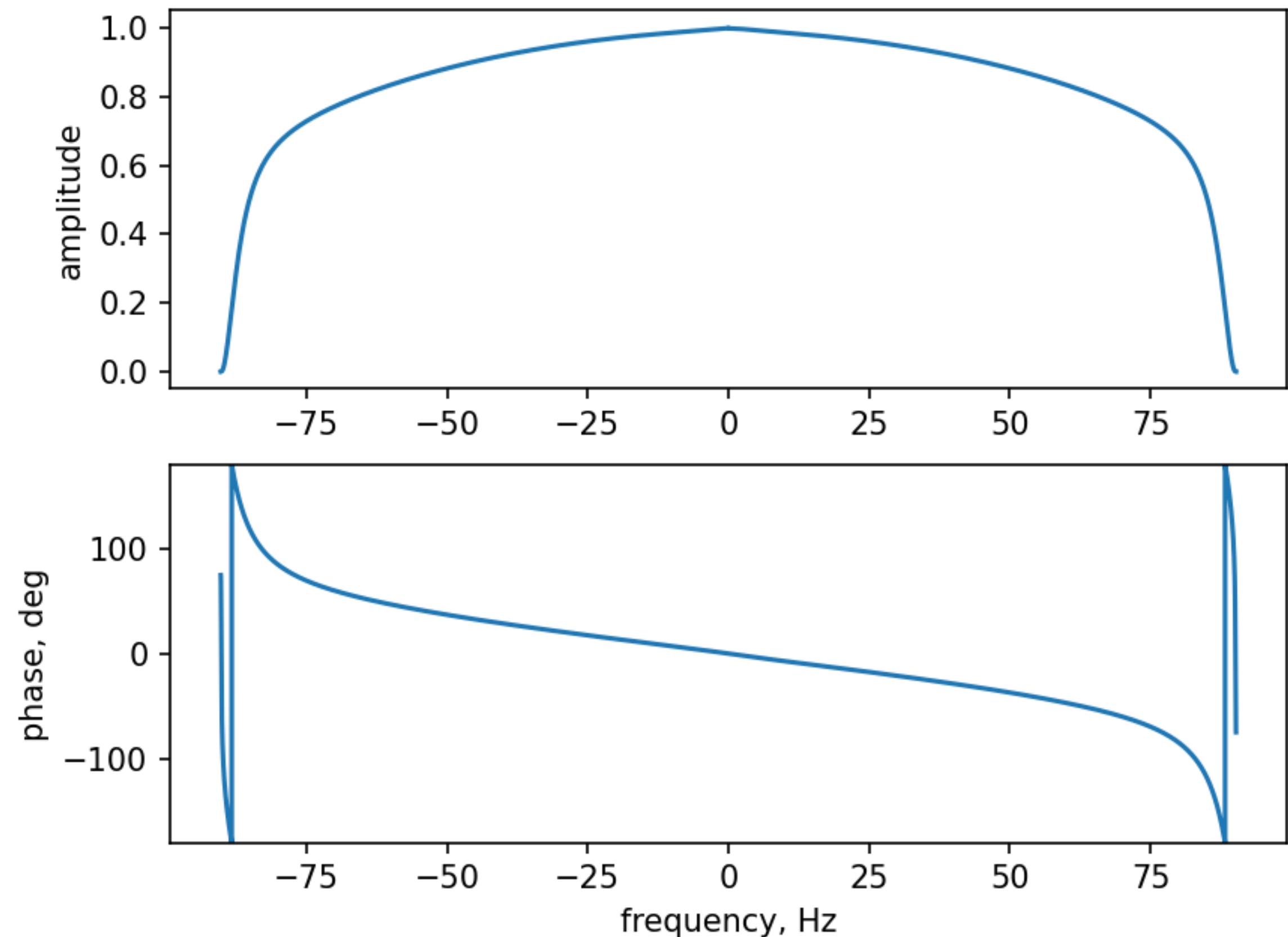
$$f_{\text{tran}}(\omega) = F(\omega)H'(\omega)$$

$$F(\omega) = \sum_{i=1,4} \frac{a_i}{1 + i\omega\tau_i}$$

$$H(\omega) = \prod_{i=1,5} h_i$$

single pole low pass filters (bolometer transfer function)

effective electronics transfer function



TRANSFER FUNCTION

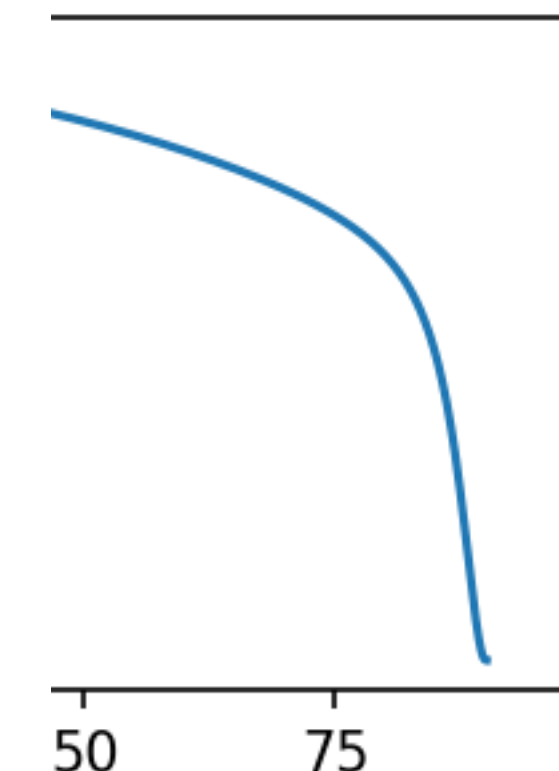
- Descriptions of filters

$$f_{\text{tran}}(\omega) :$$

$$F(\omega) =$$

$$H(\omega) =$$

Filter	Description	Parameters	Function
0	Stray capacitance low pass filter	$\tau_{\text{stray}} = R_{\text{bolo}} C_{\text{stray}}$	$h_0 = \frac{1}{1.0 + \tau_{\text{stray}} s}$
1	Low pass filter	$R_1 = 1 \text{ k}\Omega$ $C_1 = 100 \text{ nF}$	$h_1 = \frac{2 + R_1 C_1 s}{2(1 + R_1 C_1 s)}$
2	Sallen Key high pass filter	$R_2 = 51 \text{ k}\Omega$ $C_2 = 1 \mu\text{F}$	$h_2 = \frac{(R_2 C_2 s)^2}{(1 + R_2 C_2 s)^2}$
3	Sign reverse with gain	...	$h_3 = -5.1$
4	Single pole low pass filter with gain	$R_4 = 10 \text{ k}\Omega$ $C_4 = 10 \text{ nF}$	$h_4 = \frac{1.5}{1 + R_4 C_4 s}$
5	Single pole high pass filter coupled to a Sallen Key low pass filter	$R_9 = 18.7 \text{ k}\Omega$ $R_{12} = 37.4 \text{ k}\Omega$ $C = 10.0 \text{ nF}$ $R_{78} = 510 \text{ k}\Omega$ $C_{18} = 1.0 \mu\text{F}$ $K_3 = R_9^2 R_{78} R_{12}^2 C^2 C_{18}$ $K_2 = R_9 R_{12}^2 R_{78} C^2 + R_9^2 R_{12}^2 C^2$ $\quad + R_9 R_{12}^2 R_{78} C_{18} C$ $K_1 = R_9 R_{12}^2 C + R_{12} R_{78} R_9 C_{18}$	$h_5 = \frac{2 R_{12} R_9 R_{78} C_{18} s}{s^3 K_3 + s^2 K_2 + s K_1 + R_{12} R_9}$



Bolometer	a_1	τ_1 [ms]	a_2	τ_2 [ms]	a_3	τ_3 [ms]	a_4	τ_4 [ms]	τ_{stray} [ms]	S_{phase}
100-1a	0.392	10.0	0.534	20.9	0.0656	51.3	0.00833	572	1.59	0.00139
100-1b	0.484	10.3	0.463	19.2	0.0451	71.4	0.00808	594	1.49	0.00139
100-2a	0.474	6.84	0.421	13.6	0.0942	37.6	0.0106	346	1.32	0.00125
100-2b	0.126	5.84	0.717	15.1	0.142	35.1	0.0145	293	1.38	0.00125
100-3a	0.744	5.39	0.223	14.7	0.0262	58.6	0.00636	907	1.42	0.00125
100-3b	0.608	5.48	0.352	15.5	0.0321	63.6	0.00821	504	1.66	0.00125
100-4a	0.411	8.2	0.514	17.8	0.0581	57.9	0.0168	370	1.25	0.00125
100-4b	0.687	11.3	0.282	24.3	0.0218	62.0	0.00875	431	1.38	0.00139
143-1a	0.817	4.47	0.144	12.1	0.0293	38.7	0.0101	472	1.42	0.00125
143-1b	0.49	4.72	0.333	15.6	0.134	48.1	0.0435	270	1.49	0.00125
143-2a	0.909	4.7	0.076	17.0	0.00634	100	0.00871	363	1.48	0.00125
143-2b	0.912	5.24	0.051	16.7	0.0244	26.5	0.0123	295	1.46	0.00125
143-3a	0.681	4.19	0.273	9.56	0.0345	34.8	0.0115	317	1.45	0.00125
143-3b	0.82	4.48	0.131	13.2	0.0354	35.1	0.0133	283	1.61	0.00083
143-4a	0.914	5.69	0.072	18.9	0.00602	48.2	0.00756	225	1.59	0.00125
143-4b	0.428	6.06	0.508	6.06	0.0554	22.7	0.00882	84	1.82	0.00125
143-5	0.491	6.64	0.397	6.64	0.0962	26.4	0.0156	336	2.02	0.00139
143-6	0.518	5.51	0.409	5.51	0.0614	26.6	0.0116	314	1.53	0.00111
143-7	0.414	5.43	0.562	5.43	0.0185	44.9	0.00545	314	1.86	0.00139
217-5a	0.905	6.69	0.080	21.6	0.00585	65.8	0.00986	342	1.57	0.00111
217-5b	0.925	5.76	0.061	18.0	0.00513	65.6	0.0094	287	1.87	0.00125
217-6a	0.844	6.45	0.068	19.7	0.0737	31.6	0.0147	297	1.54	0.00125
217-6b	0.284	6.23	0.666	6.23	0.0384	24	0.0117	150	1.46	0.00111
217-7a	0.343	5.48	0.574	5.48	0.0717	23	0.0107	320	1.52	0.00139
217-7b	0.846	5.07	0.127	14.40	0.0131	47.9	0.0133	311	1.51	0.00139
217-8a	0.496	7.22	0.439	7.22	0.0521	32.5	0.0128	382	1.79	0.00111
217-8b	0.512	7.03	0.41	7.03	0.0639	27.2	0.0139	232	1.73	0.00125
217-1	0.014	3.46	0.956	3.46	0.0271	23.3	0.00359	1980	1.59	0.00111
217-2	0.978	3.52	0.014	26.1	0.00614	42	0.00194	686	1.6	0.00125
217-3	0.932	3.55	0.034	3.55	0.0292	32.4	0.00491	279	1.74	0.00125
217-4	0.658	1.35	0.32	5.55	0.0174	26.8	0.00424	473	1.71	0.00111
353-3a	0.554	7.04	0.36	7.04	0.0699	30.5	0.0163	344	1.7	0.00125
353-3b	0.219	2.68	0.671	6.95	0.0977	23.8	0.0119	289	1.57	0.00111
353-4a	0.768	4.73	0.198	9.93	0.0283	50.5	0.00628	536	1.81	0.00125
353-4b	0.684	4.54	0.224	10.8	0.0774	80	0.0149	267	1.66	0.00111
353-5a	0.767	5.96	0.159	12.4	0.0628	30.3	0.0109	357	1.56	0.00111
353-5b	0.832	6.19	0.126	11.1	0.0324	35	0.0096	397	1.66	0.00111
353-6a	0.049	1.76	0.855	6.0	0.0856	21.6	0.0105	222	1.99	0.00125
353-6b	0.829	5.61	0.127	5.61	0.0373	25.2	0.00696	360	2.28	0.00111
353-1	0.41	0.74	0.502	4.22	0.0811	17.7	0.0063	329	1.32	0.00097
353-2	0.747	3.09	0.225	7.26	0.0252	44.7	0.00267	513	1.54	0.00097
353-7	0.448	0.9	0.537	4.1	0.0122	27.3	0.00346	433	1.78	0.00125
353-8	0.718	2.23	0.261	6.08	0.0165	38	0.00408	268	1.77	0.00111
545-1	0.991	2.93	0.007	26.0	0.00139	2600	2.16	0.00111
545-2	0.985	2.77	0.013	24.0	0.00246	2800	1.87	0.00097
545-4	0.972	3.0	0.028	25.0	0.00078	2500	2.22	0.00111
857-1	0.974	3.38	0.023	25.0	0.00349	2200	1.76	0.00111
857-2	0.84	1.48	0.158	6.56	0.00249	3200	2.2	0.00125
857-3	0.36	0.04	0.627	2.4	0.0111	17	0.002	1900	1.52	0.00126
857-4	0.278	0.4	0.719	3.92	0.00162	90	0.00152	800	1.49	0.00056

TT

NI

Filter Desc

Function

- Descri measu filters

$$f_{\text{tran}}(\omega) =$$

$$F(\omega) =$$

$$H(\omega) =$$

0 Stray capacitance l

1 Low pass filter

2 Sallen Key high pa

3 Sign reverse with g

4 Single pole low pa

5 Single pole high p
Sallen Key low]

$$= \frac{1}{1.0 + \tau_{\text{stray}} s}$$

$$= \frac{2 + R_1 C_1 s}{2(1 + R_1 C_1 s)}$$

$$= \frac{(R_2 C_2 s)^2}{(1 + R_2 C_2 s)^2}$$

$$= -5.1$$

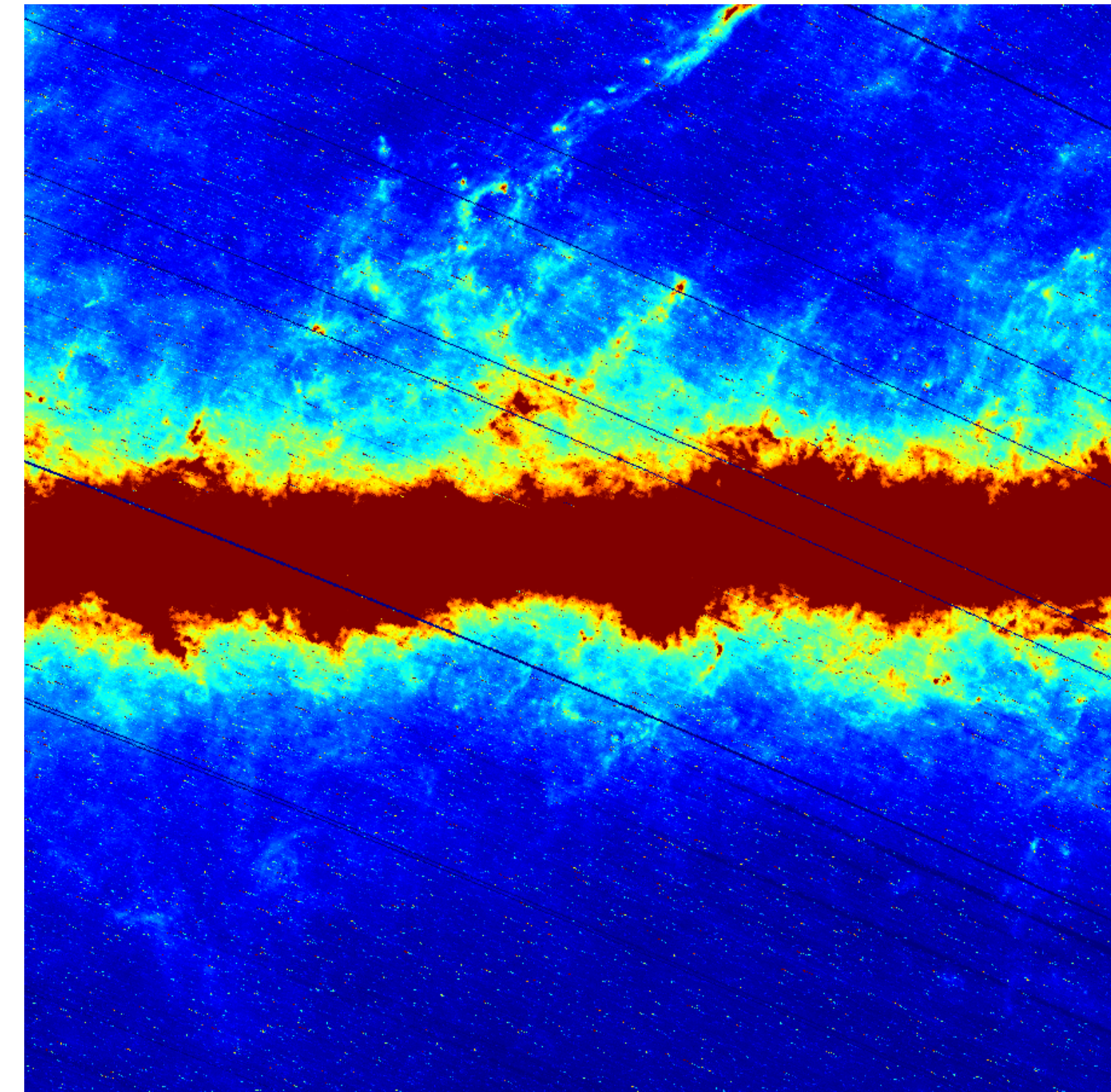
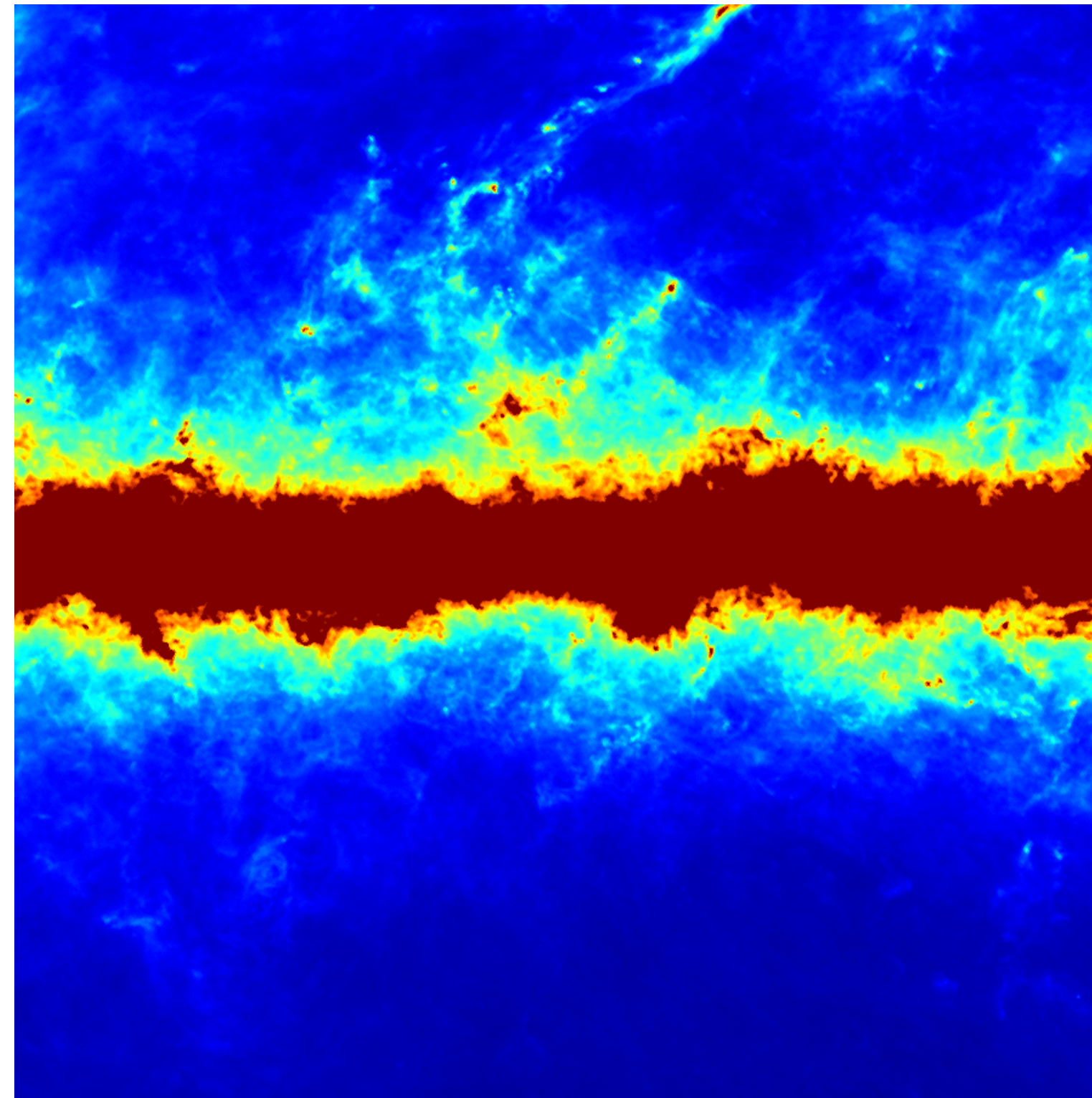
$$= \frac{1.5}{1 + R_4 C_4 s}$$

$$= \frac{2 R_{12} R_9 R_{78} C_{18} s}{s^3 K_3 + s^2 K_2 + s K_1 + R_{12} R_9}$$



WHAT'S THE DIFFERENCE?

- Besides from other effects, correction for which has not been implemented yet, the transfer function effect is the most obvious one
- The map looks slightly shifted, which is exactly the transfer function effect



DATA MODEL

$$d = Ts + n$$

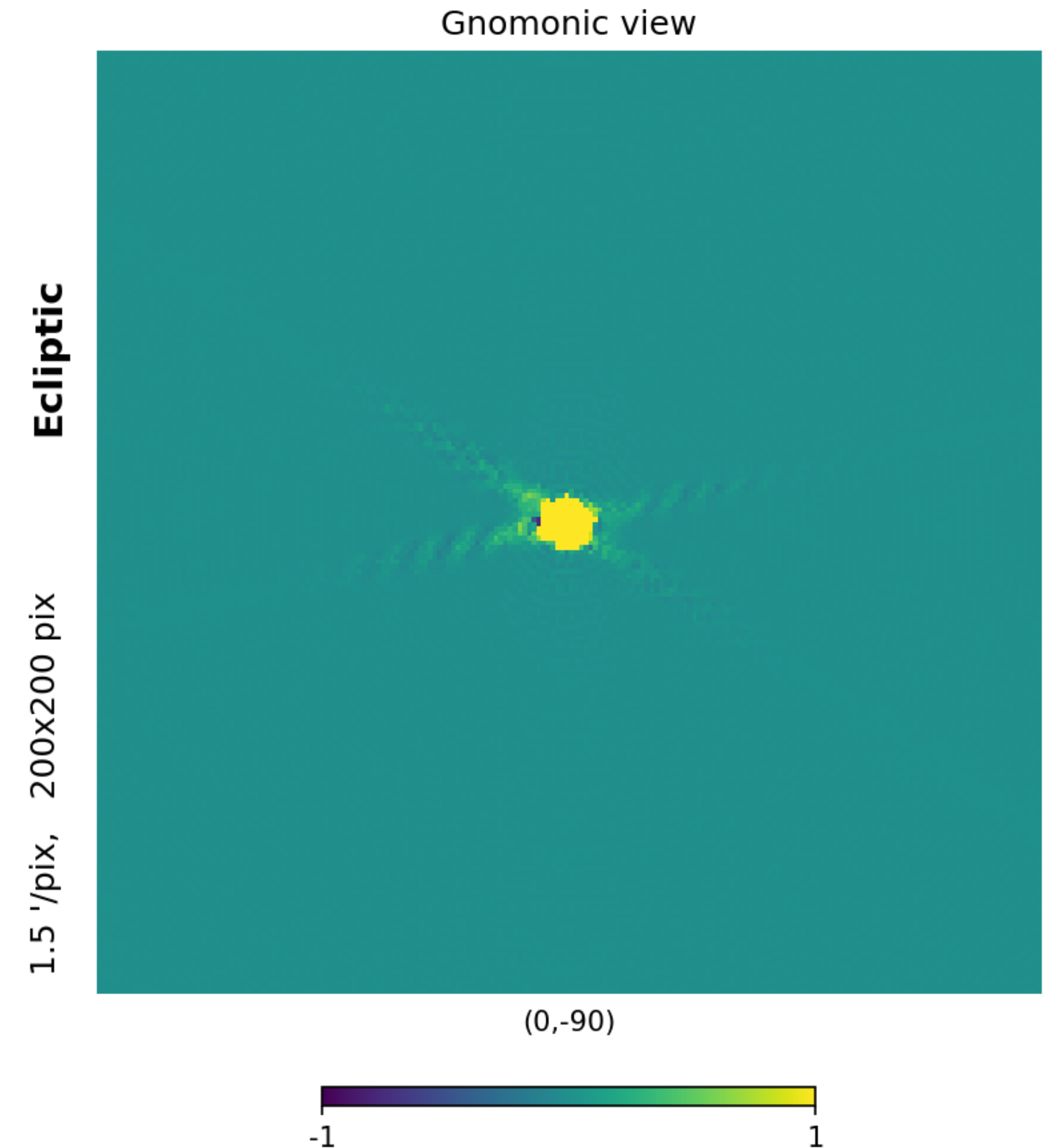
Data recorded from the detector (d) is a sky signal (s) modified with the detector transfer function (T) plus noise (n)

$$T = F^{-1}f_{tran}(\omega)F$$

The operator (T) describing the transfer function effect is a convolution operator in real space or a multiplication operator in Fourier space with transfer function (f) and Fourier transform (F)

EXPERIMENT

- Let's take the Planck HFI pointing
- Generate a bright beam at one of the often passed points (pole) (s)
- Apply a transfer function T
- Add normal noise n to data d

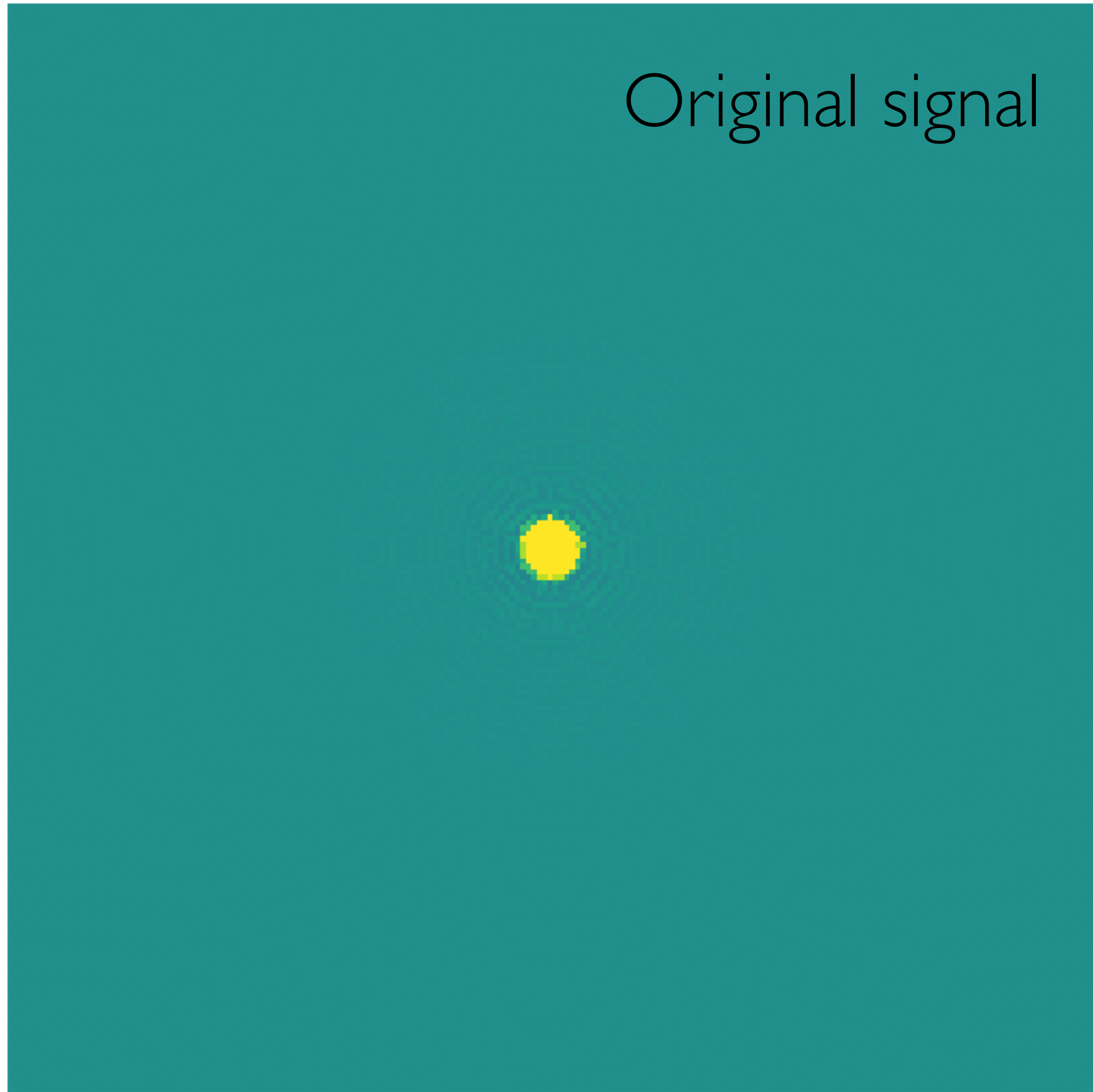


Gnomonic view

Original signal

Ecliptic

1.5 '/pix, 200x200 pix



(0,-90)

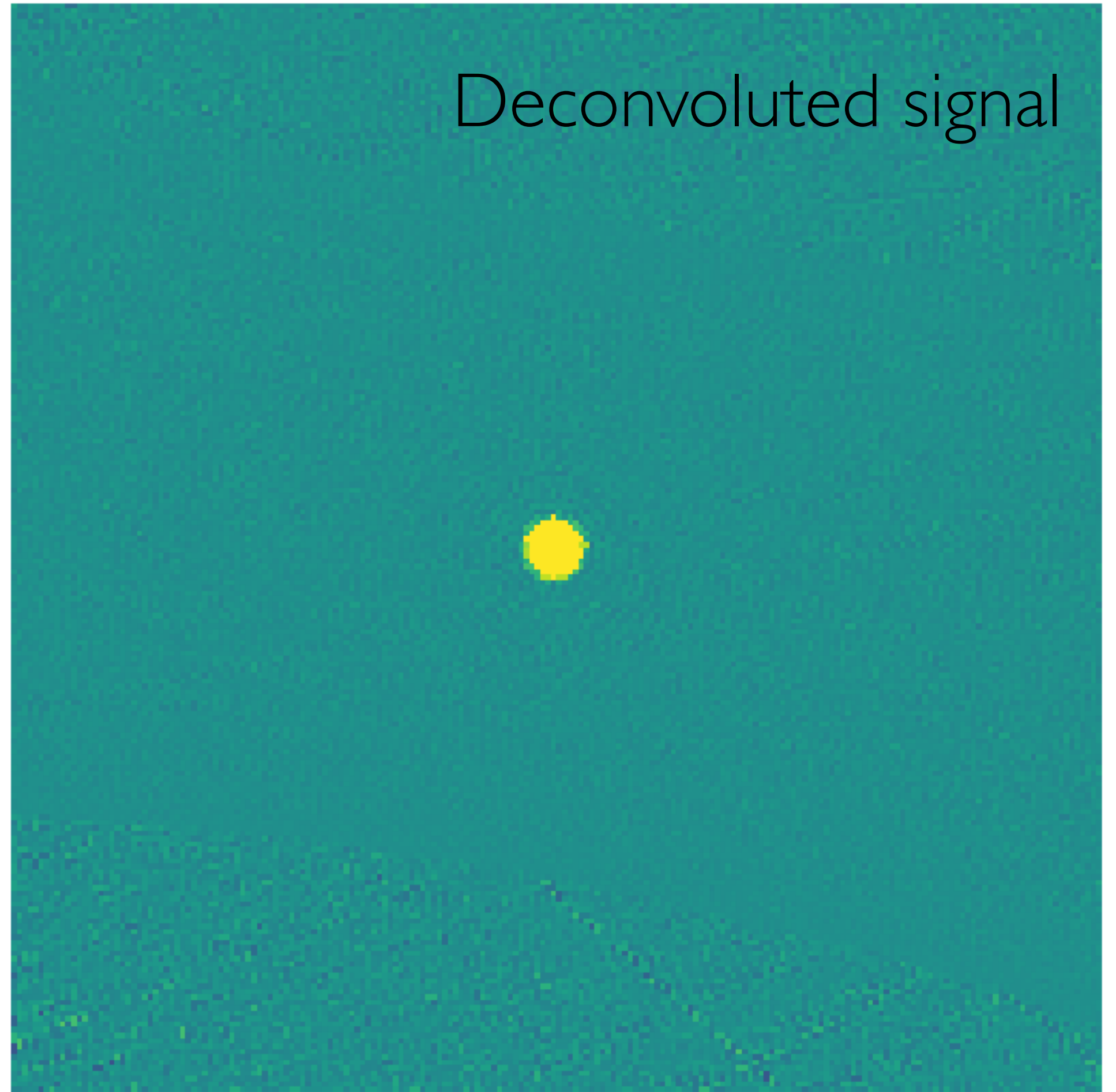


Gnomonic view

Deconvoluted signal

Ecliptic

1.5 '/pix, 200x200 pix



(0,-90)



Straight deconvolution (applying T^{-1} to d) amplifies noise as $T^{-1}n$

Gnomonic view

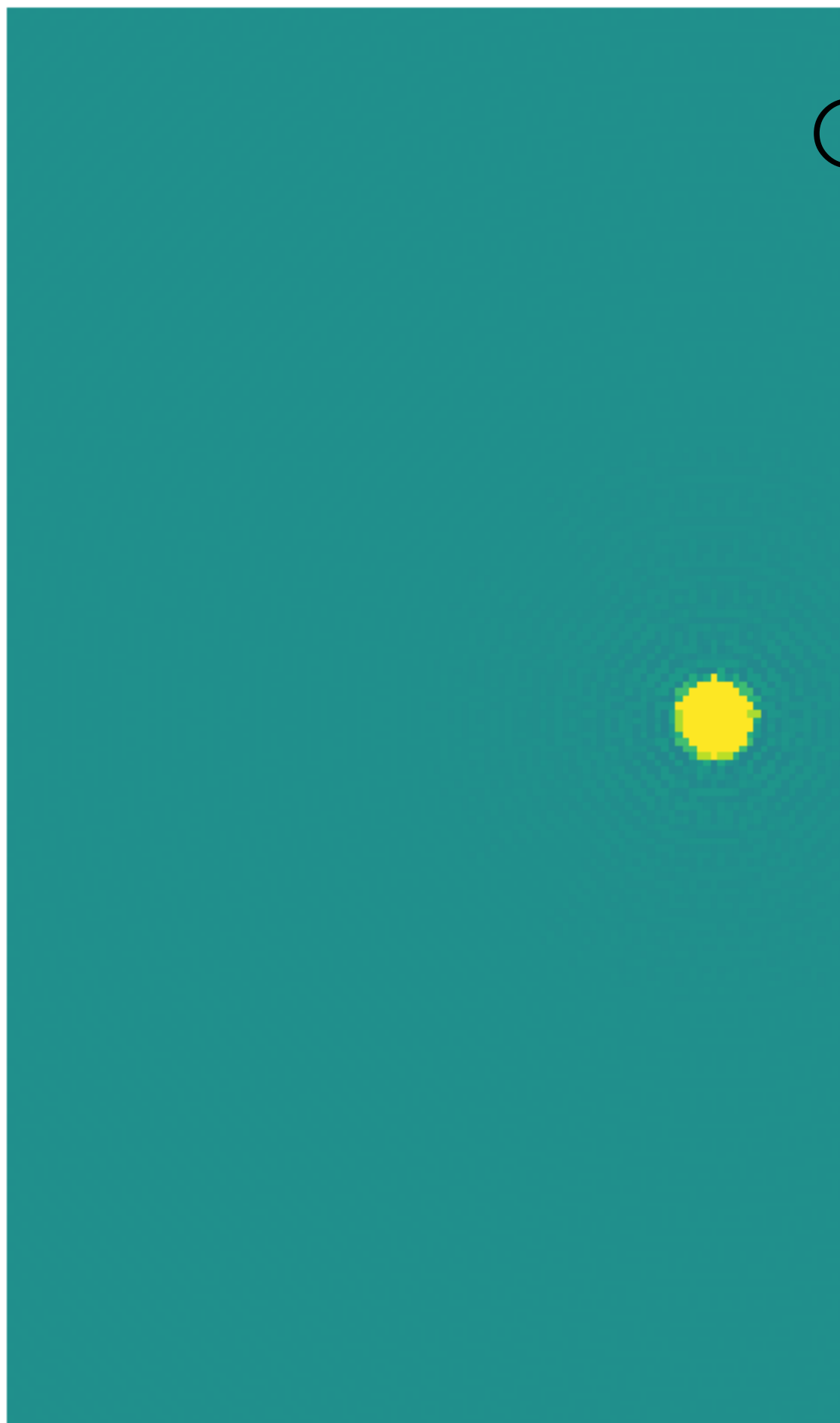
Gnomonic view

Gnomonic view

Deconvoluted signal

Ecliptic

1.5 ' /pix, 200x200 pix



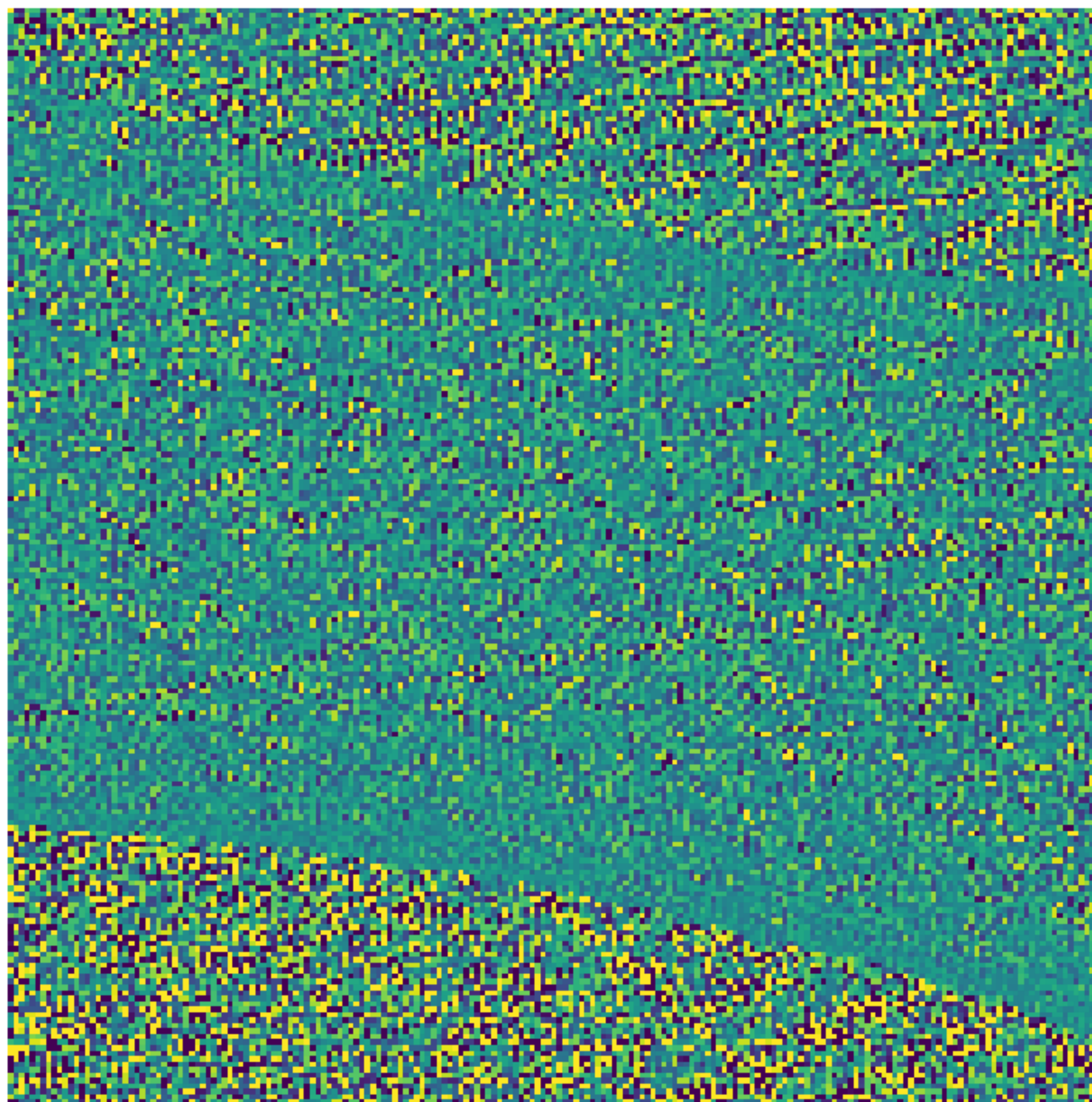
(0,-90)

-1

Straight deco

Ecliptic

1.5 ' /pix, 200x200 pix



(0,-90)

-0.1

0.1

(0,-90)

1

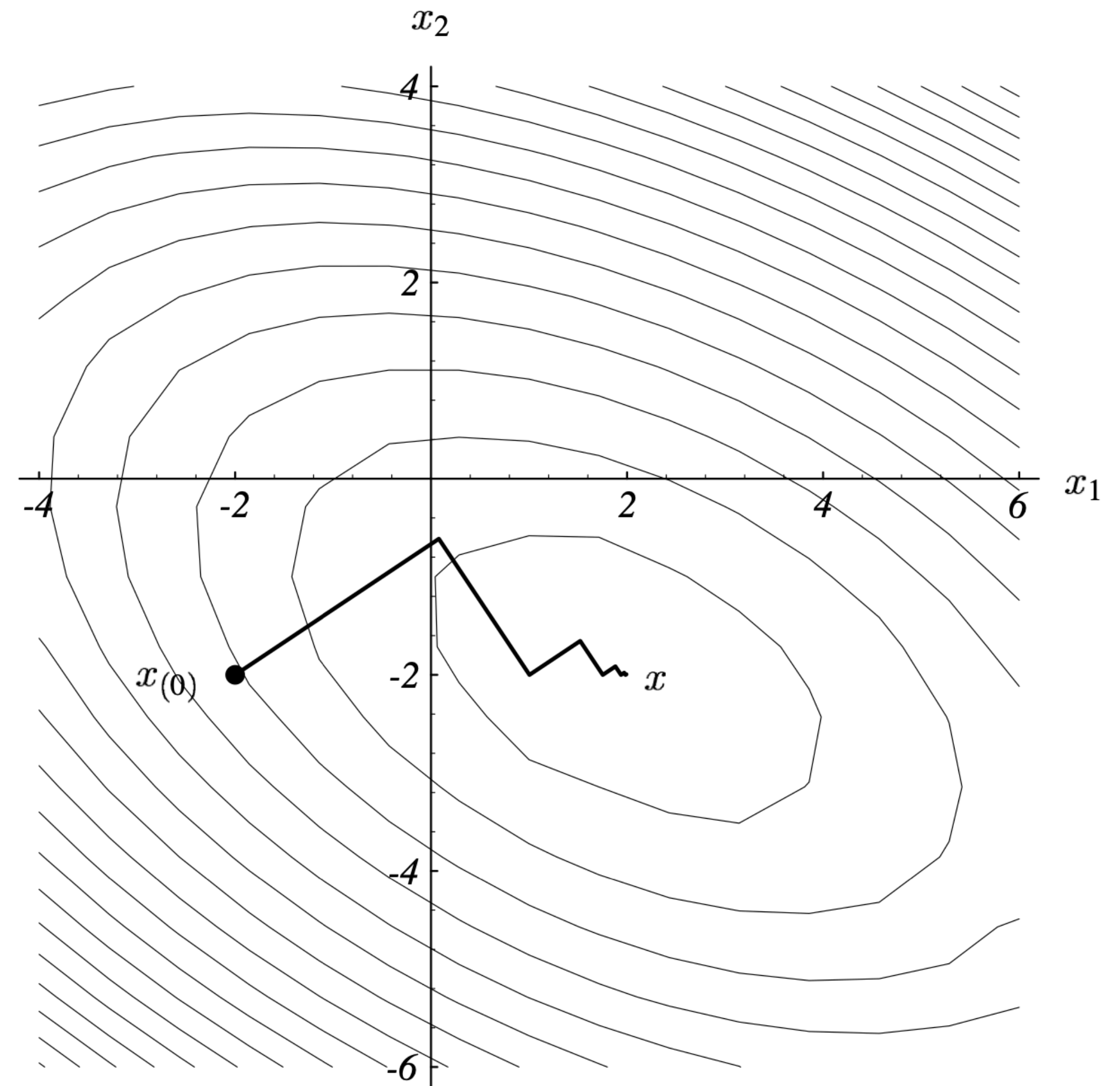
noise as $T^{-1}n$

DEALING WITH TRANSFER FUNCTION AT MAPMAKING LEVEL

- Instead of applying T^{-1} to the data d , as was done by Planck HFI, we can include the operator T into the mapmaking equation
$$(P^T T^T N^{-1} T P)m = (P^T T^T N^{-1})d$$
- Instead of applying the inverse, we are applying the transpose, which is identical to shifting the data forward in time
- We are stacking the data and applying T along the pointing direction, decreasing white noise

THE COST?

- Extremely computationally heavy, since we are dealing with $\text{NTOD} = 7 \cdot 10^{11}$, and $\text{NSIDE} = 2048$, corresponding to $\text{NPIX} = 10^7$
- For example, the pointing matrix $P = (\text{NPIX}, \text{NTOD})$
- However, it's still **possible** to solve for m using conjugate gradient method
- The basic mapmaking equation for LFI was $(P^T N^{-1} P)m = P^T N^{-1} d$



Thank you for your attention!