



Jet Pull:
Resummation for the Pull Magnitude and Beyond

Chang Wu*

Dipartimento di Fisica
Universit'a di Genova and INFN, Sezione di Genova,

HARPS Meeting
31th Oct, 2018

With: Simone Marzani †
Andrew Larkoski ‡

In Preparation:
Theory Predictions for Pull
[arXiv:18xx.xxxx]
To appear soon... hopefully!

* <mailto:cwu@ge.infn.it>

† <mailto:simone.marzani@ge.infn.it>

‡ <mailto:larkoski@reed.edu>

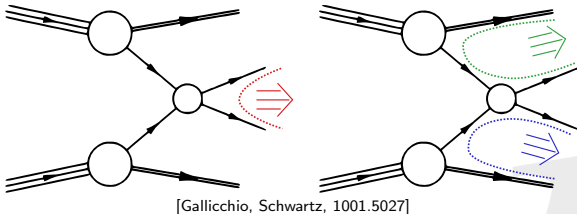
- 1 *Introduction and Motivation*
 - colour flow
 - definition of pull
- 2 *Fixed Order Calculation*
 - set up for the calculation
 - leading order result
 - check with EVENT2
- 3 *NLL Resummation for the Magnitude of Pull*
 - resummation formalism
 - fixed-order vs resummation
 - improvement for the fixed-order results
- 4 *Beyond the Magnitude*



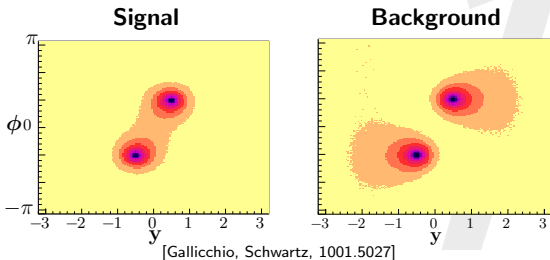
Precision era of Higgs Physics

- ▶ With the high accuracy data from the LHC Run-2, entering a precision era
- ▶ The main higgs decay channel: $H \rightarrow b\bar{b}$, branching ratio about 58%
- ▶ Recently CMS and ATLAS have just reported the first direct measurements of Higgs decay to bottom quarks
- ▶ Need to separate the signal ($H \rightarrow b\bar{b}$) from background ($g \rightarrow b\bar{b}$)

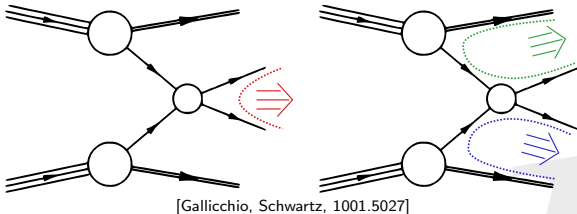
- ▶ difference between colour singlet (signal) and colour octet (background)



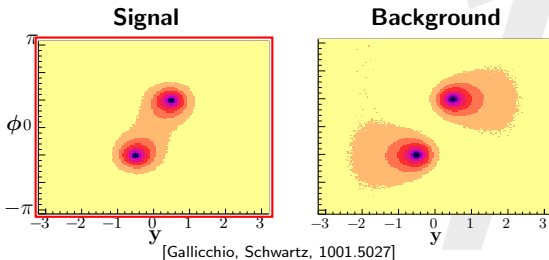
- ▶ From MC shower picture: (signal) radiation pulled toward each other



- ▶ difference between colour singlet (signal) and colour octet (background)

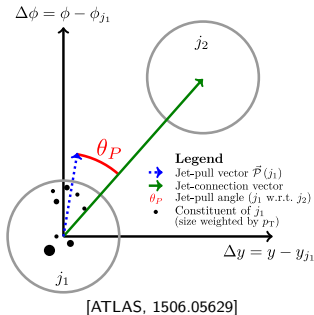


- ▶ From MC shower picture: (signal) radiation pulled toward each other



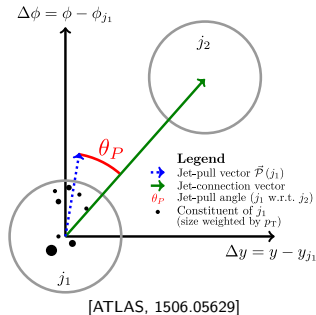
Definition of Pull

- ▶ Diagram for the construction of the jet pull:



Definition of Pull

- ▶ Diagram for the construction of the jet pull:



- ▶ Definition of pull: jet constituents with transverse momentum p_T^i and location \vec{r}_i

$$\vec{t} = \sum_{i \in \text{jet}} \frac{p_T^i |r_i|}{p_T^{\text{jet}}} \vec{r}_i$$

- ▶ Definition of pull: jet constituents with transverse momentum p_T^i and location \vec{r}_i

$$\vec{t} = \sum_{i \in \text{jet}} \frac{p_T^i |r_i|}{p_T^{\text{jet}}} \vec{r}_i$$



- ▶ Definition of pull: jet constituents with transverse momentum p_T^i and location \vec{r}_i

$$\vec{t} = \sum_{i \in \text{jet}} \frac{p_T^i |r_i|}{p_T^{\text{jet}}} \vec{r}_i$$

- ▶ Properties of pull:

- IRC safety: soft or collinear emissions don't change the hard jets

$$O(p_1 \dots p_i, p_j \dots p_n) \rightarrow O(p_1 \dots (p_i + p_j) \dots p_n), \text{ if } (p_i + p_j)^2 = 0$$

- Additive observable: separate the contributions from soft and collinear emissions
- Pull angle: IRC unsafe

$$\phi_p = \cos^{-1} \frac{t_x}{t}$$

Modification for Pull

- ▶ Modified version of the pull vector in $e_+ e_-$

$$\vec{t}_{modified} = \sum_{i \in jet} \frac{E_i \sin^2 \theta_i}{E_J} (\cos \phi_i, \sin \phi_i)$$

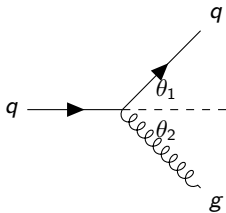


Modification for Pull

- ▶ Modified version of the pull vector in $e_+ e_-$

$$\vec{t}_{modified} = \sum_{i \in jet} \frac{E_i \sin^2 \theta_i}{E_J} (\cos \phi_i, \sin \phi_i)$$

- ▶ Example: LO (2 parton), collinear splitting



$$z \text{ particle: } \vec{t}_z = z \cdot (1 - z)^2 \theta^2 (\cos \phi, \sin \phi)$$

$$1 - z \text{ particle: } \vec{t}_{1-z} = (1 - z) \cdot z^2 \theta^2 (-\cos \phi, -\sin \phi)$$

$$\vec{t} = z(1 - z)(1 - 2z)\theta^2 (\cos \phi, \sin \phi)$$

Compare Pull Magnitude with Jet Mass

- ▶ Magnitude of pull:

$$t = z(1-z)(1-2z)\theta^2 \leq 0.1R^2$$

- ▶ Definition of jet mass:

$$\rho = \frac{m_J^2}{E_J^2} \sim z(1-z)\theta^2 \leq \frac{R^2}{4}$$

Compare Pull Magnitude with Jet Mass

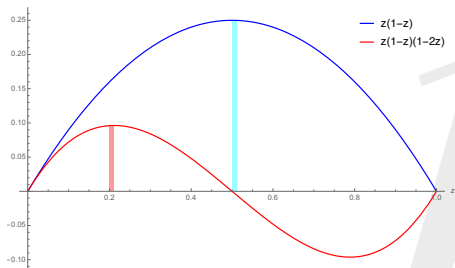
- ▶ Magnitude of pull:

$$t = z(1-z)(1-2z)\theta^2 \leq 0.1R^2$$

- ▶ Definition of jet mass:

$$\rho = \frac{m_J^2}{E_J^2} \sim z(1-z)\theta^2 \leq \frac{R^2}{4}$$

- ▶ End point:



EVENT2: $\rho_{max} = 0.431$, $t_{max} = 0.204$

Set Up For the Calculation

- ▶ Set up:

$$\frac{d^2\sigma}{d\vec{t}} = S(t, \phi_p, \mu) + J(t, \phi_p, \mu)$$

soft function:
eikonal factor

$$\mathcal{J}(q) = C_F \frac{2k_1 k_2}{(qk_1)(qk_2)}$$

jet function:
collinear splitting functions

$$P_{qq} = C_F \frac{1+(1-z)^2}{z}$$

- ▶ Double differential distribution

$$\frac{d^2\sigma}{dt d\phi_p} = \frac{\alpha_s C_F}{\pi^2 t} \left[\log \frac{4 \tan^2 \frac{R}{2}}{t} - \frac{3}{4} + 2 \cot \phi_p \tan^{-1} \frac{\frac{\tan \frac{R}{2}}{\tan \frac{\theta_{12}}{2}} \sin \phi_p}{1 - \frac{\tan \frac{R}{2}}{\tan \frac{\theta_{12}}{2}} \cos \phi_p} - \log \left(1 + \frac{\tan^2 \frac{R}{2}}{\tan^2 \frac{\theta_{12}}{2}} - 2 \frac{\tan \frac{R}{2}}{\tan \frac{\theta_{12}}{2}} \cos \phi_p \right) \right]$$

- ▶ Magnitude of pull

$$\frac{d\sigma}{dt} = \frac{\alpha_s C_F}{\pi t} \left[\log \frac{1}{t} - \frac{3}{4} - \log \left(\frac{1 - \frac{\tan^2 \frac{R}{2}}{\tan^2 \frac{\theta_{12}}{2}}}{4 \tan^2 \frac{R}{2}} \right) \right]$$

- ▶ Double differential distribution

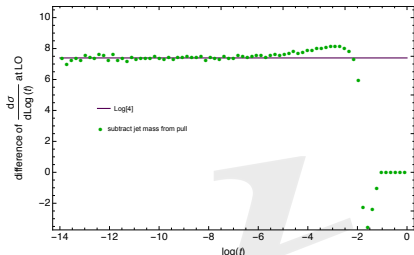
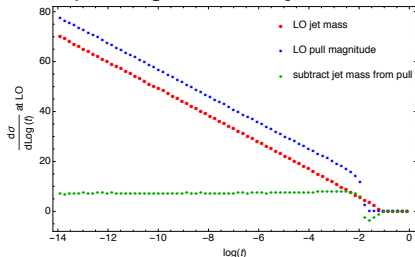
$$\frac{d^2\sigma}{dt d\phi_p} = \frac{\alpha_s C_F}{\pi^2 t} \left[\log \frac{4 \tan^2 \frac{R}{2}}{t} - \frac{3}{4} \right.$$

$$\left. + 2 \cot \phi_p \tan^{-1} \frac{\frac{\tan \frac{R}{2}}{\tan \frac{\theta_{12}}{2}} \sin \phi_p}{1 - \frac{\tan \frac{R}{2}}{\tan \frac{\theta_{12}}{2}} \cos \phi_p} - \log \left(1 + \frac{\tan^2 \frac{R}{2}}{\tan^2 \frac{\theta_{12}}{2}} - 2 \frac{\tan \frac{R}{2}}{\tan \frac{\theta_{12}}{2}} \cos \phi_p \right) \right]$$

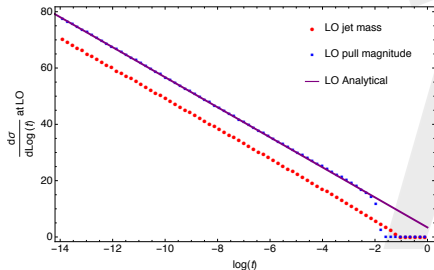
- ▶ Magnitude of pull

$$\frac{d\sigma}{dt} = \frac{\alpha_s C_F}{\pi t} \left[\log \frac{1}{t} - \frac{3}{4} - \log \left(\frac{1 - \frac{\tan^2 \frac{R}{2}}{\tan^2 \frac{\theta_{12}}{2}}}{4 \tan^2 \frac{R}{2}} \right) \right].$$

- ▶ Check pull magnitude with jet mass:



- ▶ Compare with fixed-order calculation:



- ▶ Q_T resummation formalism: (detail see: Giancarlo Ferrera' talk)

$$\frac{d^2\sigma}{d\vec{t}} = \sum_{n=0}^{\infty} \frac{1}{n!} \prod_{i=1}^n \int [dk_i] P(z_i) \delta^{(2)} \left(\vec{t} - \sum_{i=1}^n \vec{t}_i \right) \nu$$

$$\frac{d^2\sigma}{d\vec{t}} = \frac{1}{4\pi^2} \int d^2 \underline{b} e^{i\underline{b} \cdot \vec{t}} \exp \left[- \int [dk] P(z) \left(1 - e^{-i\underline{b} \cdot \vec{t}} \right) \right]$$

$$\equiv \frac{1}{4\pi^2} \int d^2 \underline{b} e^{i\underline{b} \cdot \vec{t}} e^{-R(b)}$$

$$\frac{d\sigma}{tdt} = \int_0^{\infty} b db J_0(bt) e^{-R(b)}$$

- ▶ Q_T resummation formalism: (detail see: Giancarlo Ferrera' talk)

$$\frac{d^2\sigma}{d\vec{t}} = \sum_{n=0}^{\infty} \frac{1}{n!} \prod_{i=1}^n \int [dk_i] P(z_i) \delta^{(2)} \left(\vec{t} - \sum_{i=1}^n \vec{t}_i \right) \mathcal{V}$$

$$\frac{d^2\sigma}{d\vec{t}} = \frac{1}{4\pi^2} \int d^2\vec{b} e^{i\vec{b}\cdot\vec{t}} \exp \left[- \int [dk] P(z) \left(1 - e^{-i\vec{b}\cdot\vec{t}} \right) \right]$$

$$\equiv \frac{1}{4\pi^2} \int d^2\vec{b} e^{i\vec{b}\cdot\vec{t}} e^{-R(b)}$$

$$\frac{d\sigma}{tdt} = \int_0^{\infty} b db J_0(bt) e^{-R(b)}$$

- ▶ Structure of NLL resummation

$$\Sigma(t) = (1 + \alpha_s C_1^{(q)}) S(\alpha_s L) e^{-R_q(\alpha_s C_F, L)} + \alpha_s C_1^{(g)} e^{-R_g(\alpha_s C_A, L)}$$

- ▶ Non Global Logarithms [Dasgupta, Salam, hep-ph/0104277]

$$S(\alpha_s L) = 1 + \sum_{n=2} S_n(\bar{\alpha}_s L)^n$$

$$\rightarrow 1 - (\bar{\alpha}_s L)^2 \cdot C_F C_A \frac{\pi^2}{3}$$

Radiator in b -space

- Radiator in b -space: $-R = Lf_1 + f_{2c} + f_{2s}$, $\lambda = \alpha_s \beta_0 \bar{L}$, $B_q = \frac{3}{4}$

$$f_1(\lambda) = -\frac{C_F}{2\pi\beta_0\lambda} [(1-2\lambda)\log(1-2\lambda) - 2(1-\lambda)\log(1-\lambda)]$$

$$f_{2c}(\lambda) = -\frac{C_F B_q}{\pi\beta_0} \log(1-\lambda) - \frac{C_F K}{4\pi^2\beta_0^2} [2\log(1-\lambda) - \log(1-2\lambda)] \\ - \frac{C_F \beta_1}{2\pi\beta_0^3} \left[\log(1-2\lambda) - 2\log(1-\lambda) + \frac{1}{2} \log^2(1-2\lambda) - \log^2(1-\lambda) \right]$$

$$f_{2s}(\lambda) = -\frac{C_F}{2\pi\beta_0} \log\left(\frac{1 - \frac{\tan^2 \frac{R}{2}}{\tan^2 \frac{\theta_{12}}{2}}}{4 \tan^2 \frac{R}{2}}\right) \log(1-2\lambda)$$

Radiator in b -space

- ▶ Radiator in b -space: $-R = Lf_1 + f_{2c} + f_{2s}$, $\lambda = \alpha_s \beta_0 \bar{L}$, $B_q = \frac{3}{4}$

$$f_1(\lambda) = -\frac{C_F}{2\pi\beta_0\lambda} [(1-2\lambda)\log(1-2\lambda) - 2(1-\lambda)\log(1-\lambda)]$$
$$f_{2c}(\lambda) = -\frac{C_F B_q}{\pi\beta_0} \log(1-\lambda) - \frac{C_F K}{4\pi^2\beta_0^2} [2\log(1-\lambda) - \log(1-2\lambda)]$$
$$- \frac{C_F \beta_1}{2\pi\beta_0^3} \left[\log(1-2\lambda) - 2\log(1-\lambda) + \frac{1}{2} \log^2(1-2\lambda) - \log^2(1-\lambda) \right]$$

$$f_{2s}(\lambda) = -\frac{C_F}{2\pi\beta_0} \log\left(\frac{1 - \frac{\tan^2 \frac{R}{2}}{\tan^2 \frac{\theta_{12}}{2}}}{4 \tan^2 \frac{R}{2}}\right) \log(1-2\lambda)$$

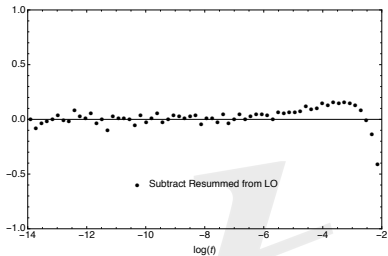
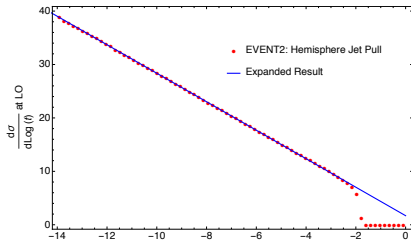
- ▶ Expansion of resummed result:

$$\frac{d\sigma^{\text{exp}}}{dt} = \int_0^\infty b db J_0(bt) \left(1 - R + \frac{R^2}{2}\right)$$

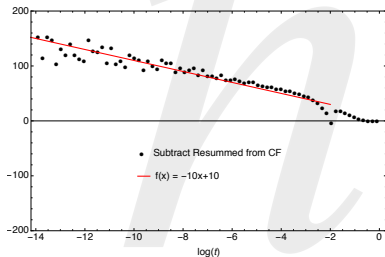
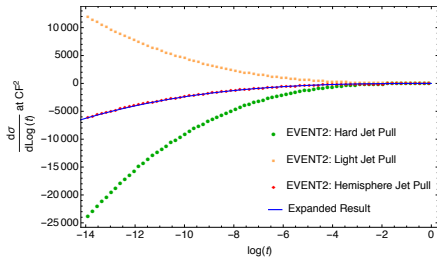
$$\frac{d\sigma^{\text{LO}}}{d\log t} = -\frac{\alpha_s C_F}{\pi} \left(\log \frac{t}{4 \tan^2 \frac{R}{2}} + \frac{3}{4} \right)$$

Compare with EVENT2

▶ LO channel

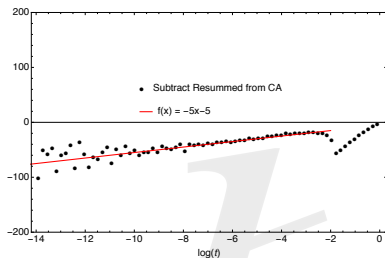
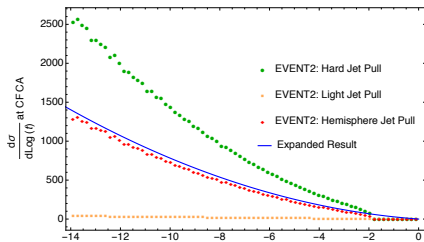


▶ CF^2 channel $\sim \alpha_s^2 L^3$

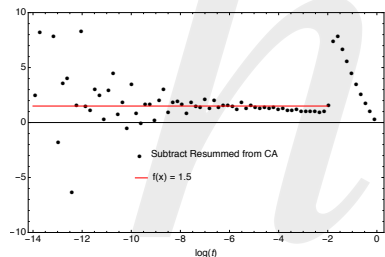
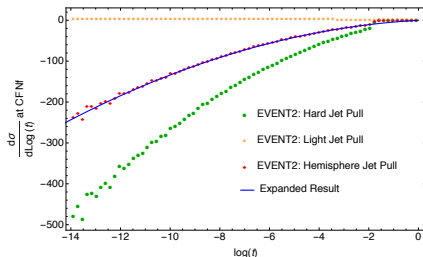


Compare with EVENT2

- CF CA channel (with NGL) $\sim \alpha_s^2 L^2$



- CF Nf channel $\sim \alpha_s^2 L^2 \log(f)$



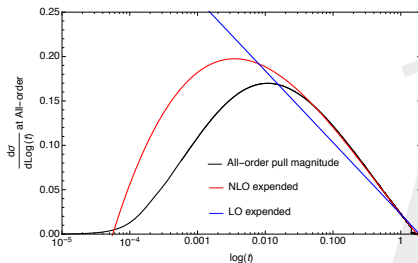
All-Order Resumed Result

- ▶ All-order numerical integration:

$$\frac{d\sigma^{all}}{dt} = \int_{b_{min}}^{b_{max}} b db J_0(bt) e^{-R(\alpha_s \bar{L})}$$

$$b_{min} = 2e^{-\gamma_E}, \quad \lambda \leq \frac{1}{2}$$

- ▶ All-order result:



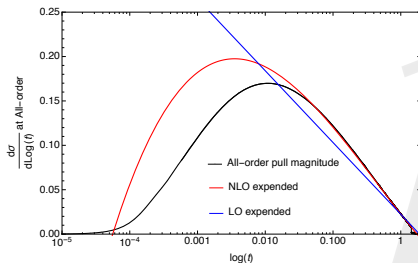
All-Order Resumed Result

- ▶ All-order numerical integration:

$$\frac{d\sigma^{all}}{dt} = \int_{b_{min}}^{b_{max}} b db J_0(bt) e^{-R(\alpha_s \bar{L})}$$

$$b_{min} = 2e^{-\gamma_E}, \quad \lambda \leq \frac{1}{2}$$

- ▶ All-order result:



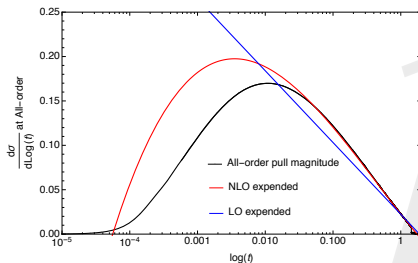
All-Order Resumed Result

- ▶ All-order numerical integration:

$$\frac{d\sigma^{all}}{dt} = \int_{b_{min}}^{b_{max}} b db J_0(bt) e^{-R(\alpha_s \bar{L})}$$

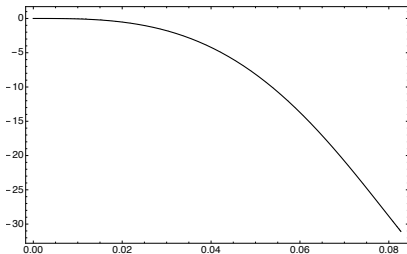
$$b_{min} = 2e^{-\gamma_E}, \quad \lambda \leq \frac{1}{2}$$

- ▶ All-order result:

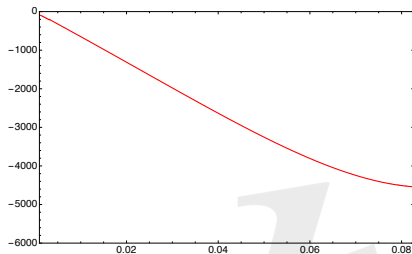


- ▶ Cross check: subtract expanded result from all-order, as a function of α_s

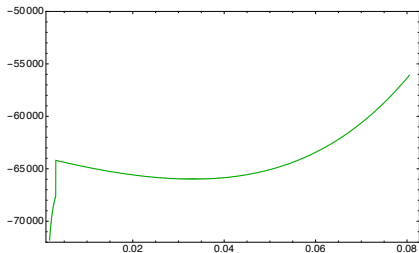
Cross Check: NLO



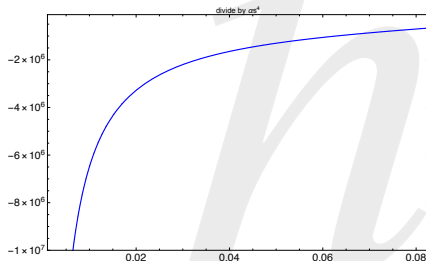
subtract NLO from all-order



divide by α_s^2



divide by α_s^3



divide by α_s^4

Improvement for the Fixed-Order Results

- ▶ Method of matching

$$\frac{1}{\sigma} \frac{d\sigma_{NLL+LO}}{d\log t} = \frac{1}{\sigma} \left[\frac{d\sigma_{LO}}{d\log t} + \frac{d\sigma_{NLL}}{d\log t} - \frac{d\sigma_{NLL, \alpha_s}}{d\log t} \right]$$

Improvement for the Fixed-Order Results

- ▶ Method of matching

$$\frac{1}{\sigma} \frac{d\sigma_{NLL+LO}}{d\log t} = \frac{1}{\sigma} \left[\frac{d\sigma_{LO}}{d\log t} + \frac{d\sigma_{NLL}}{d\log t} - \frac{d\sigma_{NLL, \alpha_s}}{d\log t} \right]$$

- ▶ Matched end-point

$$\log \frac{1}{t} \rightarrow \log \left(\frac{1}{t} - \frac{1}{t_{max}} + \frac{e^{Bq}}{4} \right)$$

with $t_{all} = 4e^{-Bq}$, $t_{max} \sim 0.2$

Improvement for the Fixed-Order Results

- ▶ Method of matching

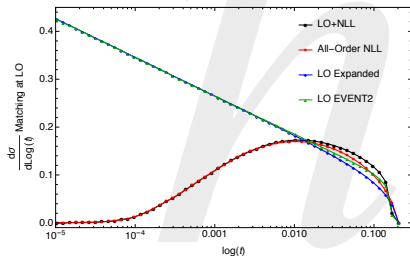
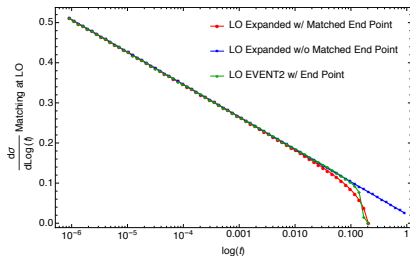
$$\frac{1}{\sigma} \frac{d\sigma_{NLL+LO}}{d\log t} = \frac{1}{\sigma} \left[\frac{d\sigma_{LO}}{d\log t} + \frac{d\sigma_{NLL}}{d\log t} - \frac{d\sigma_{NLL, \alpha_s}}{d\log t} \right]$$

- ▶ Matched end-point

$$\log \frac{1}{t} \rightarrow \log \left(\frac{1}{t} - \frac{1}{t_{max}} + \frac{e^{Bq}}{4} \right)$$

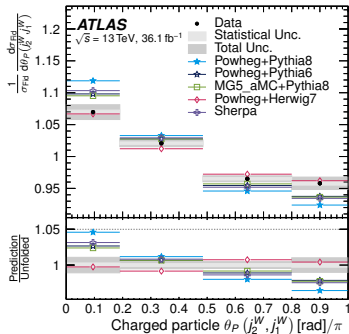
with $t_{all} = 4e^{-Bq}$, $t_{max} \sim 0.2$

- ▶ Result



Pull Angle: IRC unsafety

▶ Result from ATLAS



▶ Definition of pull angle

$$\phi_p = \cos^{-1} \frac{t_x}{t}$$

Pull Angle: *IRC* unsafety

- ▶ Joint probability approach:

$$\begin{aligned} p(\phi_p) &= \int dt p(t) p(\phi_p | t) \\ &\sim \int dt e^{-R(t)} \frac{d^2 \sigma^{Fo}}{dt d\phi_p} \end{aligned}$$

exponential suppression at soft-collinear region

- ▶ In the region of soft-collinear, fix order calculation spoiled by large logarithm $\log^m(t)$ enhancement

$$\frac{d\sigma}{dt} = \frac{d\sigma^{Res}}{dt} + \frac{d\sigma^{Fo}}{dt}$$

Calculation Technique (sketch)

► Formalism for the pull angle:

- Full double differential resummation approach ✗

$$\frac{d\sigma}{d\phi_p} = \frac{1}{2\pi} \int_0^\infty dt t \int_0^\infty b db J_0(bt) e^{-R(b)}$$

- Sudakov safety approach ✓

$$\frac{d\sigma}{d\phi_p} = \int dt e^{-R(t)} \frac{d^2\sigma^{Fo}}{dt d\phi_p}$$

Calculation Technique (sketch)

► Formalism for the pull angle:

- Full double differential resummation approach ✗

$$\frac{d\sigma}{d\phi_p} = \frac{1}{2\pi} \int_0^\infty dt t \int_0^\infty b db J_0(bt) e^{-R(b)}$$

- Sudakov safety approach ✓

$$\frac{d\sigma}{d\phi_p} = \int dt e^{-R(t)} \frac{d^2\sigma^{Fo}}{dt d\phi_p}$$






- New (IRC safe) observable: $t_x = \sum_i \frac{E_i \sin^2 \theta_i}{E_J} \cos \phi_i$

$$\frac{d\sigma}{dt_x} = \frac{1}{\pi} \int_0^\infty db \cos(bt_x) e^{-R(b)}.$$

- ▶ Sudakov safety calculation
- ▶ Full double differential resummation
- ▶ Evaluate non-perturbative corrections, with Pythia

Future Works

- ▶ Push to higher accuracy (NNLL) and compare with ATLAS (**next project**)

-  J. Gallicchio and M. D. Schwartz, Seeing in Color: Jet Superstructure, Phys. Rev. Lett. 105 (2010) 022001, [arXiv:1001.5027 [hep-ph]].
-  ATLAS Collaboration, Measurement of color flow with the jet pull angle in $t\bar{t}$ events using the ATLAS detector at $\sqrt{s} = 8\text{ TeV}$, [arXiv: 1506.05629[hep-ex]].
-  ATLAS Collaboration, Measurement of color flow using jet-pull observables in $t\bar{t}$ events with the ATLAS experiment at $\sqrt{s} = 13\text{ TeV}$, [arXiv: 1805.02935[hep-ex]].
-  A. J. Larkoski and J. Thaler, Unsafe but Calculable: Ratios of Angularities in Perturbative QCD, JHEP 1309 (2013) 137, [arXiv:1307.1699[hep-ph]].
-  M. Dasgupta and G. P. Salam, Resummation of non-global QCD observables, Phys. Lett. B512, 323(2001), [arXiv: hep-ph/0104277]