



Toroidal plasma response modeling for ELM control optimization via RMPs in perspective DTT plasmas

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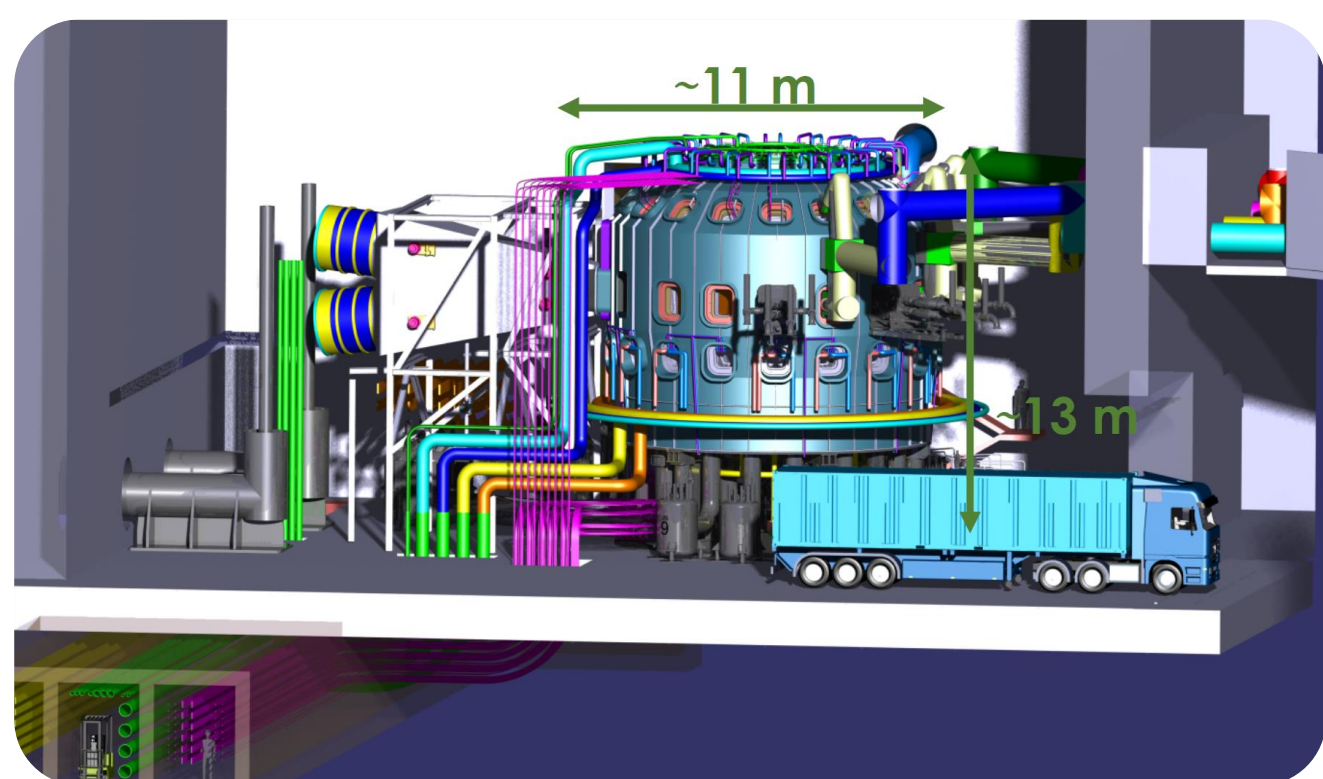
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Type-I Edge Localized Modes (ELMs) are strong bursts that eject particles and energy from the plasma

- ELM behavior is correlated to peeling-ballooning stability and can be therefore modified with external magnetic perturbations [1-3] often referred to as Resonant Magnetic Perturbations (RMPs)

The Divertor Tokamak Test (DTT) facility is a large superconducting tokamak conceived to develop power exhaust solutions in view of DEMO [4,5]

- ELM control is a task of particular importance for DTT operations



$B_t = 6 \text{ T}$
 $I_p = 5.5 \text{ MA}$

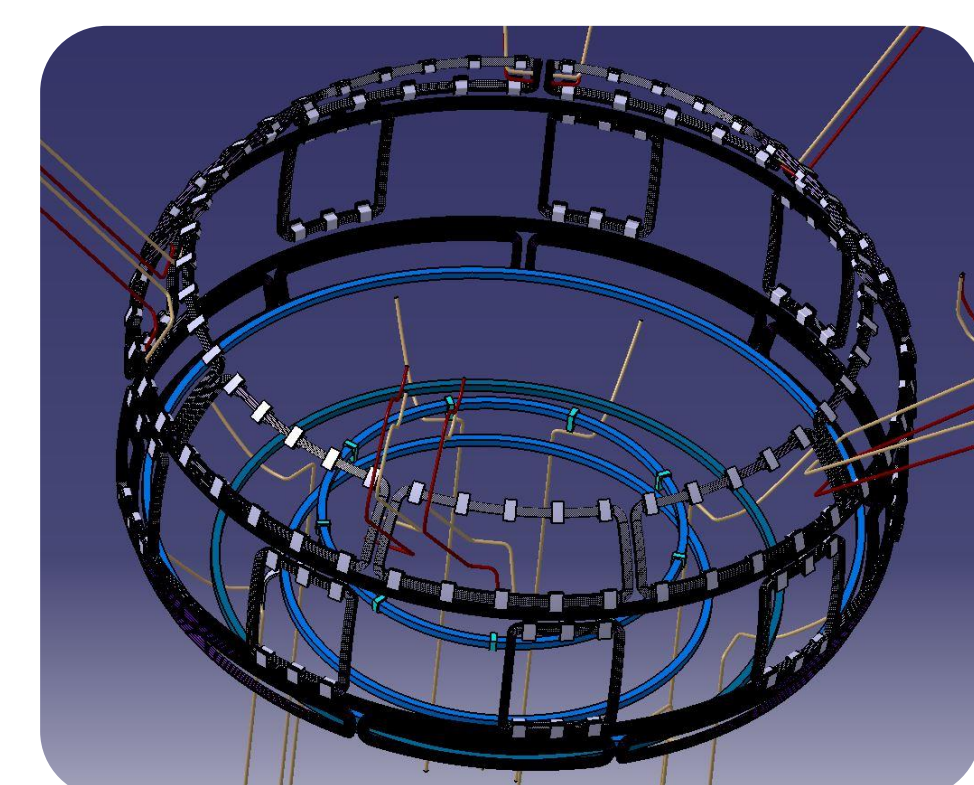
- Integration of exhaust with core performance in DEMO relevant conditions
- Joint European collaboration according to EUROfusion roadmap

A system of non-axisymmetric coils is being designed for the purpose of ELM and Error Field control on DTT

Linear resistive plasma response calculations with MARS-F [6] are used for a first assessment of the RMP requirements for ELM mitigation or suppression.

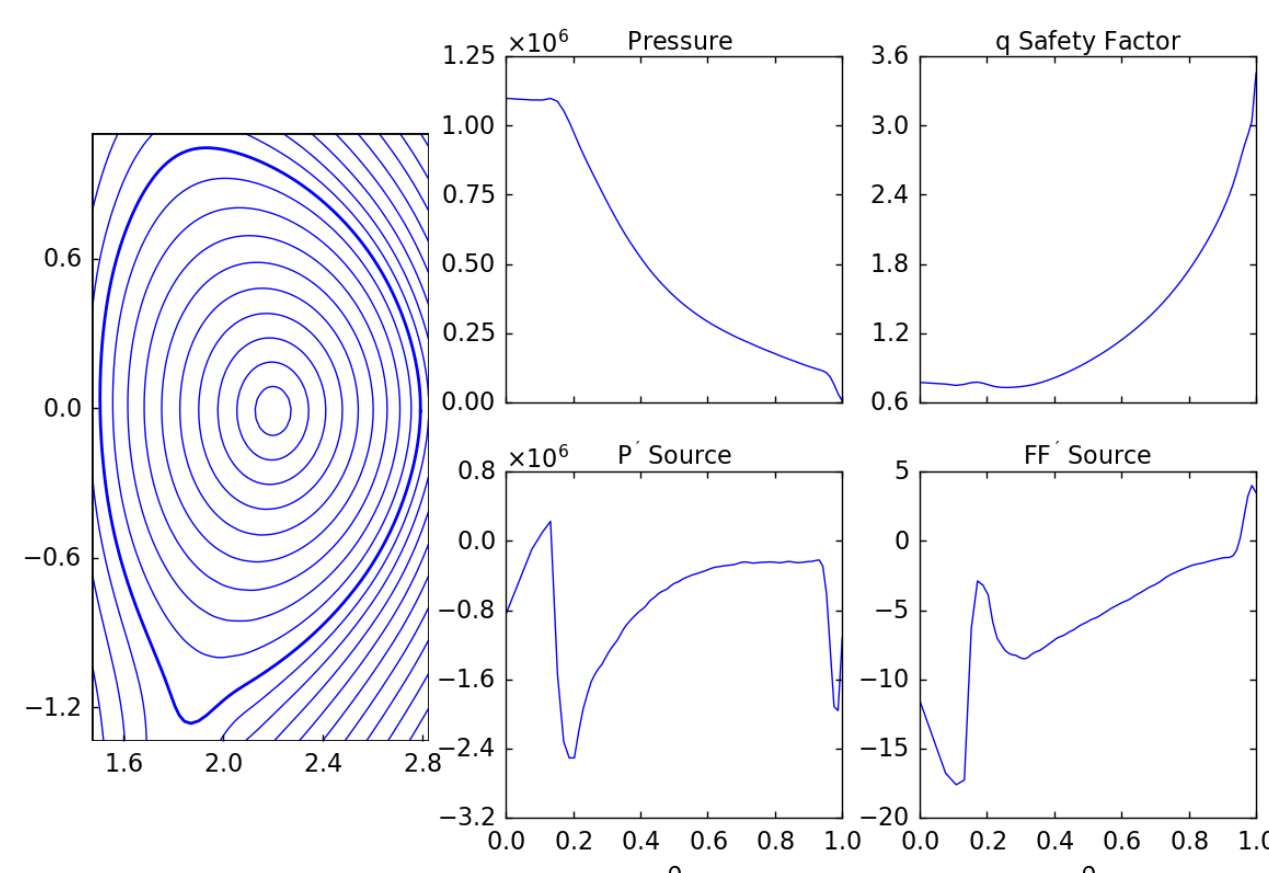
Different coil combinations and metrics are applied:

- Two rows off-midplane coils + equatorial array with half toroidal width
- X-point plasma displacement linked to ELM mitigation by empirical evidence
- Chirikov parameter expressing magnetic field line stochasticization



Realistic equilibrium for DTT full power phase [7] with consistent toroidal flow

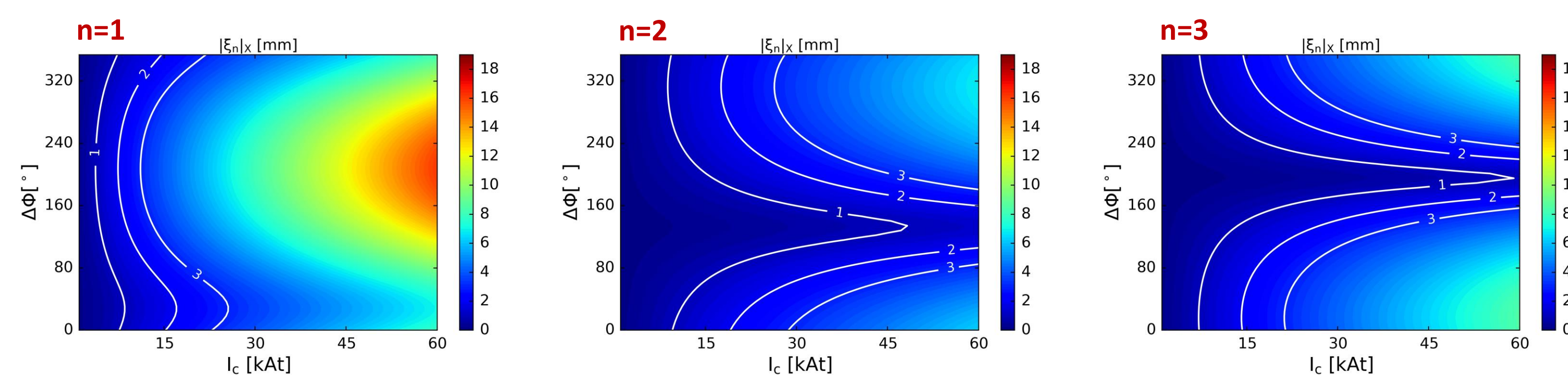
- Proper calculation of resistive response



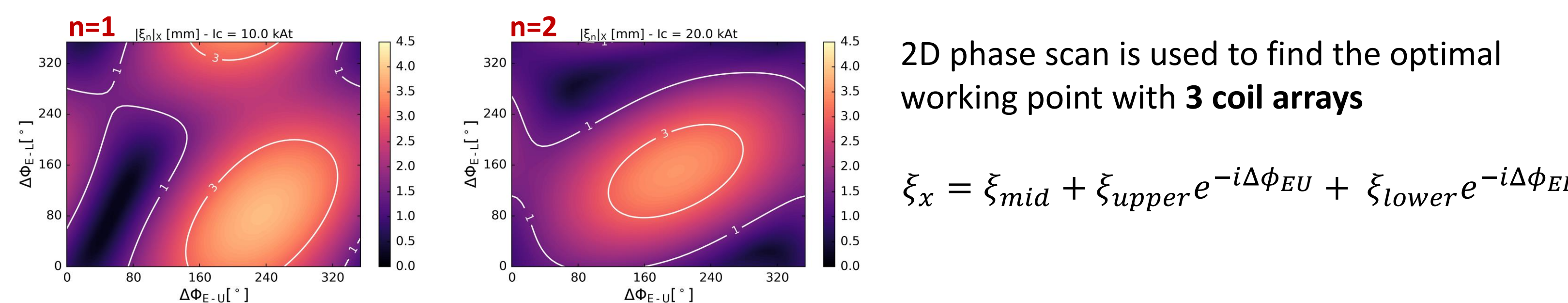
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DC magnetic field perturbations are applied with varying toroidal mode number $n=1,2,3$

Two rows of in-vessel coils can yield $\xi_{n,X} \sim 3 \text{ mm}$ with coil currents ranging from 15 kAt to 30 kAt depending on the toroidal mode number

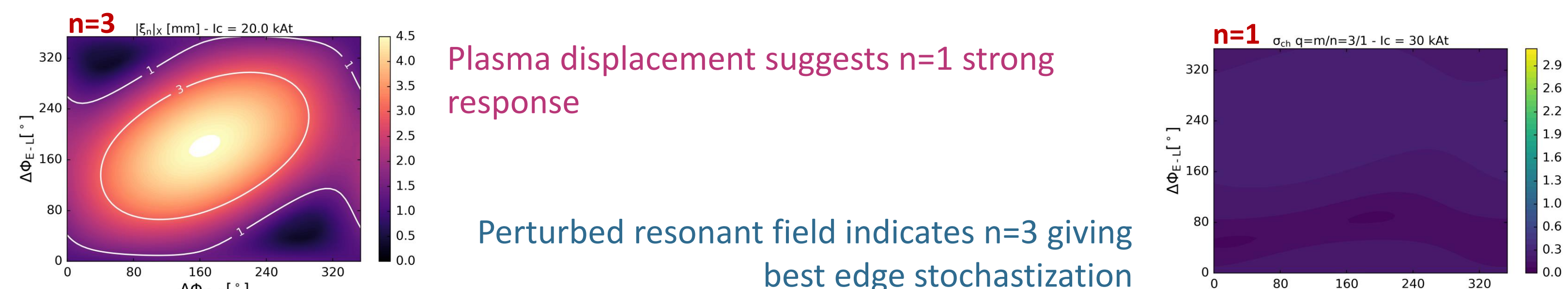


- Note $n=1$ perturbations trigger important core response as well as edge peeling response



2D phase scan is used to find the optimal working point with 3 coil arrays

$$\xi_X = \xi_{mid} + \xi_{upper} e^{-i\Delta\phi_{EU}} + \xi_{lower} e^{-i\Delta\phi_{EL}}$$



Plasma displacement suggests $n=1$ strong response

Perturbed resonant field indicates $n=3$ giving best edge stochasticization

Chirikov parameter maps on last rational surface

$$B_{mn} = B_{mn}^M + B_{mn}^U e^{-i\Delta\phi_{EU}} + B_{mn}^L e^{-i\Delta\phi_{EL}}$$

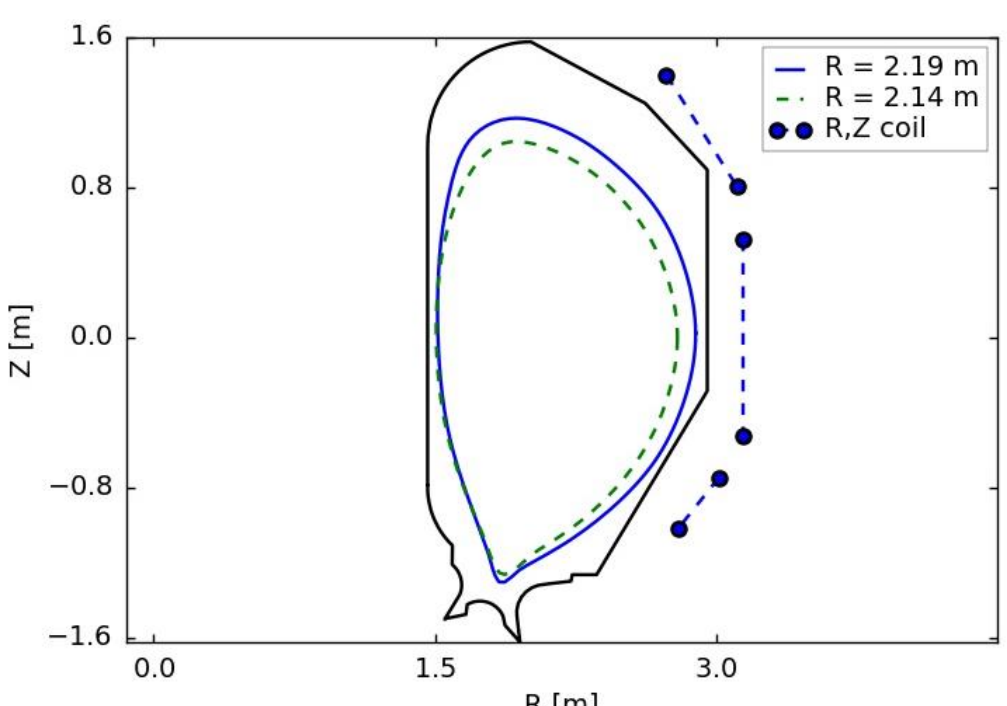
- Toroidal plasma response modeling can provide useful insight into ELM mitigation with RMPs during DTT operations.
- Equatorial array of coils provides significant contribution in reducing the coil current to reach selected thresholds, resulting in $\sim 10 \text{ kAt}$ for $n=1$ and $\sim 20 \text{ kAt}$ for $n=2,3$.
- Using the Chirikov parameter metric, only $n=3$ perturbations with $I_c \sim 30 \text{ kAt}$ satisfy the $\sigma_{chir} > 1$ threshold

$$(\gamma + i n \Omega) \xi = \mathbf{v} + (\xi \cdot \nabla \Omega) R^2 \nabla \Phi$$

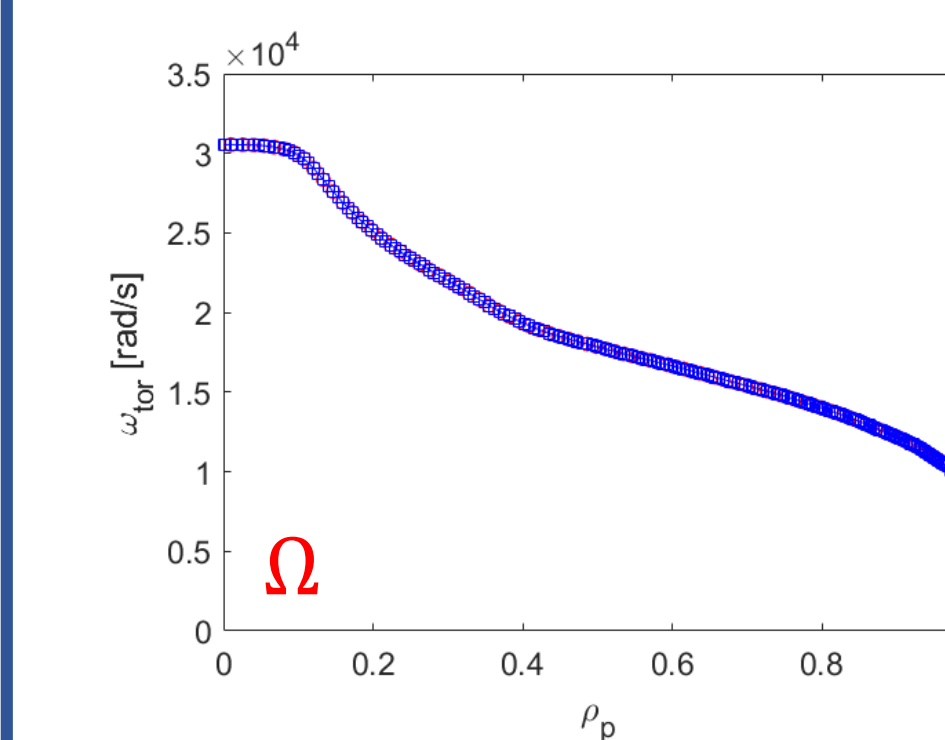
$$\rho(\gamma + i n \Omega) \mathbf{v} = -\nabla p + \mathbf{j} \times \mathbf{B} + \mathbf{J} \times \mathbf{b} - \rho[2\Omega \hat{\mathbf{z}} \times \mathbf{v} + (\mathbf{v} \cdot \nabla \Omega) R^2 \nabla \Phi] - \nabla \cdot \Pi$$

$$(\gamma + i n \Omega) \mathbf{b} = \nabla \times (\mathbf{v} \times \mathbf{B}) + (\mathbf{b} \cdot \nabla \Omega) R^2 \nabla \Phi - \nabla \times \eta \mathbf{j}$$

$$(\gamma + i n \Omega) p = -\mathbf{v} \cdot \nabla p - \Gamma p \nabla \cdot \mathbf{v}$$



$$\mathbf{j} = \nabla \times \mathbf{b}$$

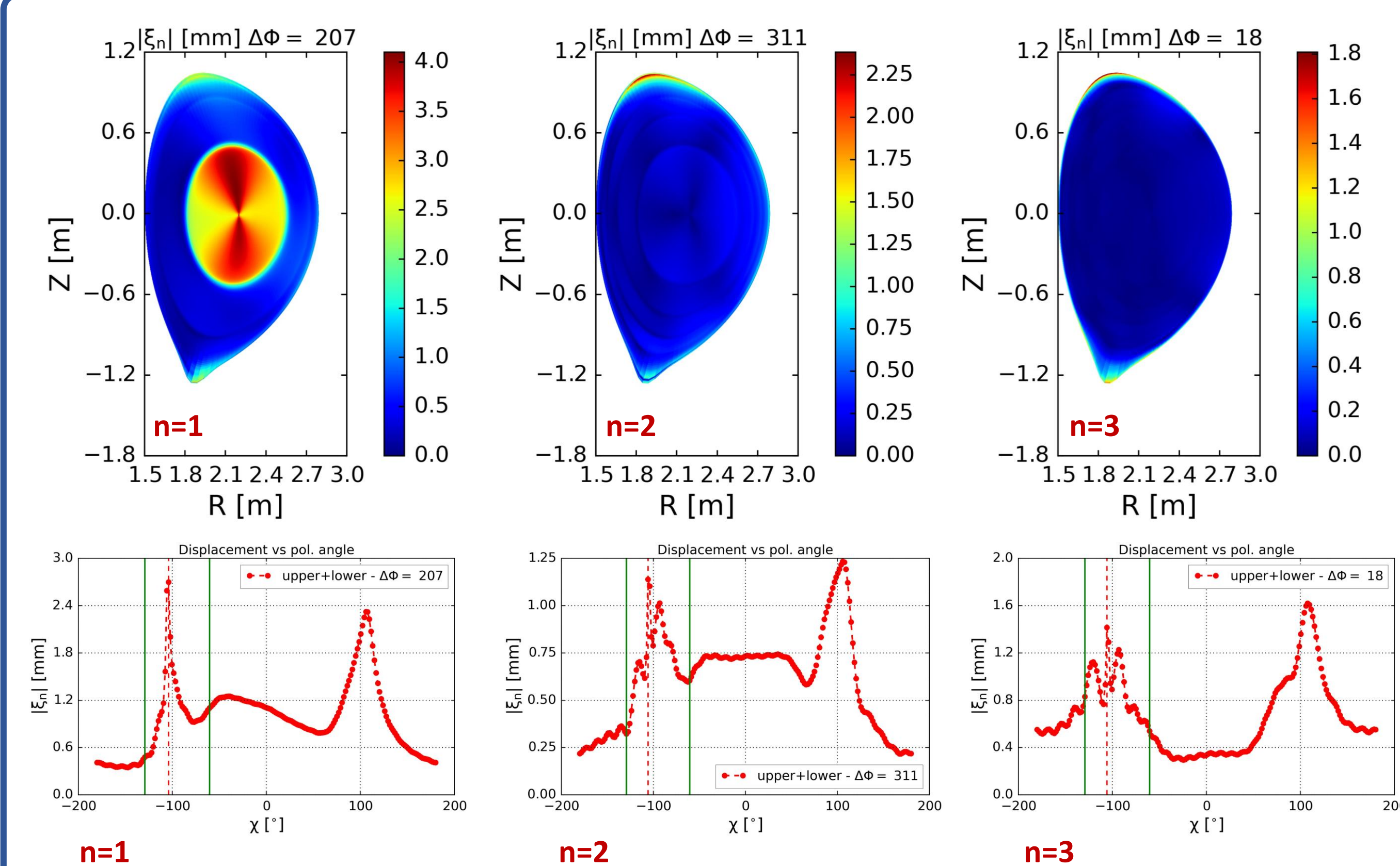


Normal displacement near the x-point region [8,9]

$$\xi_X$$

Chirikov parameter calculated with resonant radial field components in PEST-like straight field line coordinates [10]

$$\sigma = 4 \sqrt{\left| \frac{n Q dq}{\psi' ds} \right|} > 1 \quad Q = \left(\frac{\mathbf{b} \cdot \nabla \psi_p}{\mathbf{B}_{eq} \cdot \nabla \Phi} \right)_{mn}$$



Notes and outlook:

- X-point displacement results can be affected by the edge safety factor
- Non-linear damping of plasma flow or poloidal rotation have not been considered
- Torque-based metrics can be added for a complete picture



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