

Full flux surface (FFS) δf -gyrokinetic code: *stella*

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2. Real Space Formalism

3. Flux Tube Formalism

4. Flux Annulus Formalism

5. Code

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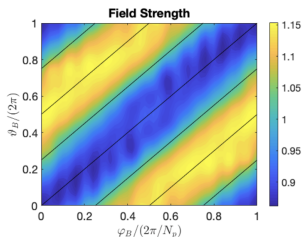
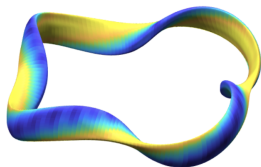
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Motivation

- ▶ Stellarators can be neoclassically optimised

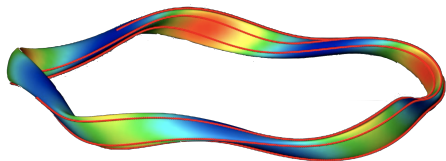
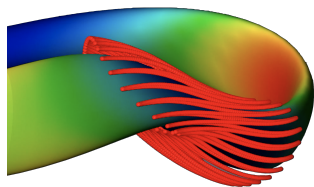
Motivation

- ▶ Stellarators are neoclassically optimised
- ▶ Demand omnigenity
- ▶ Require time-averaged radial magnetic drifts away from flux surface to vanish for all particles
- ▶ Particle orbits and neoclassical transport are the same in quasisymmetric devices as in truly axisymmetric ones
- ▶ “Unwrap” stellarator with certain transformation and magnetic field looks the same to particles



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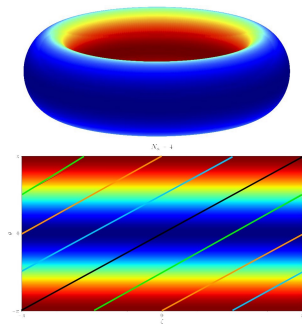


Motivation

- ▶ Stellarators are neoclassically optimised
- ▶ Hence, turbulent transport dominates \rightarrow model using δf -gyrokinetics

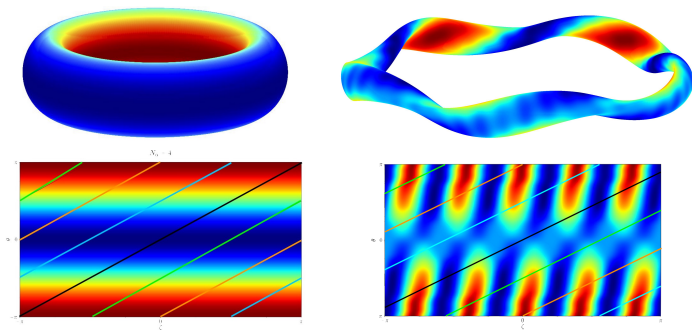
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- ▶ Modes on different field lines interact \rightarrow complicates algorithms due to α -inhomogeneity
- ▶ 3 main approaches to model turbulence:
 - ▶ real space
 - ▶ flux tube
 - ▶ full flux annulus

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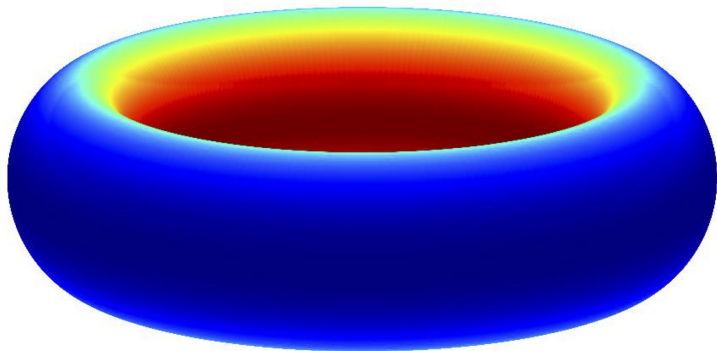
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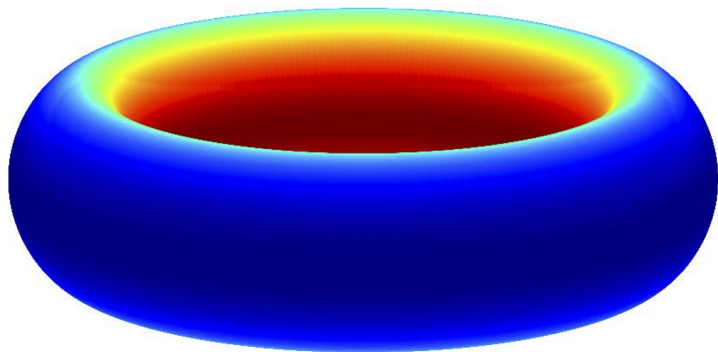
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Real space 3D formalism



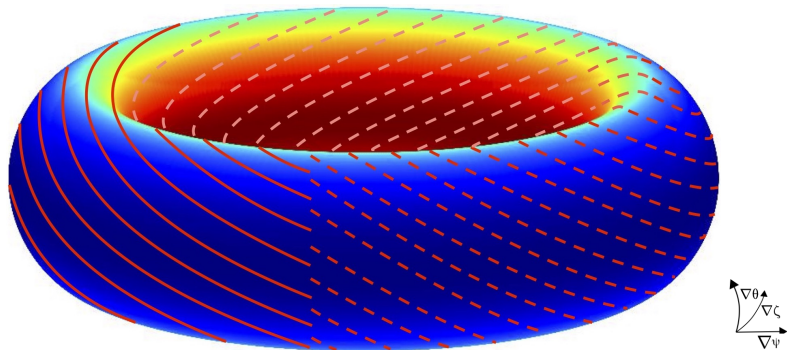
- ▶ Full device simulation in real space

Real space 3D formalism



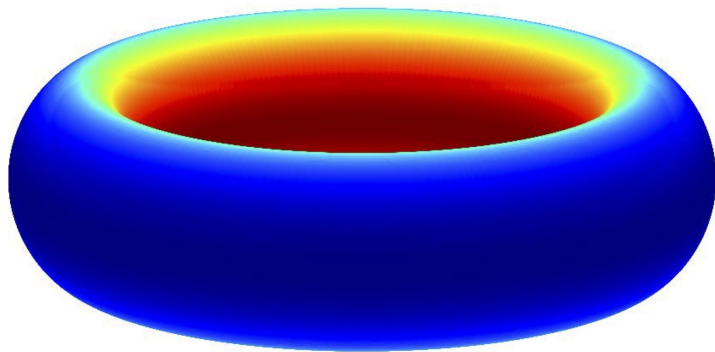
- ▶ Full device simulation in real space
- ▶ Initialise at $t = 0$ across whole device and evolve globally according to GK equation
- ▶ Use finite difference schemes to take derivatives
- ▶ Impose periodicity in ζ

Real space 3D formalism: toroidal boundary conditions



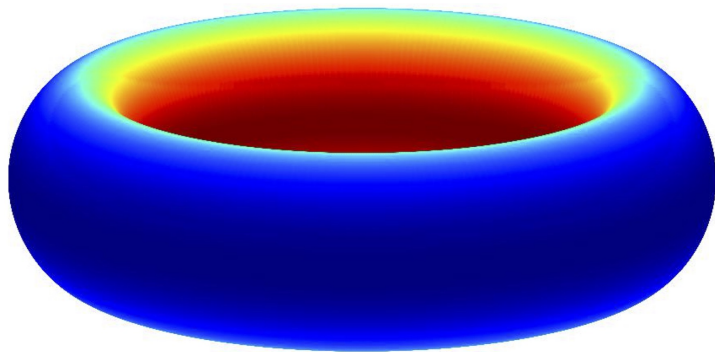
- ▶ Want domain to be 2π -periodic in ζ
- ▶ Field lines on a non-rational surface will not close on each other
- ▶ Need to interpolate field lines back onto ones which lie on our α -grid

Real space 3D formalism: pros and cons



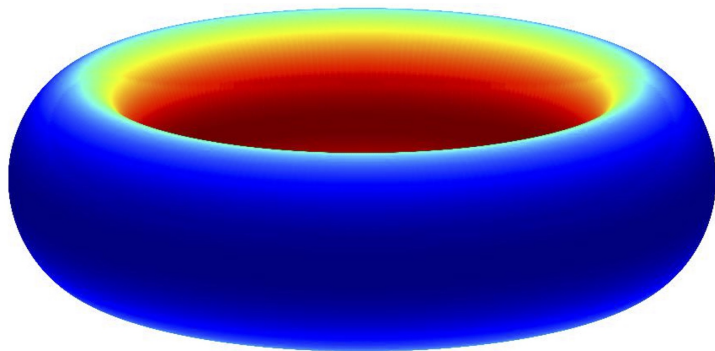
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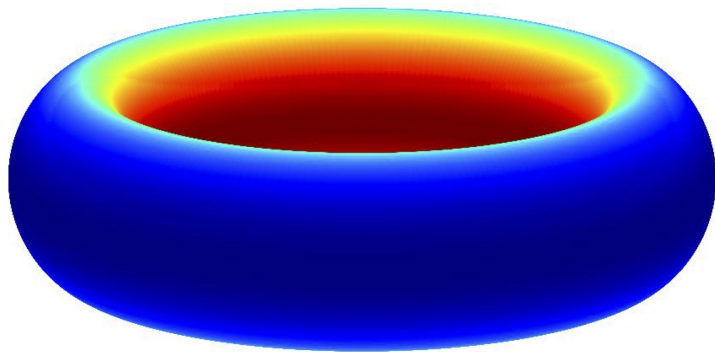
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 - ▶ Can take months on multiple CPU cores

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- ▶ Loose spectral accuracy in derivatives
- ▶ Radial boundary conditions are difficult to choose

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Flux tube formalism

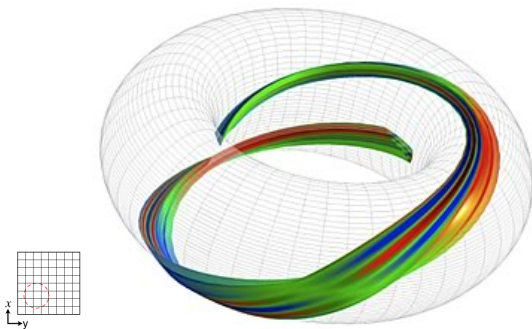


Image: SCD CCP-Plasma

- ▶ Simulation coordinates: $(x, y, z) \rightarrow (\psi, \alpha, \zeta)$

Flux tube formalism

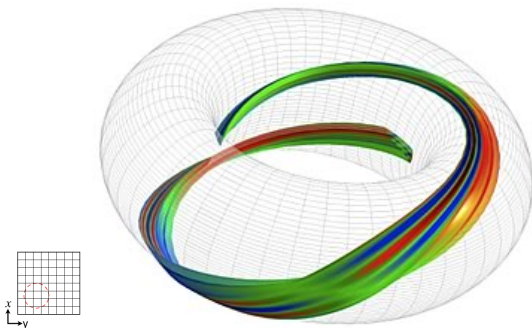


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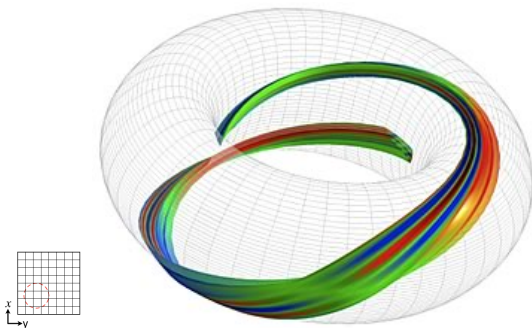


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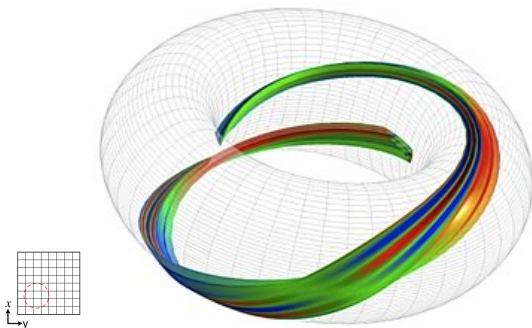


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- ▶ Initialise some δf and ϕ at $t = 0$ on simulation domain
- ▶ Evolve gyrokinetic equation pseudo-spectrally
 - ▶ Decay in v_{\parallel} ; $g(t, \mathbf{x}, v_{\parallel} \rightarrow \pm\infty, \mu) \rightarrow 0$
 - ▶ Turbulence is taken as periodic in perpendicular directions, $k_x, k_y \gg 1/L$
 - ▶ Use twist-and-shift boundary conditions in z to capture extended modes

Flux tube formalism: twist-and-shift

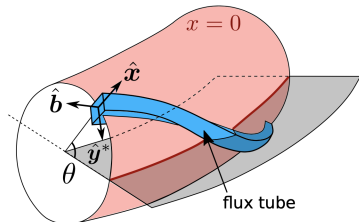


Image: Nicolas Christen, Bistable turbulent transport in fusion plasmas with rotational shear (2021)

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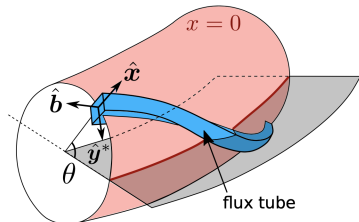
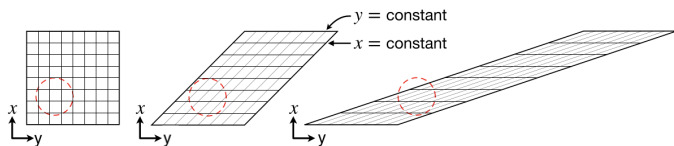


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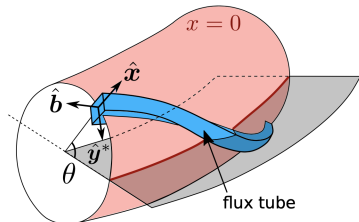
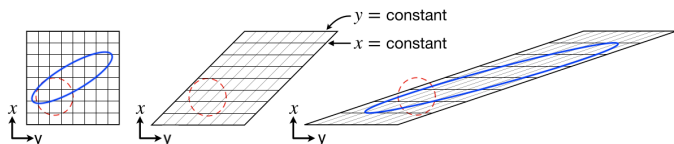


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- ▶ If $\hat{s} \propto dq/d\psi \neq 0$ then domain gets sheared as it travels around device
- ▶ Eddies get sheared
- ▶ Pushed to higher perpendicular wavenumbers

Flux tube formalism: twist-and-shift

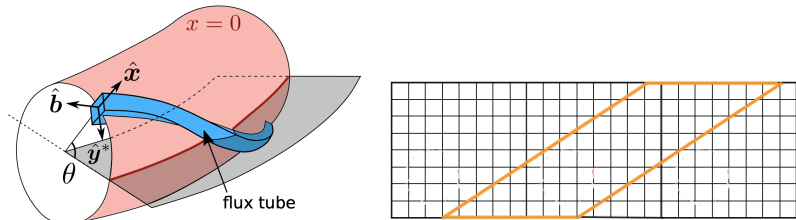


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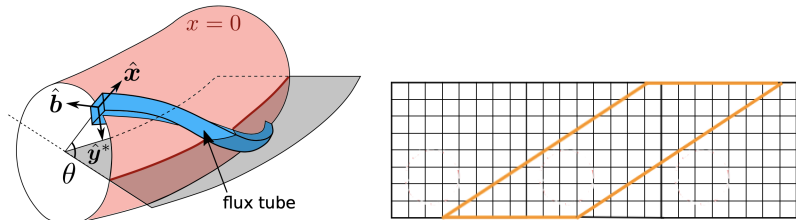


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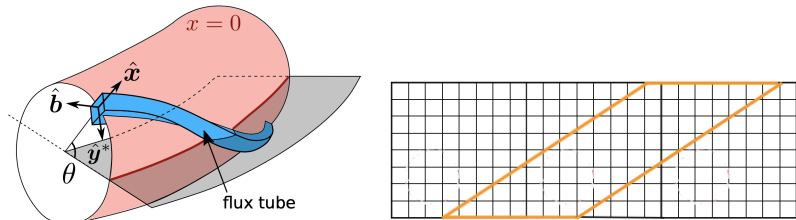


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- ▶ Use “twist-and-shift” boundary conditions to map sheared domain back onto original one
- ▶ “Twist-and-shift” is the Fourier equivalent of the real-space boundary condition *
- ▶ Enforce periodicity after one geometric turn:

$$\hat{A}_{\mathbf{k}}(z) = \hat{A}_{\mathbf{k}'}(z + 2p\pi)(\text{phase factor}) \quad (1)$$

Flux tube formalism

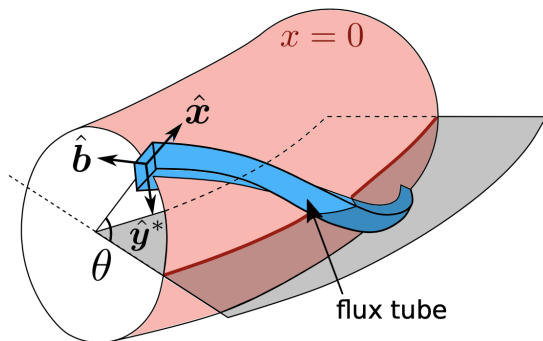


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- ▶ Flux-tube simulations are sufficient for tokamaks because we can stitch our flux tubes together

Flux tube formalism

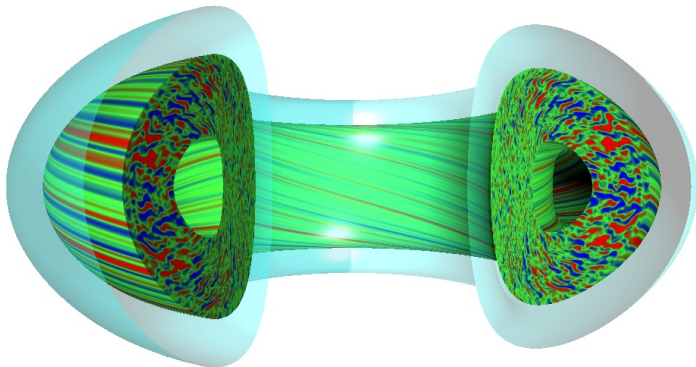


Image: J.Candy, Waltz, GYRO simulation of DIII-D

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Flux tube formalism: pros and cons

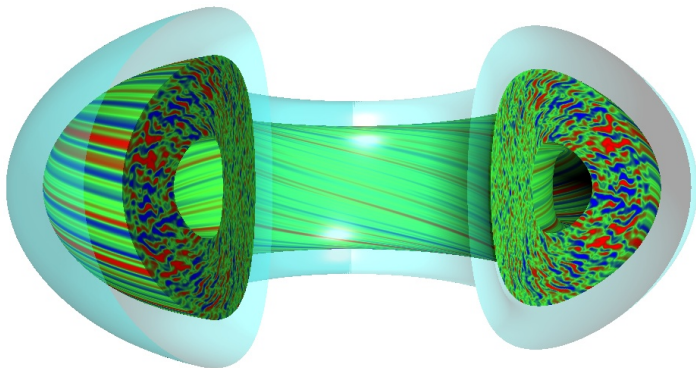


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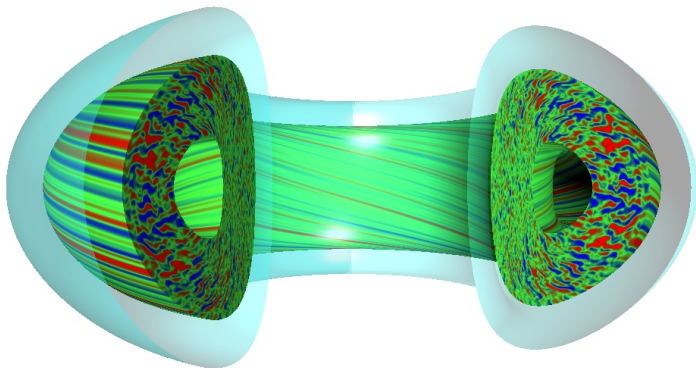


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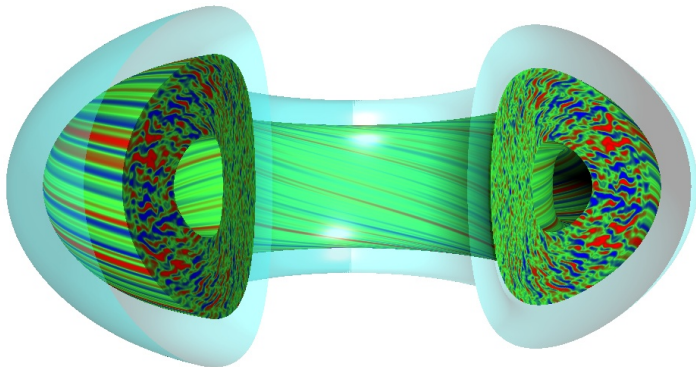


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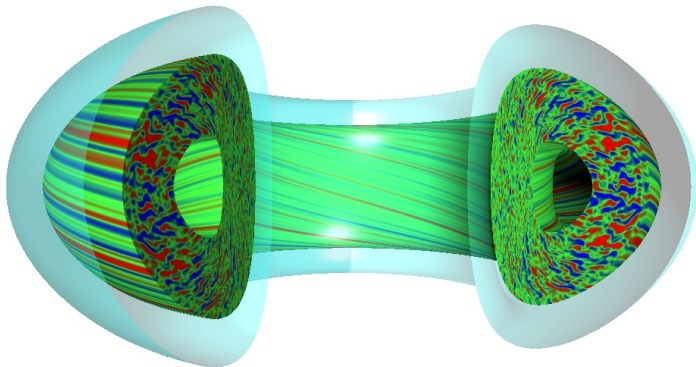


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- ▶ Very fast codes which yield quick results - can perform many simulations in quick succession
- ▶ Easy to interpret - normal modes are well defined in this system
- ▶ Retains spectral accuracy in spacial derivatives
- ▶ Does not capture global effects like coupling between different field lines

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Flux annulus formalism: motivation

- ▶ Stellarator geometry varies with field line
- ▶ Method of stitching together flux tubes no longer holds

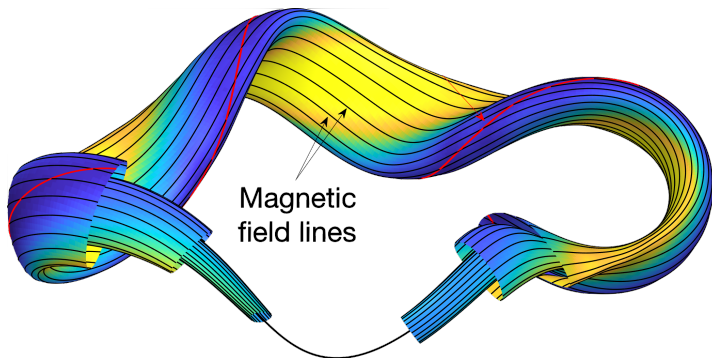
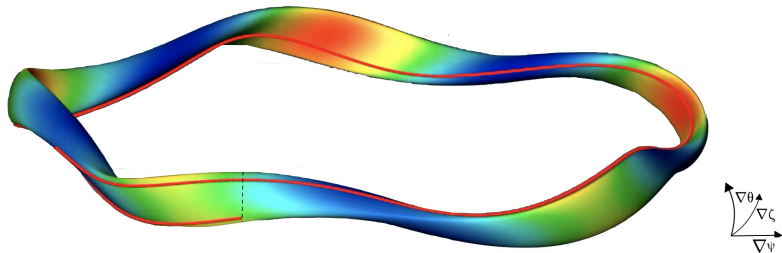


Image: UMD stellarator group

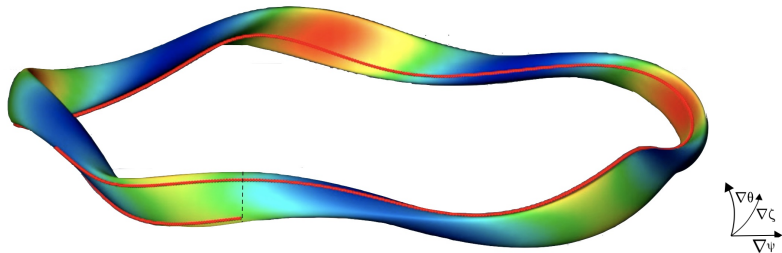
Flux annulus framework

- ▶ Domain is now 2π in ζ , not 2π in θ



Flux annulus framework

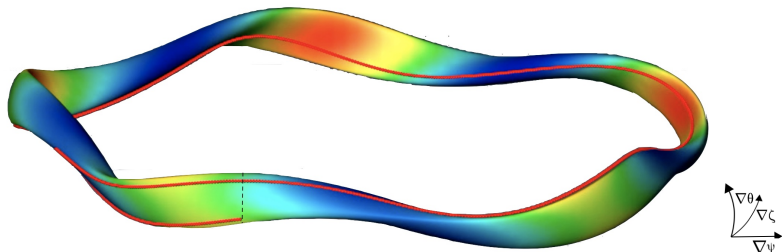
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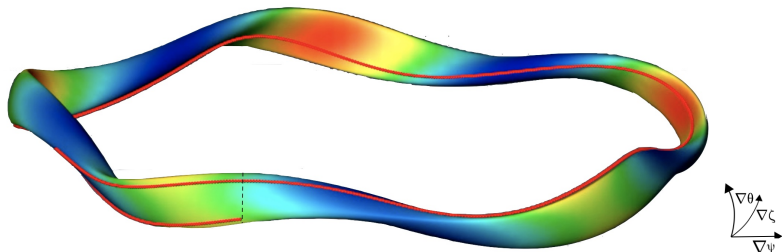
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- ▶ Simulate N_y field lines, which cover different geometry and are now coupled together

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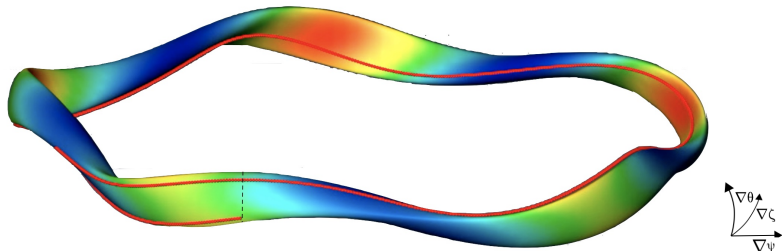
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- ▶ Want to match every incoming field line to its connecting field line - apply twist-and-shift to entire poloidal domain

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- ▶ Simulate N_y field lines, which cover different geometry and are now coupled together
- ▶ Want to match every incoming field line to its connecting field line - apply twist-and-shift to entire poloidal domain
- ▶ ρ_* now becomes an important physical parameter in simulations \rightarrow determines Δk_y

How 3D geometry modifies equations

- ▶ Geometry is no longer trivial
- ▶ But how does geometry enter our code?

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Simplified notation GK:

$$\frac{\partial g}{\partial t} = (\text{geometric factors}) \cdot (\nabla g + \nabla \langle \phi \rangle_{\mathbf{R}}) \quad (2)$$

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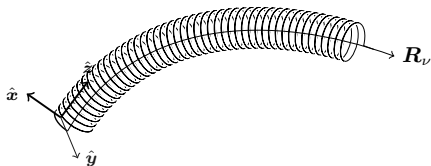
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- ▶ Geometric factors are α -dependent
- ▶ Gyro-averaging introduces coupling between different k_y -modes \rightarrow no longer a local operation



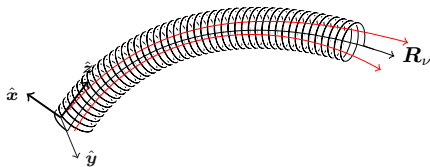
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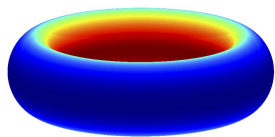
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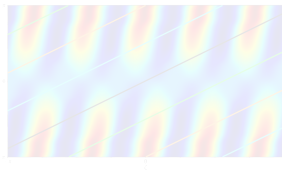
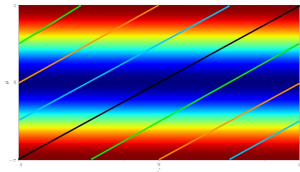
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- ▶ Geometric factors are α -dependent
- ▶ Gyro-averaging introduces coupling between different k_y -modes \rightarrow no longer a local operation
- ▶ α -inhomogeneity leads to convolutions

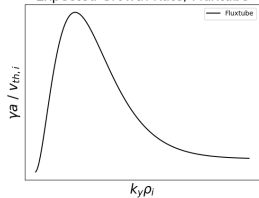
How 3D geometry modifies expectations



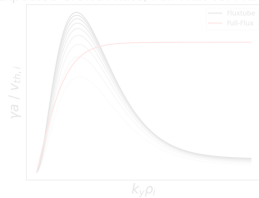
$N_x = 4$



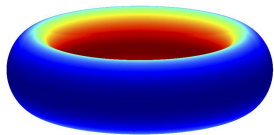
Expected Growth Rate; Fluxtube



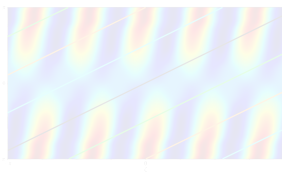
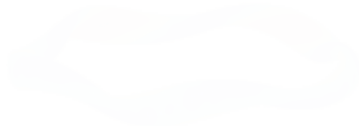
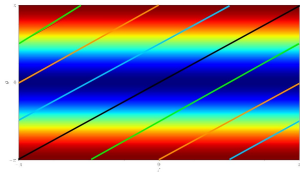
Expected Growth Rate; Full-Flux vs. Fluxtube



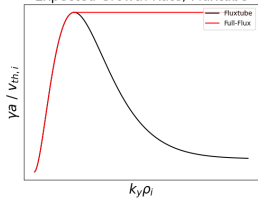
How 3D geometry modifies expectations



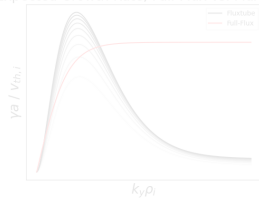
$N_x = 4$



Expected Growth Rate; Fluxtube



Expected Growth Rate; Full-Flux vs. Fluxtube



How 3D geometry modifies expectations

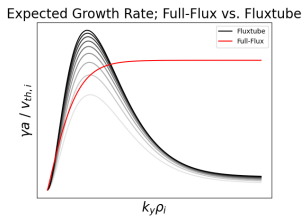
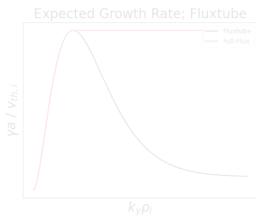
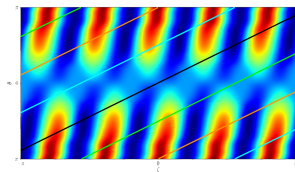
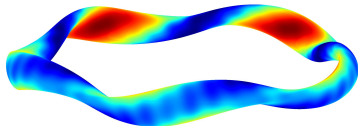
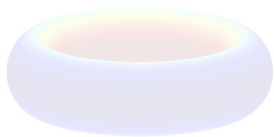


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Algorithm

- ▶ Use operator splitting to solve normalised GK equation:

Algorithm

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$$\frac{\partial g_\nu}{\partial t} + \underbrace{\mathcal{S}_\nu[g_\nu, \varphi_\nu] + \mathcal{M}_\nu[g_\nu]}_{\text{Implicit}} + \underbrace{\mathcal{D}_\nu[g_\nu, \varphi_\nu] + \mathcal{G}_\nu[\varphi_\nu] + \mathcal{N}_\nu[g_\nu, \varphi_\nu]}_{\text{Explicit}} = \mathcal{C}_\nu[\{g_{\nu'}\}, \{\varphi_{\nu'}\}], \quad (3)$$

$$\partial_t g_\nu = \sum_{i=1}^3 (\partial_t g_\nu)_i \quad \left| \quad \begin{aligned} (\partial_t g_\nu)_1 + \mathcal{D}_\nu[g_\nu, \varphi_\nu] + \mathcal{G}_\nu[\varphi_\nu] + \mathcal{N}_\nu[g_\nu, \varphi_\nu] &= 0 \\ (\partial_t g_\nu)_2 + \mathcal{M}_\nu[g_\nu] &= 0 \\ (\partial_t g_\nu)_3 + \mathcal{S}_\nu[g_\nu, \varphi_\nu] &= 0 \end{aligned} \right.$$

Algorithm

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streaming mirror
drifts
non-linear
collisions

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- Geometric coefficients introduce coupling between different k_α . For example, the gyroaverage $\varphi_\nu = \langle \phi \rangle_{\mathbf{R}_\nu}$

$$\begin{array}{l} \text{Flux tube:} \\ \hat{\phi}_{\mathbf{k}, \nu} = J_{0, (k_\psi, k_\alpha), \nu} \phi(k_\psi, k_\alpha) \end{array} \quad \left| \quad \begin{array}{l} \text{Full flux annulus: } * \\ \hat{\phi}_{\mathbf{k}, \nu} = \sum_{k'_\alpha} \underbrace{\hat{J}_{(k_\psi, k_\alpha - k'_\alpha), k'_\alpha, \nu}}_{\text{matrix}} \hat{\phi}(k_\psi, k_\alpha - k'_\alpha), \end{array} \right.$$

- Compute Fourier coefficients, $\hat{J}_{\mathbf{k}'', k'_\alpha, \nu}$, of $J_{0, (k_\psi, k_\alpha), \nu}$ once at the beginning of simulation for computational efficiency.

Implicit treatment

- ▶ `stella` is a fast GK code

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- ▶ Electron dynamics imposes stringent CFL condition on time step \rightarrow treat parallel streaming and mirror terms implicitly

Implicit treatment

- ▶ `stella` is a fast GK code
- ▶ Electron dynamics imposes stringent CFL condition on time step \rightarrow treat parallel streaming and mirror terms implicitly
- ▶ However, geometric-dependent coefficients add inhomogeneous α -dependence

$$\frac{\partial g_\nu}{\partial t} = - \underbrace{v_{\parallel} \hat{\mathbf{b}} \cdot \nabla_z}_{\alpha\text{-dependent}} \underbrace{\left(\frac{\partial g_\nu}{\partial z} + \frac{Z_\nu e}{T_\nu} \frac{\partial \varphi_s}{\partial z} F_{0,\nu} \right)}_{\alpha\text{-dependent}}. \quad (4)$$

Implicit treatment

- ▶ **stella** is a fast GK code
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- ▶ Here $\overline{\hat{\mathbf{b}} \cdot \nabla z} \doteq \frac{1}{2\pi} \int_0^{2\pi} d\alpha \left(\frac{1}{2\pi} \int_{\zeta_{\min}}^{\zeta_{\max}} \frac{d\zeta'}{\hat{\mathbf{b}} \cdot \nabla \zeta'} \right)^{-1}$ is an average over fieldlines
- ▶ $\bar{J} = \hat{J}_{(k_\psi, 0), k_\alpha}$ is the constant-in-alpha component of the Bessel function for a given k_α
- ▶ $\bar{\phi}$ is an artificial field that solves a modified quasineutrality condition (i.e. $\bar{\phi}$ is a contribution to ϕ that is treated implicitly) *

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 & - \underbrace{v_{\parallel} \left(\hat{\mathbf{b}} \cdot \nabla z - \overline{\hat{\mathbf{b}} \cdot \nabla z} \right) \left(\frac{\partial g_\nu}{\partial z} + \frac{Z_\nu e}{T_\nu} \frac{\partial \varphi_\nu}{\partial z} F_{0,\nu} \right)}_{\text{Explicit}}
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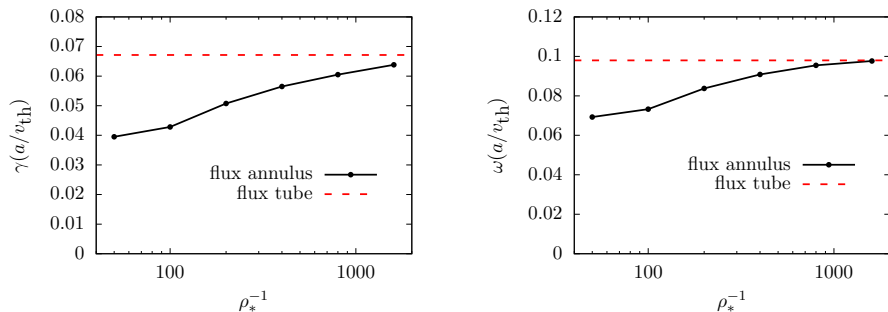
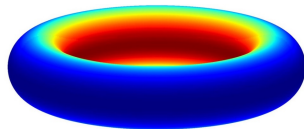


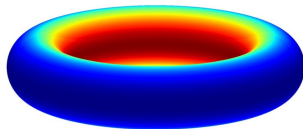
Figure 1: ρ_* scans in CBC with adiabatic electrons

Simulation results: CBC, adiabatic electrons



- ▶ Comparing code with axisymmetric geometry
- ▶ Use modified Boltzmann response $\delta n_e = \frac{en_e}{T_e} (\phi - \langle \phi \rangle_{\text{FSA}})$, where $\langle \phi \rangle_{\text{FSA}}$ is the flux-surface-averaged ϕ

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Linear simulations

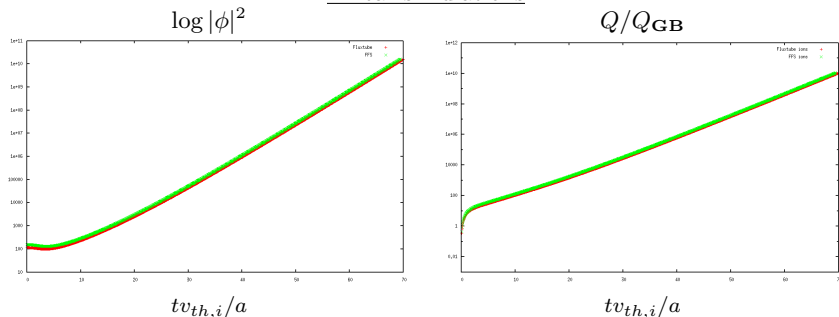
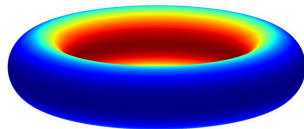


Figure 2: Linear simulations for CBC with modified electron response; $N_y = N_x = 30$, $\rho_* = 0.025$

Simulation results: CBC, adiabatic electrons



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Non-linear simulations

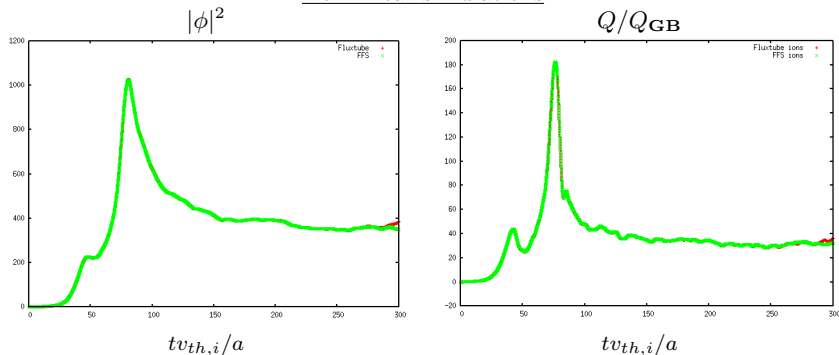
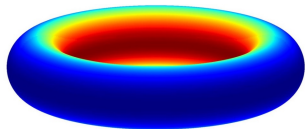


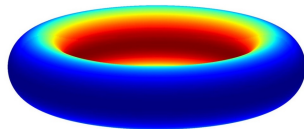
Figure 2: Non-linear simulations for CBC; $N_y = N_x = 30$, $\rho_* = 0.025$

Simulation results: CBC, kinetic electrons

- ▶ Add in kinetic electrons



Simulation results: CBC, kinetic electrons



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Linear simulations

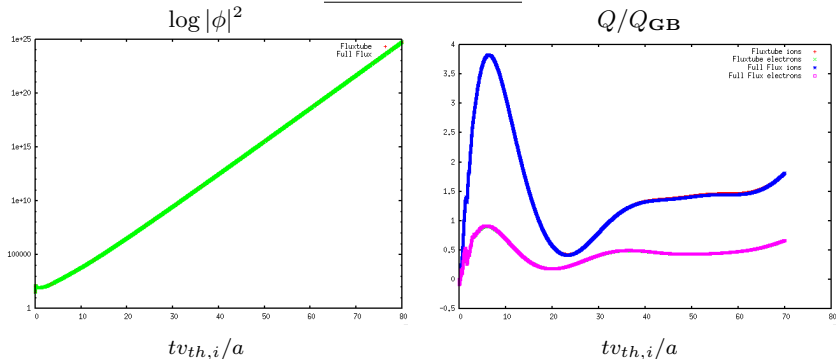
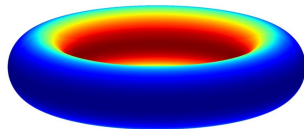


Figure 3: Linear simulations for CBC with kinetic electrons; $N_y = N_x = 30$, $\rho_* = 0.025$

Simulation results: CBC, kinetic electrons



- ▶ Add in kinetic electrons

Non-linear simulations

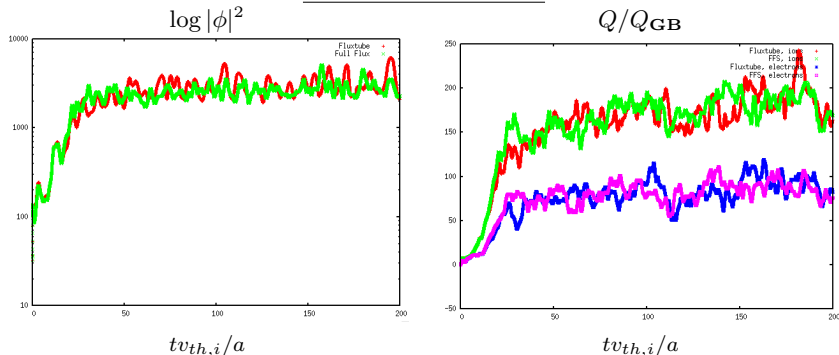
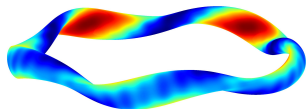
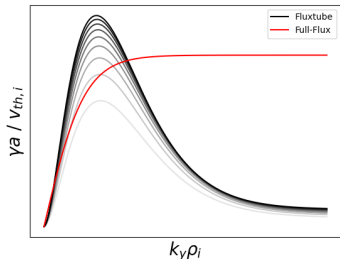


Figure 3: Non-linear simulations for CBC with kinetic electrons; $N_y = 30$, $N_x = 150$, $\rho_* = 0.025$

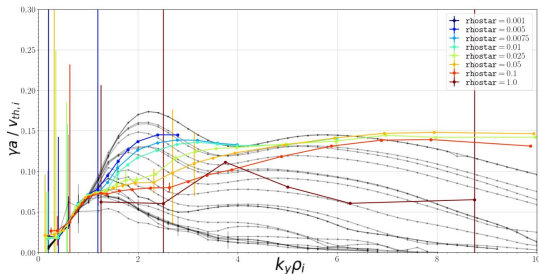
Expectations and results



- ▶ Anticipate that including higher k_α leads to a global growth rate
- ▶ Growth rate should be some average of the most unstable mode across all field lines

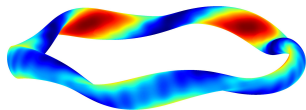


Expectation



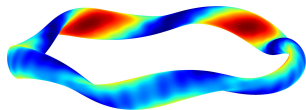
Simulation results

Simulation results: W7-X



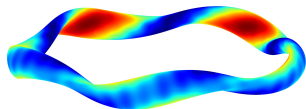
- ▶ Impose that each field line in FFS has the same geometry to benchmark algorithm

Simulation results: W7-X



- ▶ Impose that each field line in FFS has the same geometry to benchmark algorithm





- ▶ Impose that each field line in FFS has the same geometry to benchmark algorithm
- ▶ Modified adiabatic electrons

Linear simulations

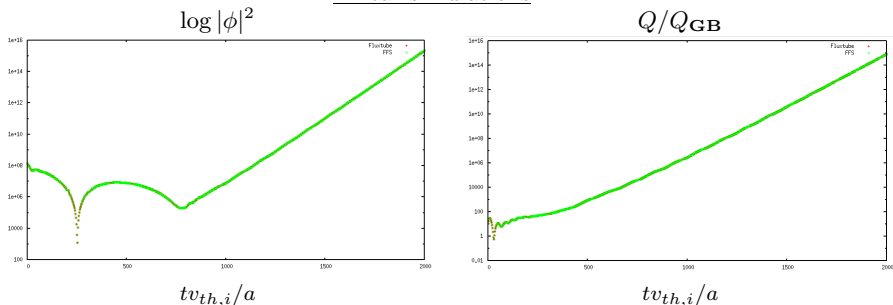
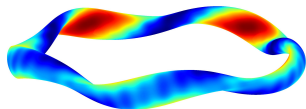


Figure 4: Linear simulations for W7-X geometry with modified adiabatic electrons testing algorithm; $N_y = N_x = 72$, $\rho_* = 0.01$



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- ▶ Modified adiabatic electrons

Non-linear simulations

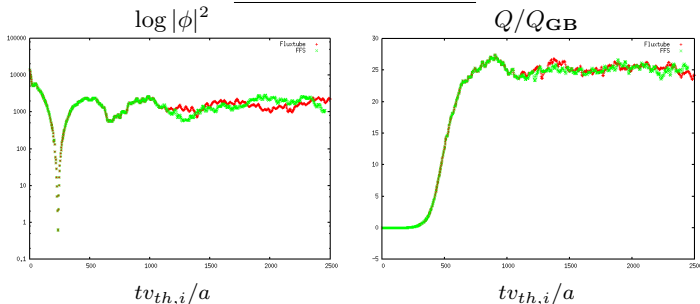
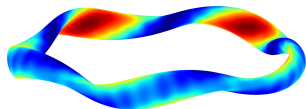


Figure 4: Non-linear simulations for W7-X geometry with modified adiabatic electrons; $N_y = N_x = 30$, $\rho_* = 0.025$

Simulation results: W7-X



- ▶ Impose that each field line in FFS has the same geometry to benchmark algorithm
- ▶ Add in kinetic electrons

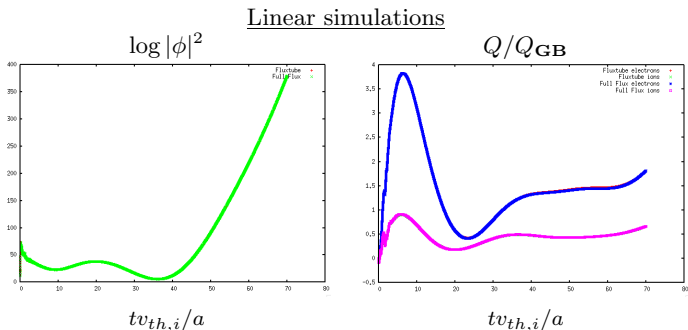
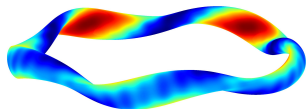


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Simulation results: W7-X



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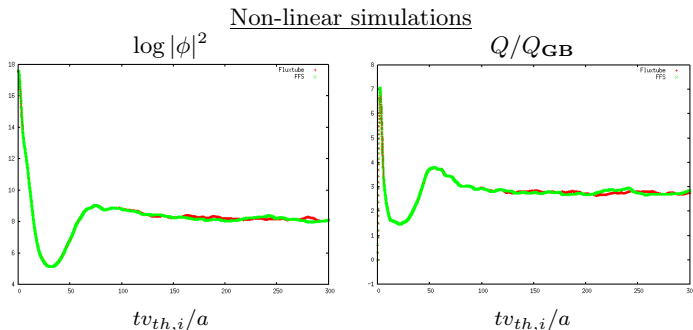
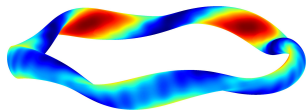


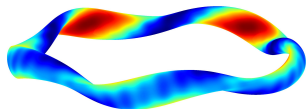
Figure 4: Non-linear simulations for W7-X geometry with kinetic electrons;
 $N_y = N_x = 64$, $\rho_* = 0.05333$

Simulation results: W7-X geometric variation



- ▶ How does geometric variation modify simulation results?

Simulation results: W7-X geometric variation



- ▶ How does geometric variation modify simulation results?

Linear simulations

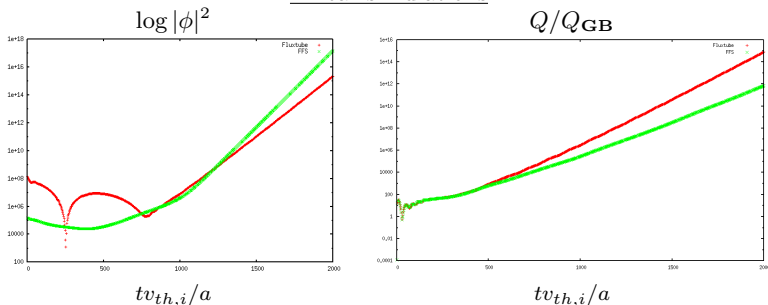
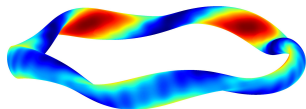


Figure 5: Linear simulations for W7-X geometry with modified adiabatic electrons including full flux effects; $N_y = N_x = 72$, $\rho_* = 0.01$

Simulation results: W7-X geometric variation



- How does geometric variation modify simulation results?

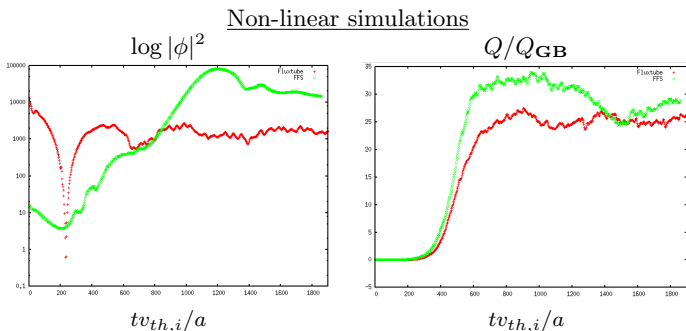


Figure 5: Non-linear simulations for W7-X geometry with modified adiabatic electrons
 $N_y = N_x = 72$, $\rho_* = 0.01$

Simulation results: code efficiency

Implicit vs. explicit

- ▶ A time-step of $1\text{E-}006$ is needed to run explicit kinetic electron simulations for W7-X \rightarrow still numerically unstable
- ▶ Implicit treatment of parallel streaming allows for time-step of $5\text{E-}002$

Simulation results: code efficiency

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Flux tube vs. full flux annulus

- ▶ Currently full-flux code takes $\sim \times 4/5$ longer to run compared with flux tube simulations
- ▶ Non-linear simulations with adiabatic electrons:

Flux tube	Full flux algorithm	Full flux with geometric variation
218.03 min	562.15 min	794.66 min
$\times 1$	$\times 2.6$	$\times 3.7$

- ▶ Like-for-like resolutions: 12 nodes, 576 cores, 2000 normalised times steps
- ▶ Anticipate with optimisation this can be reduced to $\sim \times 3$

Summary and future work

Summary

- ▶ There is a need in the community to accurately simulate turbulence on an entire flux surface for non-axisymmetric devices
- ▶ We have developed an algorithm to deal with full-flux effects in arbitrary geometry
- ▶ We are getting some promising results
- ▶ There is still work to be done
- ▶ The code is currently being checked, and optimised

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Future Work

- ▶ Finish off FFS code, and benchmark with other GK codes
- ▶ Investigate if/how zonal flows are supported in stellarators

Backup slides: Derivation of twist-and-shift boundary conditions

*

$$A(t, x, y, z) = \sum_k \hat{A}_{k_x, k_y}(t, z) e^{ik_y(y-y_0)+ik_x(x-x_0)} \quad (5)$$

Set $y_0 = 0$, $x_0 = 0$ $A(t, x, y(x, \theta, z), z) = A(t, x, y'(\theta, z + 2p\pi), z + 2p\pi)$

But $y = y(\theta, z)$

$$\sum_k \hat{A}_{k_x, k_y}(t, z) e^{ik_y y + ik_x x} = \sum_k \hat{A}_{k_x, k_y}(t, z') e^{ik_y (y'(\theta, z')) + ik_x x} \quad (6)$$

So $y'(\theta, z') = y + \frac{\partial y}{\partial z} 2\pi p = y + 2\pi p \frac{\partial y}{\partial \alpha} \frac{\partial \alpha}{\partial z} = y - 2\pi p \iota(\psi) \frac{\partial y}{\partial \alpha}$ Remembering
 $\iota(\psi) = \iota(\psi_0) + \iota' \frac{\partial \psi}{\partial x}$ so $y' = y - 2\pi p \iota(\psi_0) \frac{\partial y}{\partial \alpha} - 2(x - x_0) \pi p \iota' \frac{\partial y}{\partial \alpha} \frac{\partial \psi}{\partial x}$

$$\sum_k \hat{A}_{k_x, k_y}(t, z) e^{ik_y y + ik_x x} = \sum_k \hat{A}_{k_x, k_y}(t, z + 2\pi p) e^{ik_y y + i(k_x - 2\pi p \iota' \frac{\partial y}{\partial \alpha} \frac{\partial \psi}{\partial x} k_y) x' - i 2\pi p k_y \iota p \frac{\partial y}{\partial \alpha}} \quad (7)$$

Let $\delta k_x = 2\pi p \iota' \frac{\partial y}{\partial \alpha} \frac{\partial \psi}{\partial x} k_y$ and $\Delta = -2\pi p k_y \iota \frac{\partial y}{\partial \alpha}$

$$\sum_k \hat{A}_{k_x, k_y}(t, z) e^{ik_y y + ik_x x} = \sum_k \hat{A}_{k_x, k_y}(t, z + 2\pi p) e^{ik_y y + i(k_x - \delta k_x) x'} e^{i\Delta} \quad (8)$$

So relate $k_x = k'_x - 2\pi p \iota' \frac{\partial y}{\partial \alpha} \frac{\partial \psi}{\partial x} k_y$

Backup slides: Response matrix

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$$\phi^{n+1} = \left[\sum_{\nu} \frac{Z_{\nu}^2 n_{\nu}}{T_{\nu}} (1 - \Gamma_{0,\nu}) \right]^{-1} \sum_{\nu} Z_{\nu} n_{\nu} \frac{2B}{\pi^{1/2}} \int_{-\infty}^{\infty} dv_{\parallel} \int_0^{\infty} d_{\mu} J_{0,\nu} g_{\nu}^{n+1} \quad (9)$$

Let $g^{n+1} = g_{\text{hom}}^{n+1} + g_{\text{inhom}}^{n+1}$

$$\frac{g_{\text{inhom}}^{n+1} - g^n}{\Delta t} = -v_{\parallel} \hat{\mathbf{b}} \cdot \nabla z \left(\frac{\partial g_{\text{inhom}}^{n+1}}{\partial z} + \frac{Z_{\nu}}{T_{\nu}} \frac{\partial J_0 \phi^n}{\partial z} F_{0,\nu} \right) \quad (10)$$

$$\frac{g_{\text{hom}}^{n+1} - g^n}{\Delta t} = -v_{\parallel} \hat{\mathbf{b}} \cdot \nabla z \left(\frac{\partial g_{\text{hom}}^{n+1}}{\partial z} + \frac{Z_{\nu}}{T_{\nu}} \frac{\partial J_0 \phi^{n+1}}{\partial z} F_{0,\nu} \right) \quad (11)$$

Then

$$g^{n+1} = \sum \frac{\delta g_{\text{hom}}}{\delta \phi} \phi^{n+1} + g_{\text{inhom}}^{n+1} \quad (12)$$

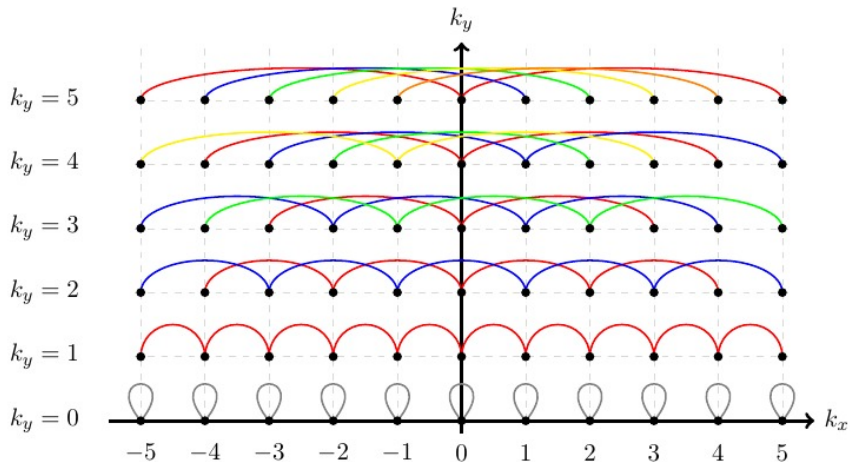
Substitute into quasineutrality equation and solve for ϕ^{n+1}

$$\left[I - Q \sum \frac{\delta g_{\text{hom}}}{\delta \phi} \right] \phi^{n+1} = \phi_{\text{inhom}}^{n+1} \quad (13)$$

With I the identity, $Q = \sum_{\nu} Z_{\nu} n_{\nu} \frac{2B}{\pi^{1/2}} \int_{-\infty}^{\infty} dv_{\parallel} \int_0^{\infty} d_{\mu} J_{0,\nu}$, and $\phi_{\text{inhom}}^{n+1} = Q g_{\text{inhom}}^{n+1}$

Backup slides: Eigenmode chains

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Backup slides: Bessel functions

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Explicitly expanding the gyroaveraged electrostatic potential in Fourier harmonics:

$$\varphi_\nu = \sum_{\mathbf{k}''} e^{i\mathbf{k}'' \cdot \mathbf{R}} J_0(a_{\mathbf{k}'', \nu}) \hat{\phi}_{\mathbf{k}''}, \quad (14)$$

with

$$a_{\mathbf{k}'', \nu} = \frac{ck''_\perp(\alpha, z)}{Z_\nu e} \sqrt{\frac{2m_\nu \mu}{B(\alpha, z)}}. \quad (15)$$

Both k_α and α appear. For axisymmetric systems, the α dependence is absent and so gyro-averaging is a local operation in k_α -space. Now there is coupling between modes with different k_α . Expanding the Bessel function:

$$\hat{\varphi}_{\mathbf{k}, \nu} = \int d^2\mathbf{R} \sum_{\mathbf{k}'', k'_\alpha} e^{i(k''_\psi - k_\psi)\psi} e^{i(k'_\alpha + k''_\alpha - k_\alpha)\alpha} \hat{J}_{\mathbf{k}'', k'_\alpha, \nu} \hat{\phi}_{\mathbf{k}''}, \quad (16)$$

where we have used

$$J_0(a_{\mathbf{k}'', \nu}) = \sum_{k'_\alpha} \hat{J}_{\mathbf{k}'', k'_\alpha, \nu}(z, \mu) e^{ik'_\alpha \alpha}. \quad (17)$$

Making use of the orthogonality of the Fourier harmonics:

$$\hat{\varphi}_{\mathbf{k}, \nu} = \sum_{k'_\alpha} \hat{J}_{(k_\psi, k_\alpha - k'_\alpha), k'_\alpha, \nu} \hat{\phi}_{(k_\psi, k_\alpha - k'_\alpha)}. \quad (18)$$

Backup slides: $\bar{\phi}$ equation

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- ▶ If we let $Q = J_0(k_\perp)B(\alpha)$ and Fourier decompose we get:

$$Q = \sum_{k'_\alpha} \hat{Q}_{k_\alpha, k'_\alpha} e^{ik'_\alpha y} \quad (19)$$

- ▶ Define \bar{Q} to be the $k'_\alpha = 0$ component of this
- ▶ Take a similar approach for $\Delta(k_\perp) \doteq \sum_\nu \frac{Z_\nu^2 n_\nu}{T_\nu} (1 - \Gamma_{0, \mathbf{k}})$

$$\Delta = \sum_{k'_\alpha} \hat{\Delta}_{k_\alpha, k'_\alpha} e^{ik'_\alpha y} \quad (20)$$

- ▶ $\bar{\Delta}$ being the $k'_\alpha = 0$ component
- ▶ Putting everything together we get the equation for $\bar{\phi}$

$$\bar{\Delta}_{\mathbf{k}} \bar{\phi}_{\mathbf{k}} = \sum_\nu Z_\nu n_\nu \int dv_\parallel \int d\mu \bar{Q}_{\mathbf{k}} g_{\mathbf{k}} \quad (21)$$