



Queen's Engineering Team Projects

Arthur B. McDonald
Canadian Astroparticle Physics Research Institute



A. Mir, J. Kingma, J. Corbett, K.
Dering, M. Dean, N. Moss, R.
Gagnon

P-ONE PMT Testing

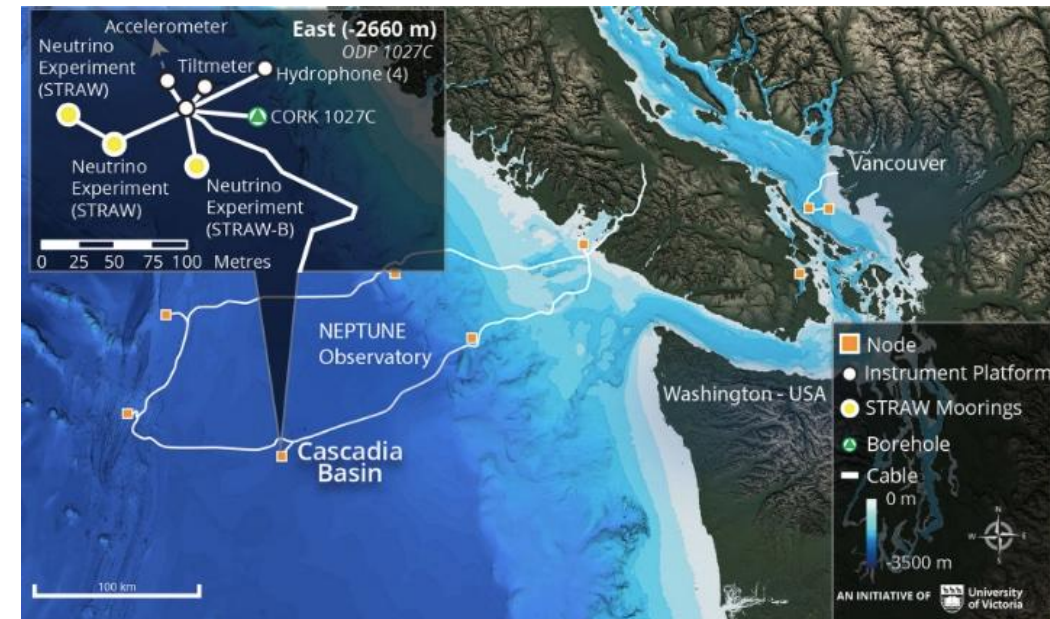
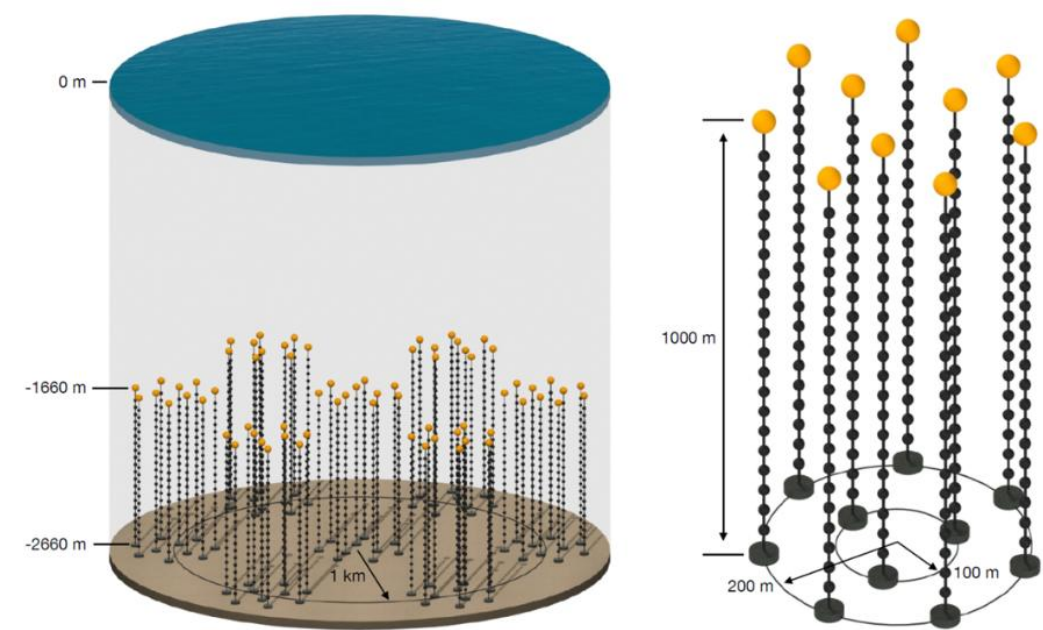
Pacific Ocean Neutrino Telescope (P-ONE)

Underwater observatory, (like IceCube) to detect high energy neutrino events, off coast of Vancouver Island w/ existing Ocean networks infrastructure

20 light detectors (Precision optical modules, P-OMs) per “string”, 10 strings make a cluster, 7 clusters make P-ONE...

$20 \times 10 \times 7 = 1400$ light detectors to calibrate, verify performance!!

*See **Jessie, Jakub & Bryan's** talk tomorrow for more about this*



P-ONE PMT Testing

Ease of installation/removal for quicker turnaround (calibrate in batches of 2×16 → that's still 44 batches to complete all 1400 PMTs)

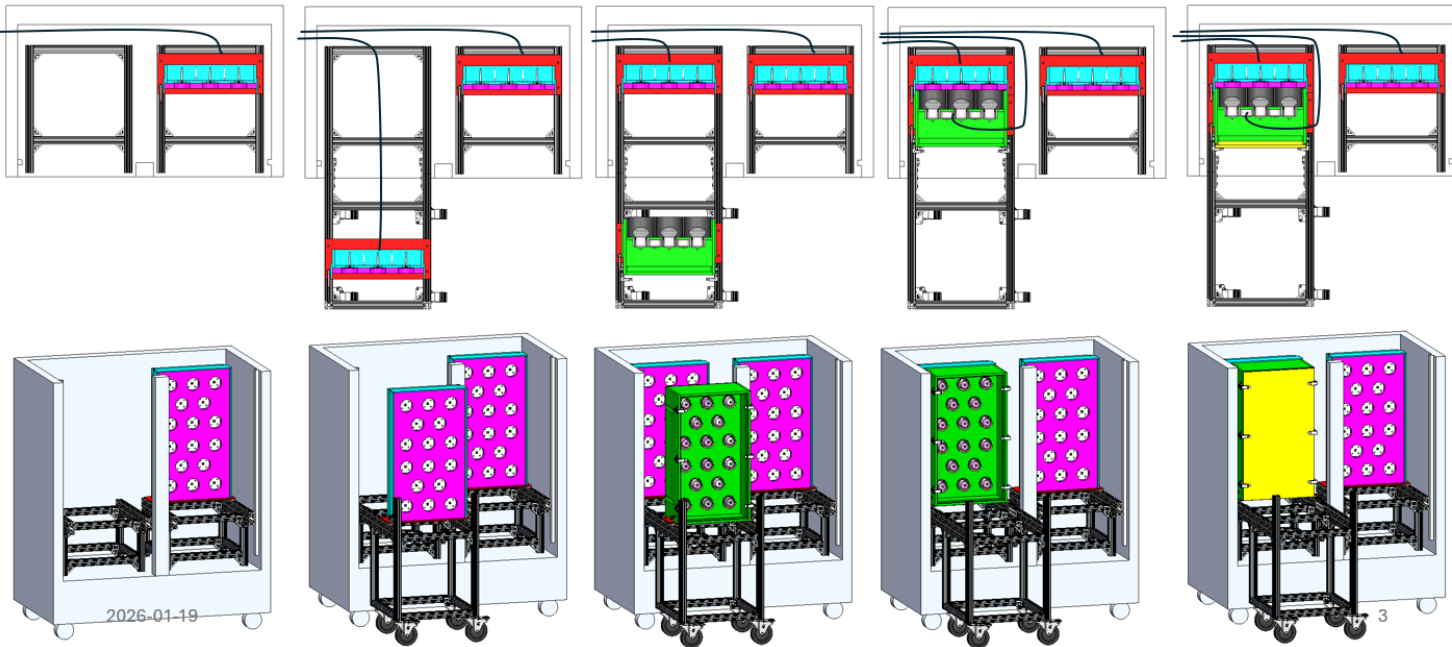
1. Insert fibre tray (right)
2. Connect fibres (right)

3. Connect fibres (left)

4. Insert fibre tray (left)
5. Prep PMT tray (left)

6. Insert PMT tray (left)
7. Connect PMT electrical (left)

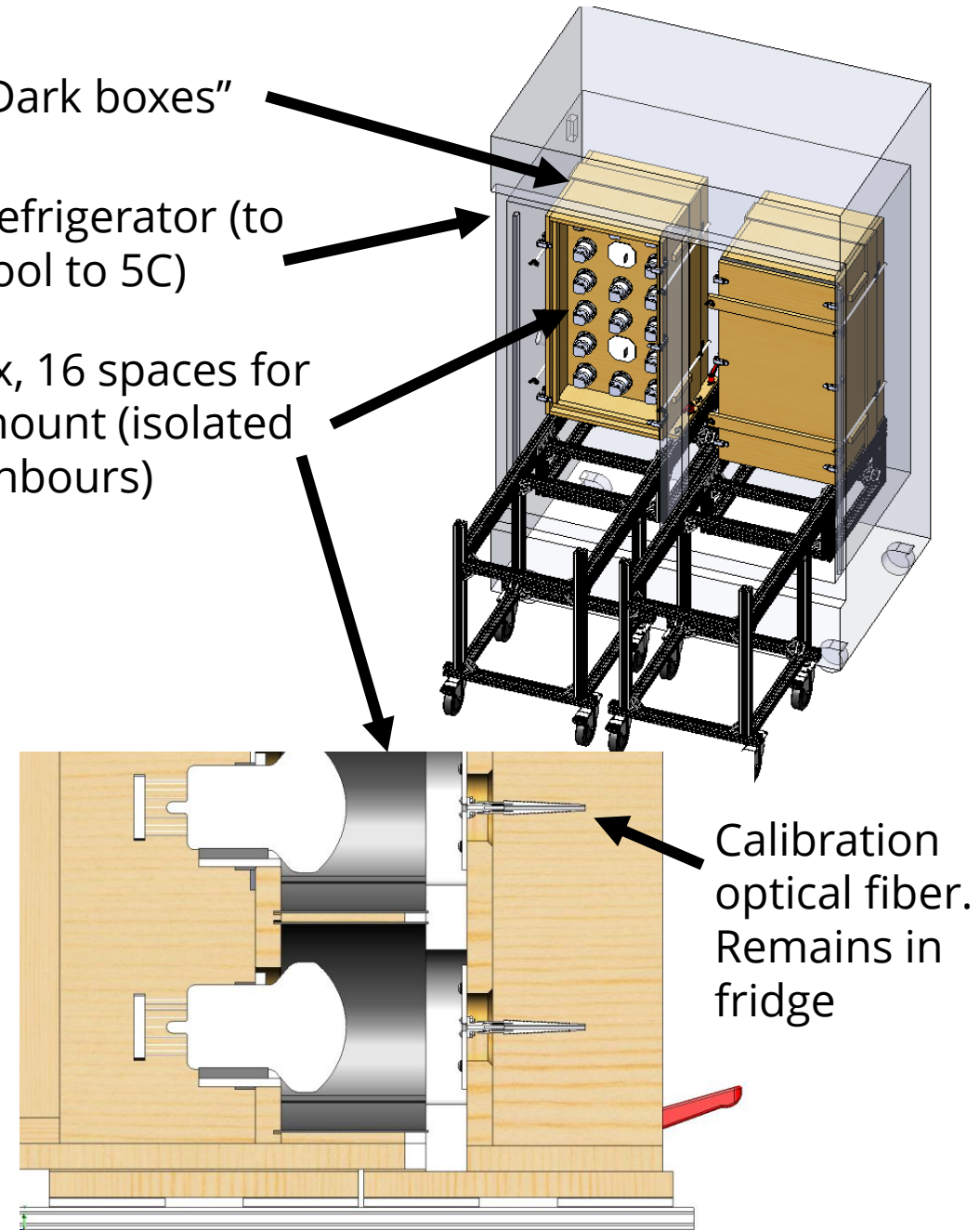
8. Install PMT tray lid (left)
9. Repeat with right PMT tray



"Dark boxes"

Refrigerator (to cool to 5C)

Within box, 16 spaces for PMTs to mount (isolated from neighbours)

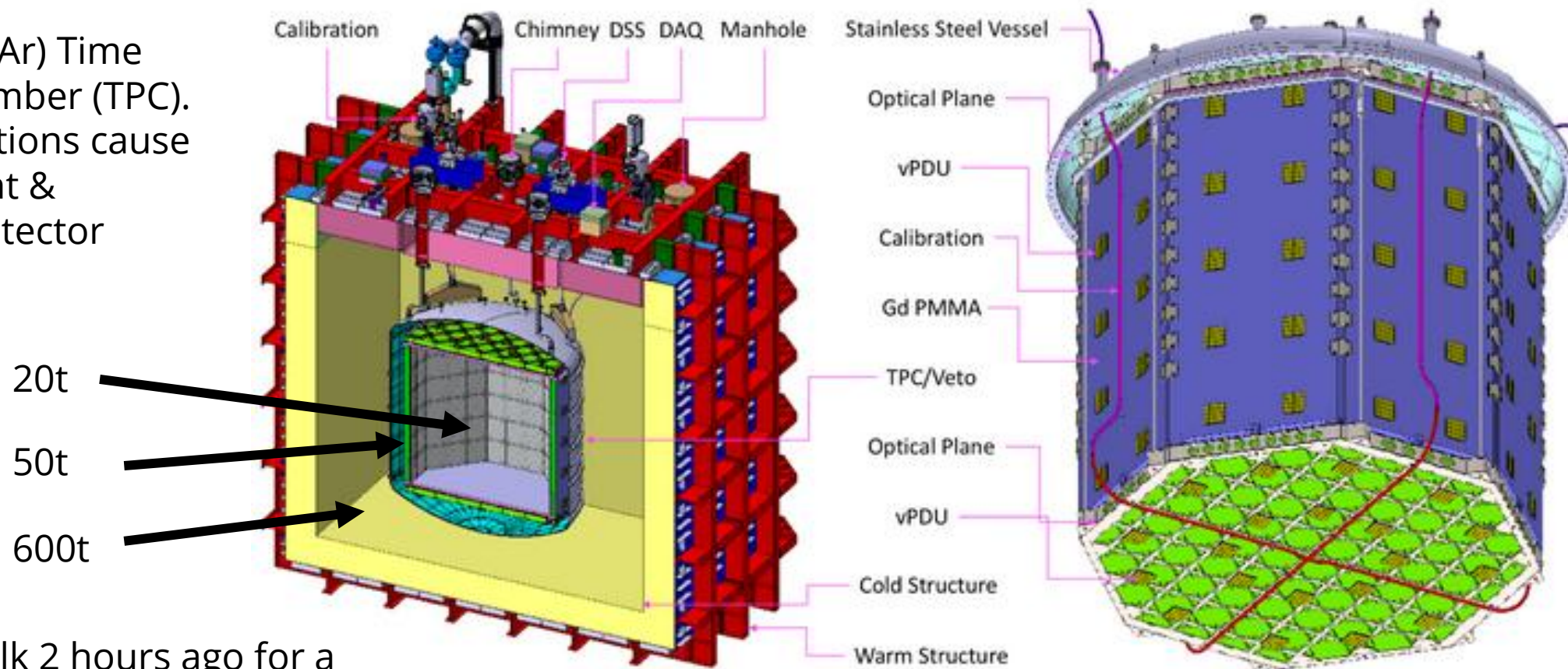


P-ONE PMT Testing Construction



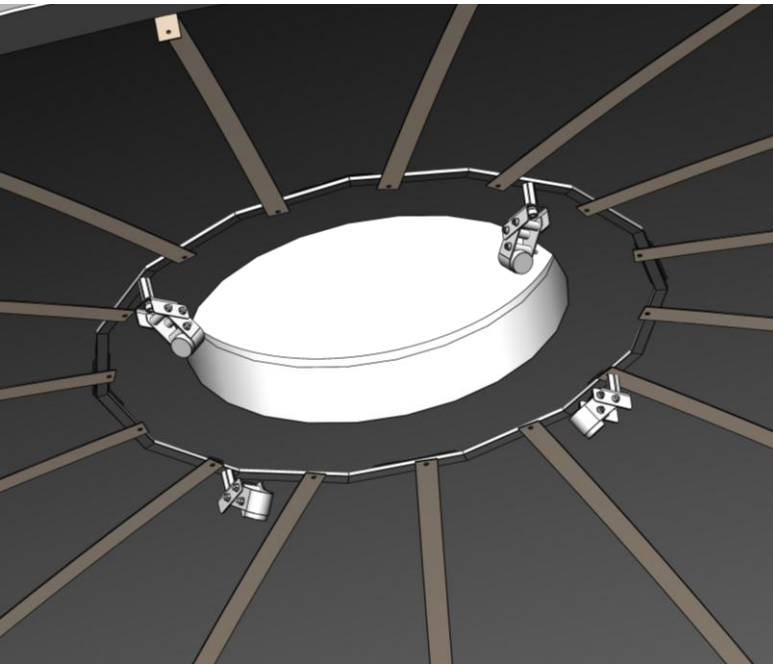
DarkSide-20k

Liquid Argon (LAr) Time Projection Chamber (TPC). Particle interactions cause scintillation light & ionization in detector

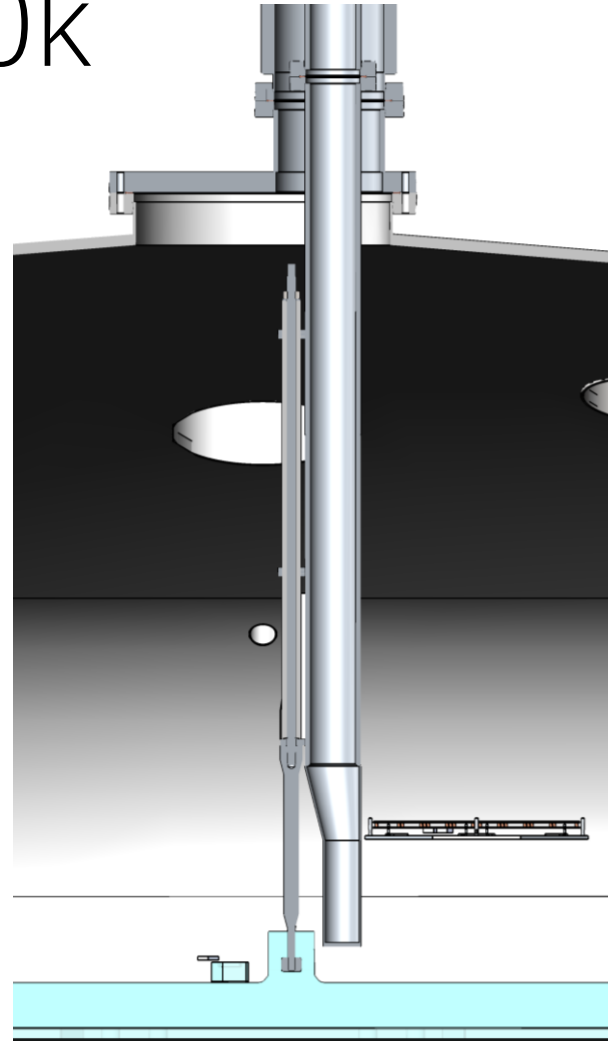


*See **Peter's** talk 2 hours ago for a related experiment (DEAP-3600)*

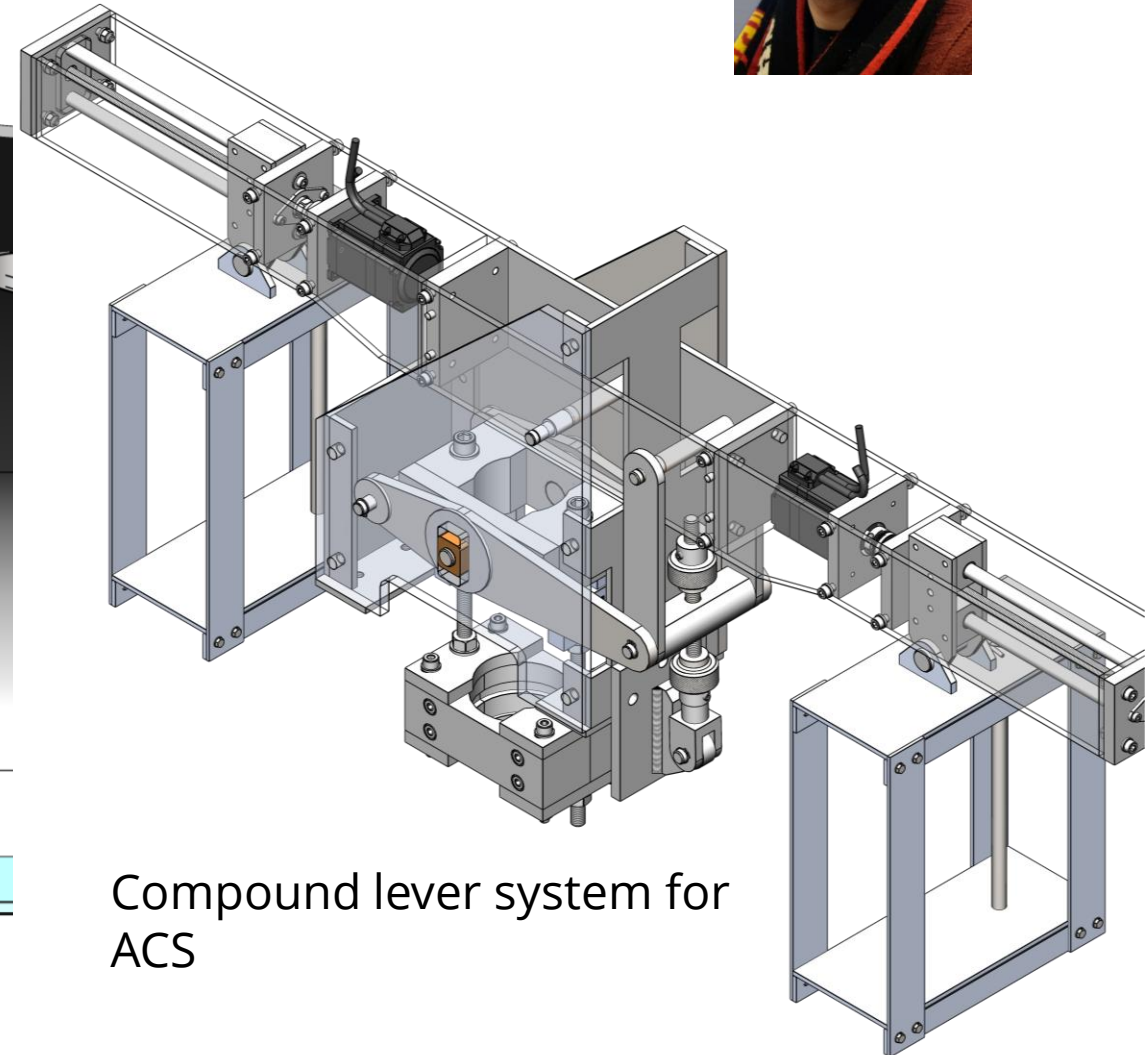
DarkSide-20k



Optical diffuser mounting
inside stainless-steel vessel.



Actuator-anode interface for
Anode Control System (ACS)



Compound lever system for
ACS

KDK SDD2

KDK SDD2 Detector Base Design

Mackenzie Dean & Jonathan Corbett

December 10th, 2025

Introduction

In the previous iteration of the KDK SDD detector design, a single detector was cooled by a chiller cooling loop (-50C) that was well thermalized to the detector. For this second generation of the experiment, two detectors are to be sandwiched around the source disk, and the strategy for cooling the detector is also changing in a hope to achieve better stability and control over the base temperature.

Geometry Changes

Going from one detector oriented along the principal axis of the vacuum tube to two detectors stacked on top of each other necessitates design changes. A large Aluminum detector base serves as the foundation that the other detector elements are secured to. The detector PCB has what the readout and biasing cable connects to and distributes the signals to the appropriate channels that the readout electronics will use. This is done by mounting the Aluminum substrate below matching the profile of the PCB. The detector is mechanically mounted to the Alumina, with the wire bonds on top and bottom surfaces connecting directly to the PCB. This assembly is then mirrored and repeats on the bottom side of the Al detector base providing a symmetric assembly of 2 detectors around a gap that the source is located. The source disk is mounted in a holder assembly which is mounted to the detector base. This holder assembly is secured to the detector base by a screw for a heater is further back on the Al detector base before it connects to the thermal rod. A diagram of one of the proposed detectors (Rev 7) is shown below.

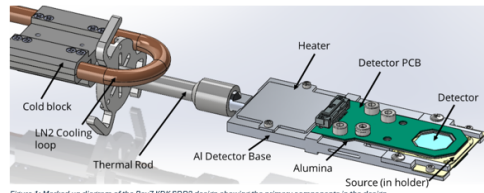
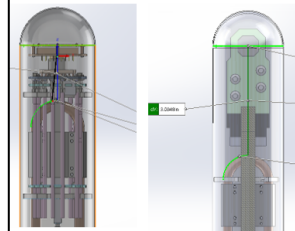


Figure 1: Marked up diagram of the Rev7 KDK SDD2 design showing the primary components in the design

thermal rod, cold block, and LN2 cooling loops remain unchanged except it will be described in subsequent sections. The end of the thermal rod will join the rod "spine" via a plastic thermal-break threaded nut, that runs the full length of the rod to provide rigid mechanical support during insertion and removal. The rod will be reused throughout the length of the vacuum chamber to aid in centering the beam. Since the Al detector base for this design is longer than the Cu cooling loop and "spine" beyond the thermal break must be adjusted rearward to have it all still fit in the same vacuum jacket (and have position of the center of MTAS), as highlighted in Figure 2 below. With both proposed beamline centering to shorten the tubes and rod by about 3.5".

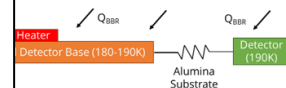


cooling tube sits further back in the vacuum tube in the new design (right side) design (left side), highlighting the need for the copper tube and Aluminum "spine" to be dated. Shown is a previous revision (rev 2) of the new design, it is expected the final the tubing and spine will be informed by the approved final detector.

Investment Strategy

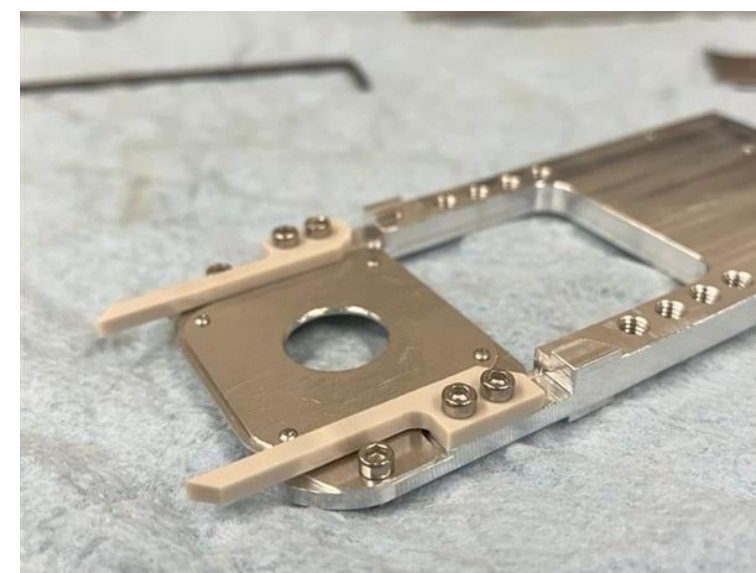
fluid coming from a chiller circulating through the cooling loop was in the range of 10 K as the desired detector and electronics temperature. From a thermal management point of view the goal was to have as efficient thermal conductivity from the detector to the cooling loop as possible. Now, Liquid Nitrogen will be flowing through a copper tubing loop at the cold block, resulting in a large temperature gradient difference

nd detector temperature. A "thermal rod", is clamped onto
nal conductance path to the base structure that
r, and source. This detector base is made from Aluminum,
ation is that temperature variations throughout the Al will
ted on an Alumina substrate serving as a lateral thermal
it has been cut away from the Al base. Because of the
and the poor conductivity of the PCB material, it is
variations (on order of $\sim$ few degrees) between the Al base
that the inbound blackbody radiative heat load on the
nd is distributed across the outer faces of the assembly –
base to the cold block to be able to conduct the heat larger
adequately cool the detector. To prevent the Aluminum
ad adjustable thermal impedance factors to the design of
uted to the detector base which can add more heat to a
desired temperature stability. The diagram below
ately.

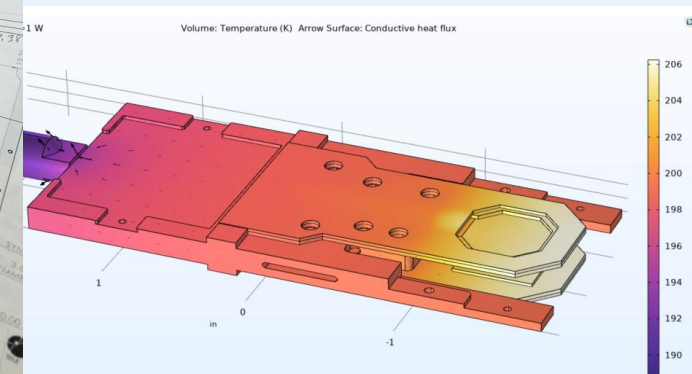
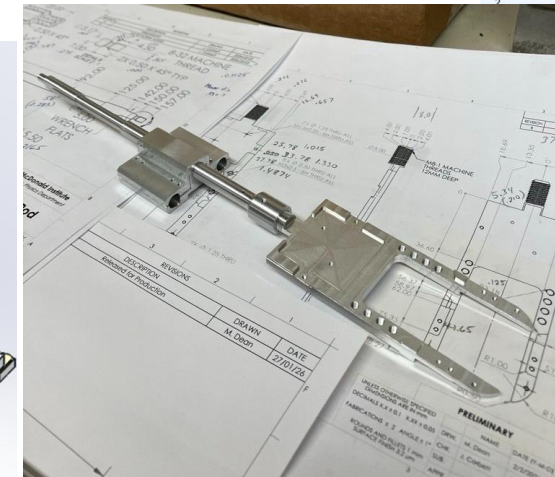
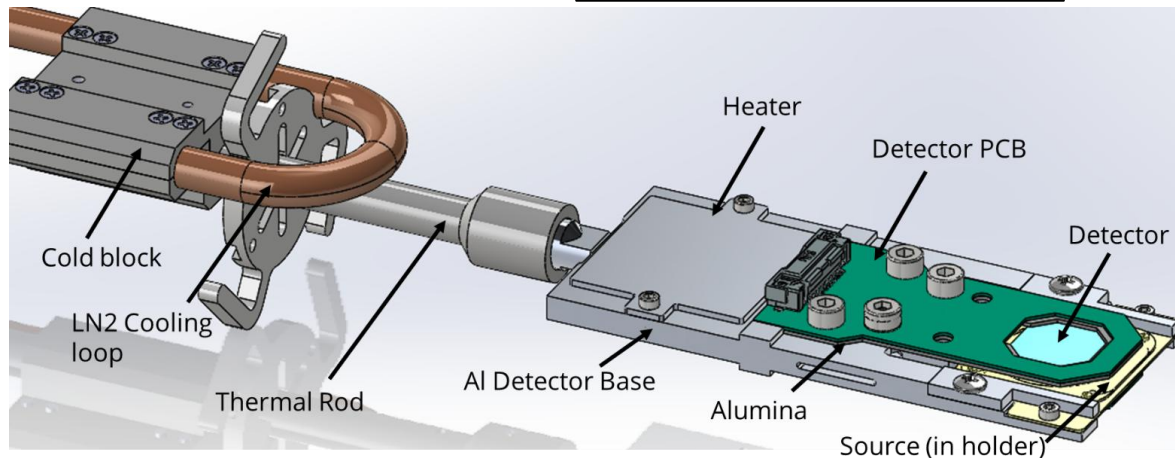
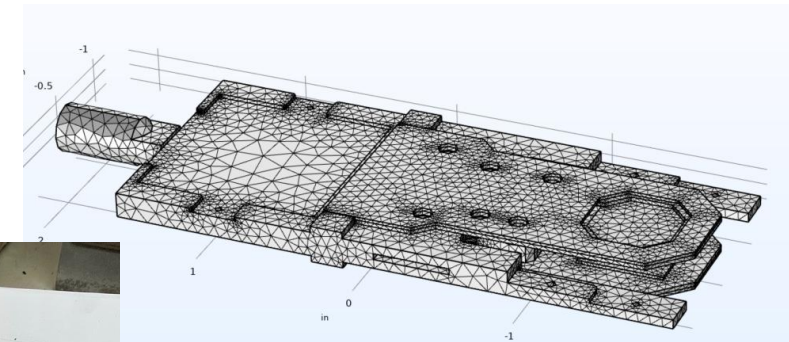


block is directly cooled by a Liquid Nitrogen loop; the thermal rod provides the Aluminum detector base. The conduction path to the detector is through an Ω of resistance. Heat from blackbody radiation is absorbed on all external be conducted away.

In the prior iteration of KDK SDD design but remaking the Copper for the lower thermal conductivity ($\sim 140 \text{ W/m}\cdot\text{K}$ vs. physics implications). As with before, we can adjust the ρ by adjusting the length of the thermal rod between the cold block forwards or backwards on the thermal rod and

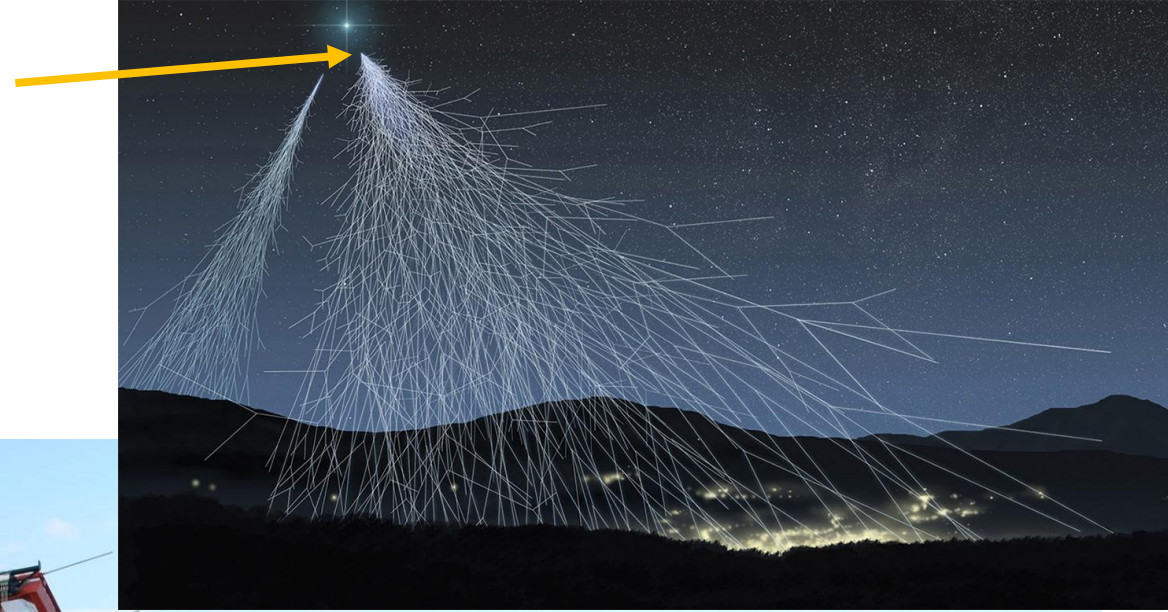


Mechanical design,
thermal verification, &
fabrication for 2nd gen
Silicon Drift Diode (SDD)
experiment looking for
rare nuclear decay
modes



HELIX

The particle that made the shower (that we go to SNOLAB to shield ourselves from)



High Energy Light Isotope eXperiment (HELIX)

40km up, “cosmic rays” hitting upper atmosphere

What’s the composition of cosmic rays?

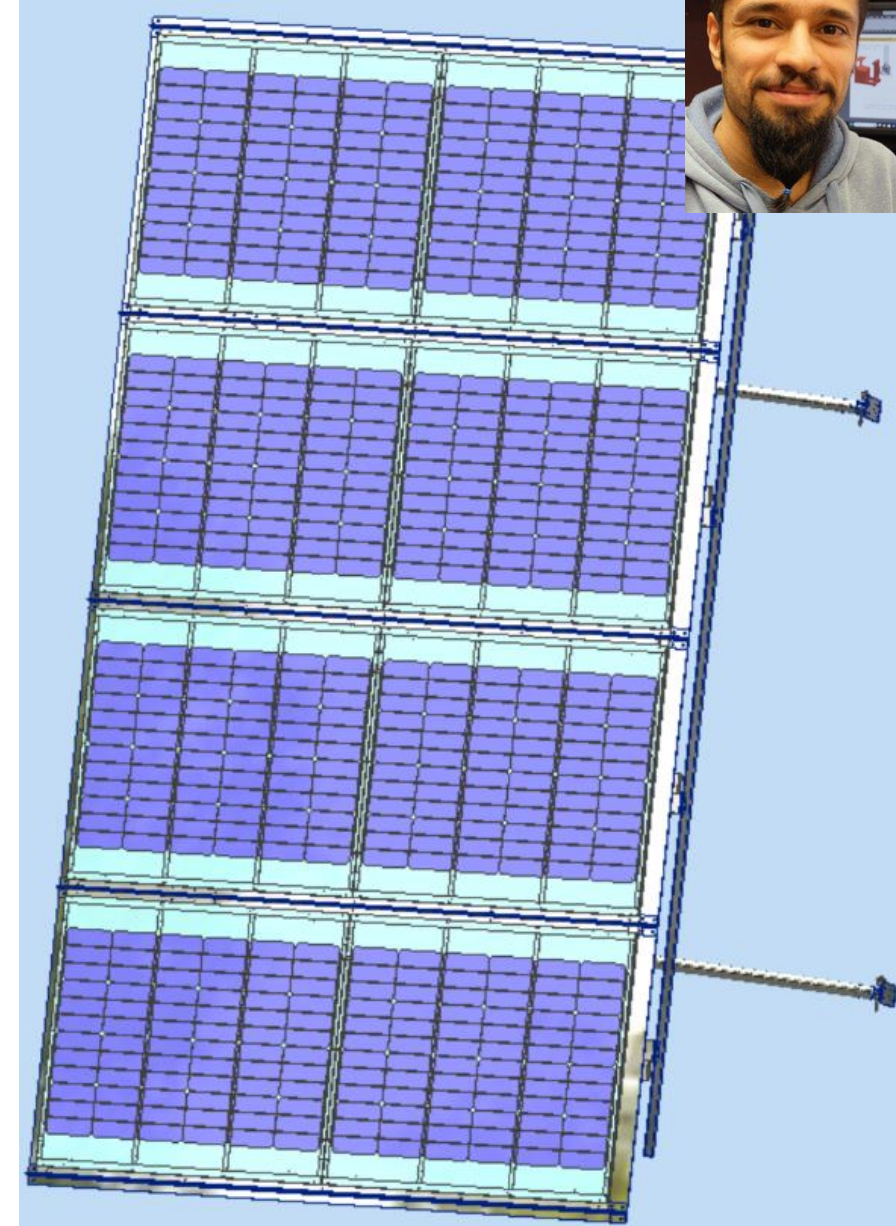
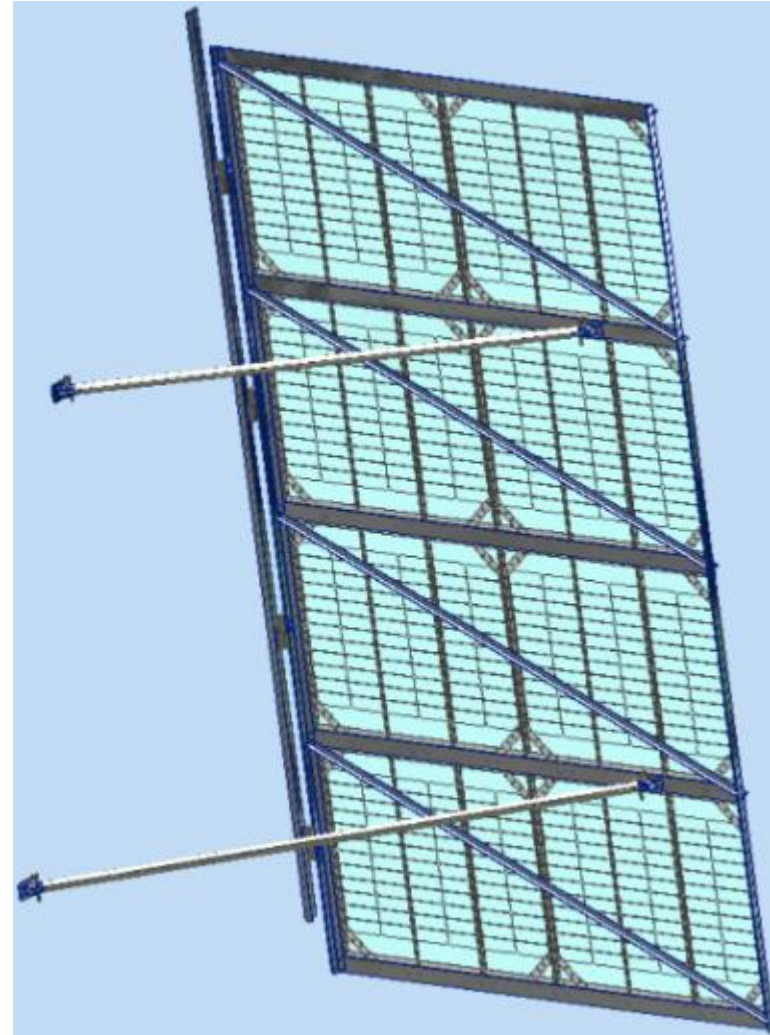
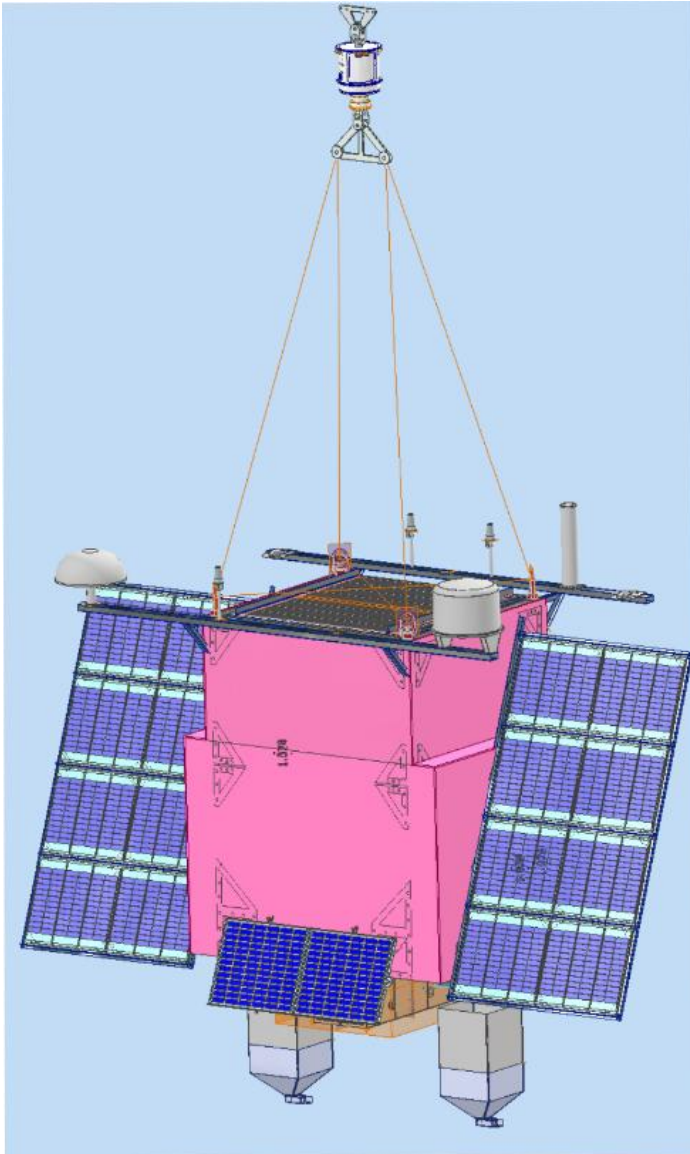
- 90% Protons
- 9% Helium/alphas
- 1% **everything else**

This experiment is measuring the composition of “everything else”

*See **Conor’s** talk tomorrow for more about this*



HELIX



HELIX - Requirements



Procedures and Guidelines (PG)

DIRECTIVE NO. 820-PG-8700.0.1A
EFFECTIVE DATE: November 5, 2024
EXPIRATION DATE: November 5, 2029

APPROVED BY Signature: Original Signed By
NAME: Andrew Hamilton
TITLE: Chief, Balloon Program Office

COMPLIANCE IS MANDATORY

Responsible Office: Code 820/ Balloon Program Office (BPO)
Title: Gondola Structural Design Requirements

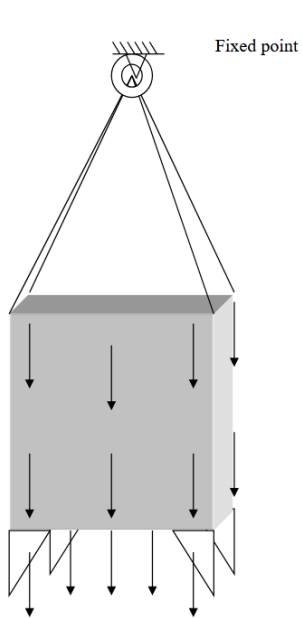


Figure 2: Load Case #1 - Gondola Vertical Loading

Parachute "shock" - 8g

Parachute failure - only 1 or 2 cables supporting - tilt!

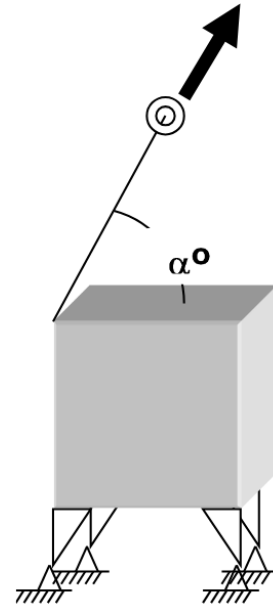
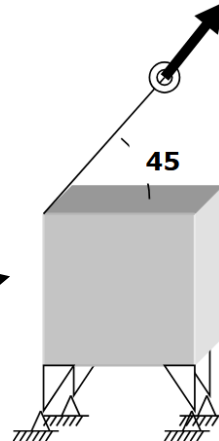
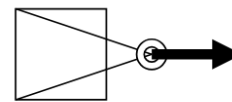


Figure 3: Load Case #2 - Gondola Single Cable Loading

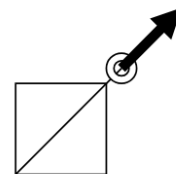
Pin constraints



Pin constraints



Load Case 3A

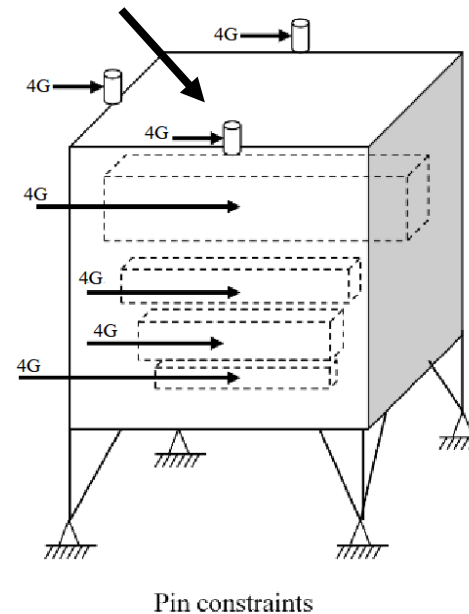


Load Case 3B

Views Looking Down

Figure 4: Load Case #3 - Off-Vertical Gondola Loading

Gondola rotated, falling sideways



Pin constraints

Figure 5: Load Case #4 - Gondola Lateral Loading

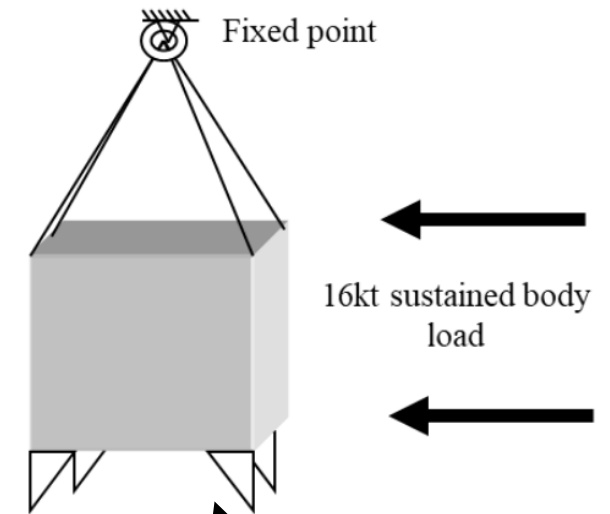


Figure 6: Load Case #6 - Sustained Wind Loading

Upper atmosphere is windy!

SNO+ Platform needed

Make platform to attach to this shell structure (safely)

To be able to remove some equipment in the way (PMT panels)

So that they can look at this

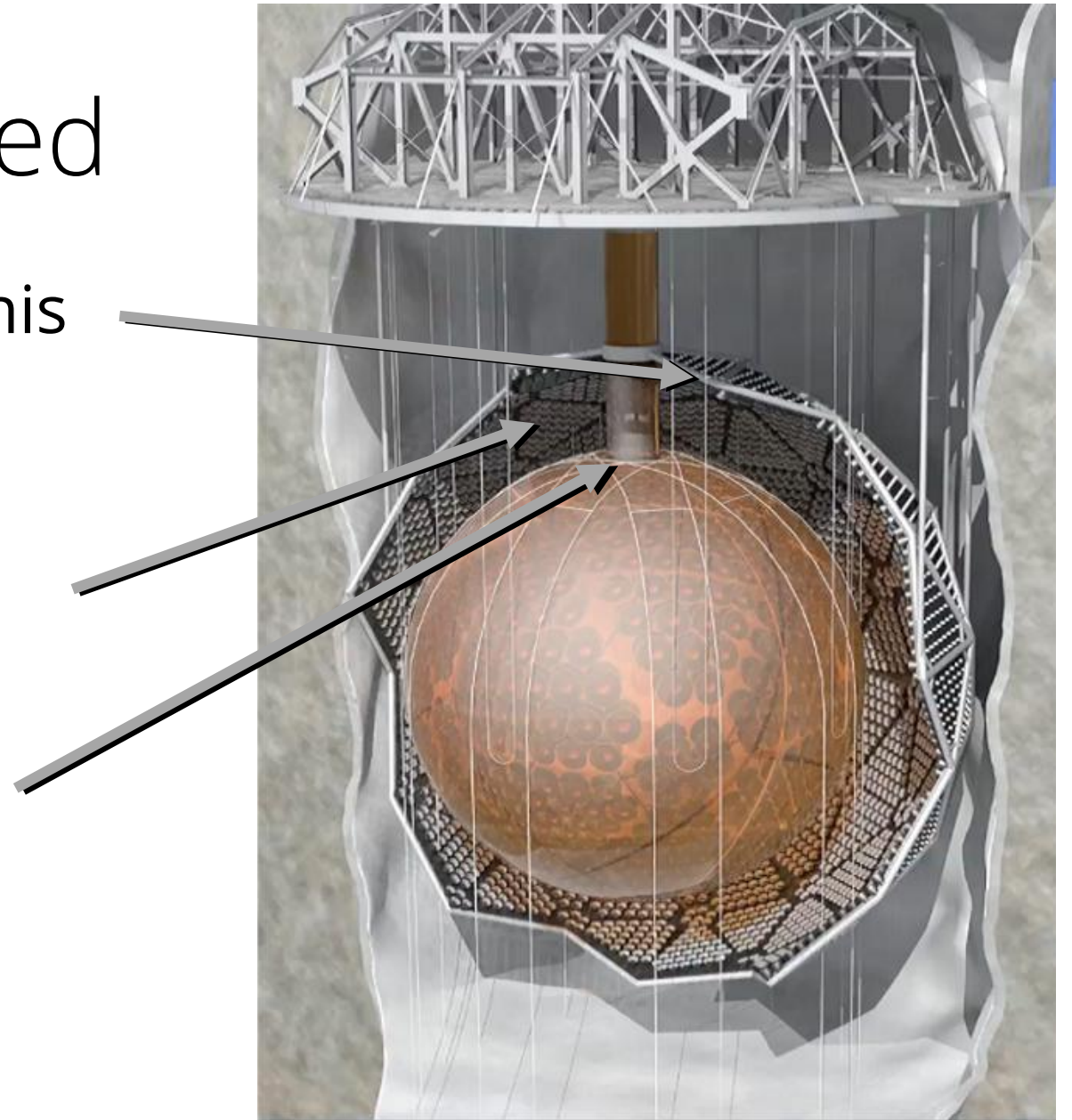
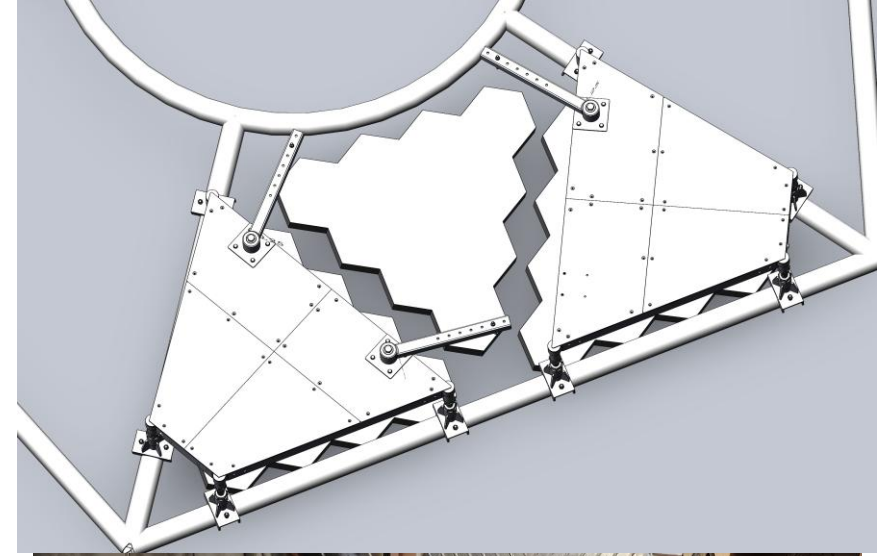


Image credit: <https://snoplus.phy.queensu.ca/about.html>

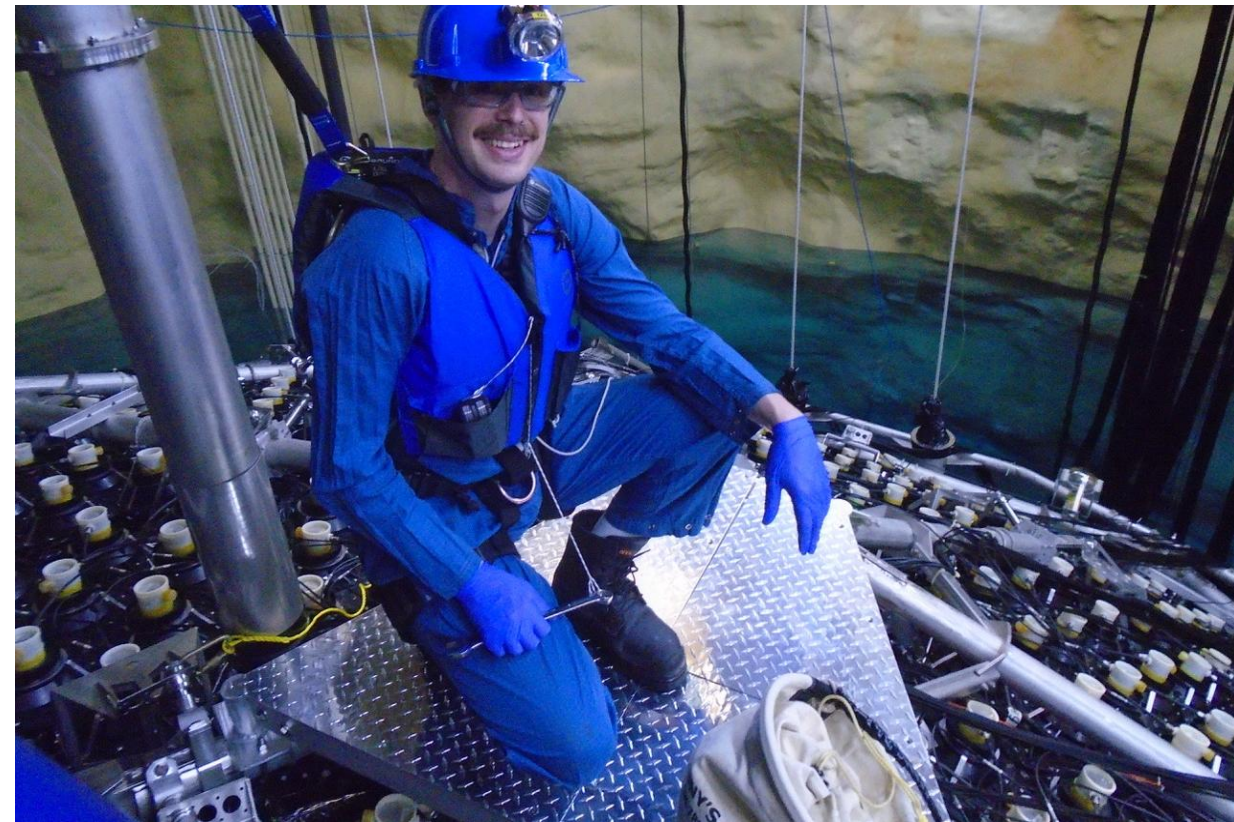
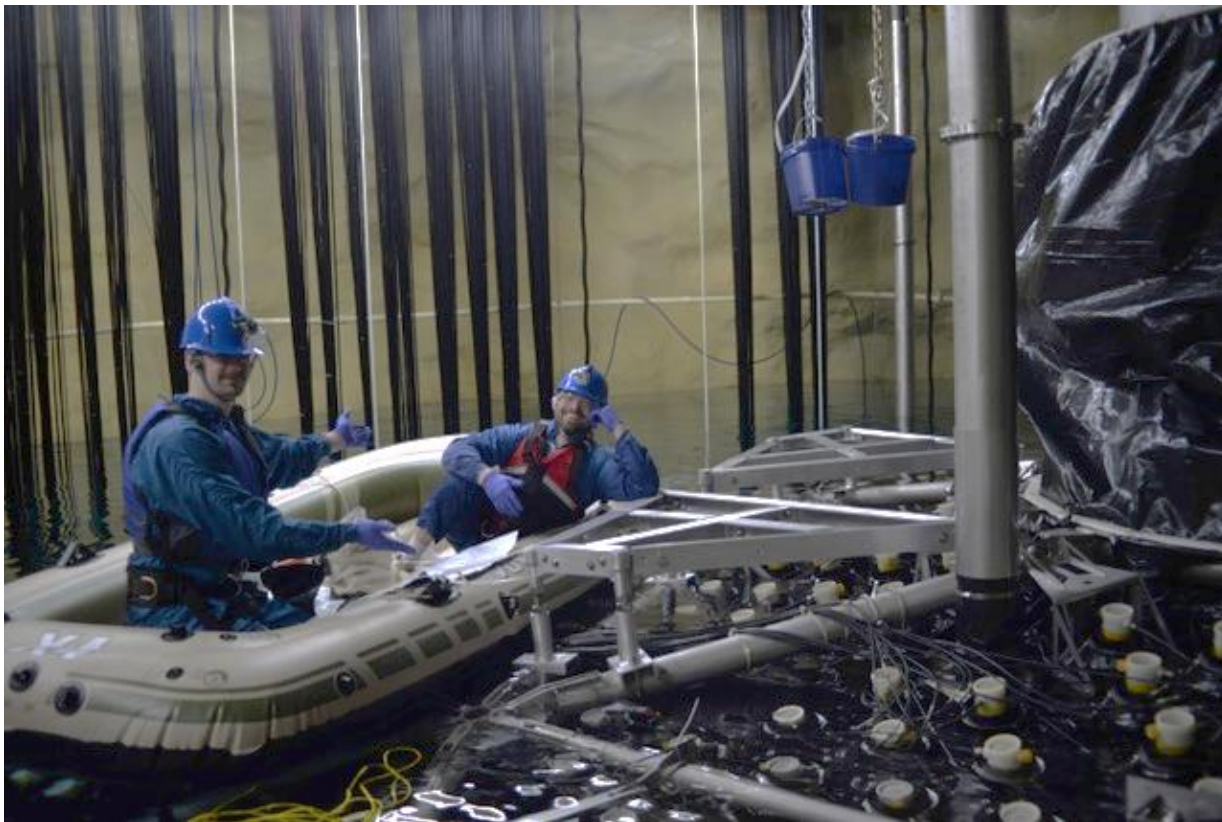
SNO+ Solution



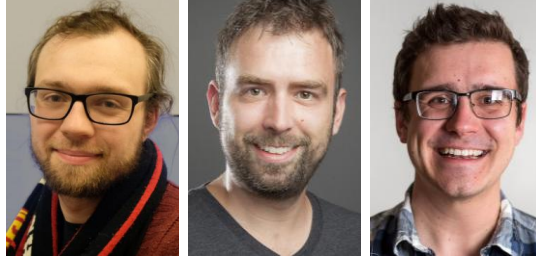
- Nic responded to the high urgency call. Great job, Nic!
- Reviewed old design & fabrication drawings/documents
- Designed platform segments
- Design reviewed & approved by SNOLAB's structural Engineer (Civil P.Eng)
- Built @ Queen's, critical (structural) welding done by certified shop in Kingston



SNO+ Platform Deployed



SBC

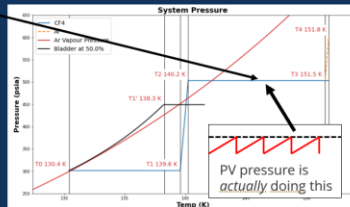


- PV Construction & TSSA Registration managing
- Maintaining engineering drawings
- Supporting documentation, engineering studies

*See **Carter, Ezri, & Alex's** talks this afternoon*

Want to test burst disk in blowdown?

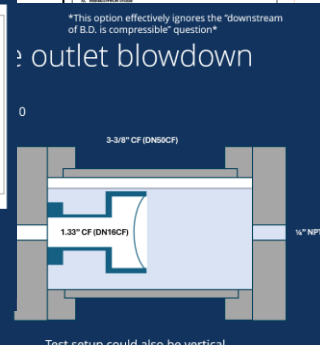
Late in T2-T3 period, inner jar floating, LAR partially tracks CF4 pressure during blowdown - P won't go down once IJ hits end stops



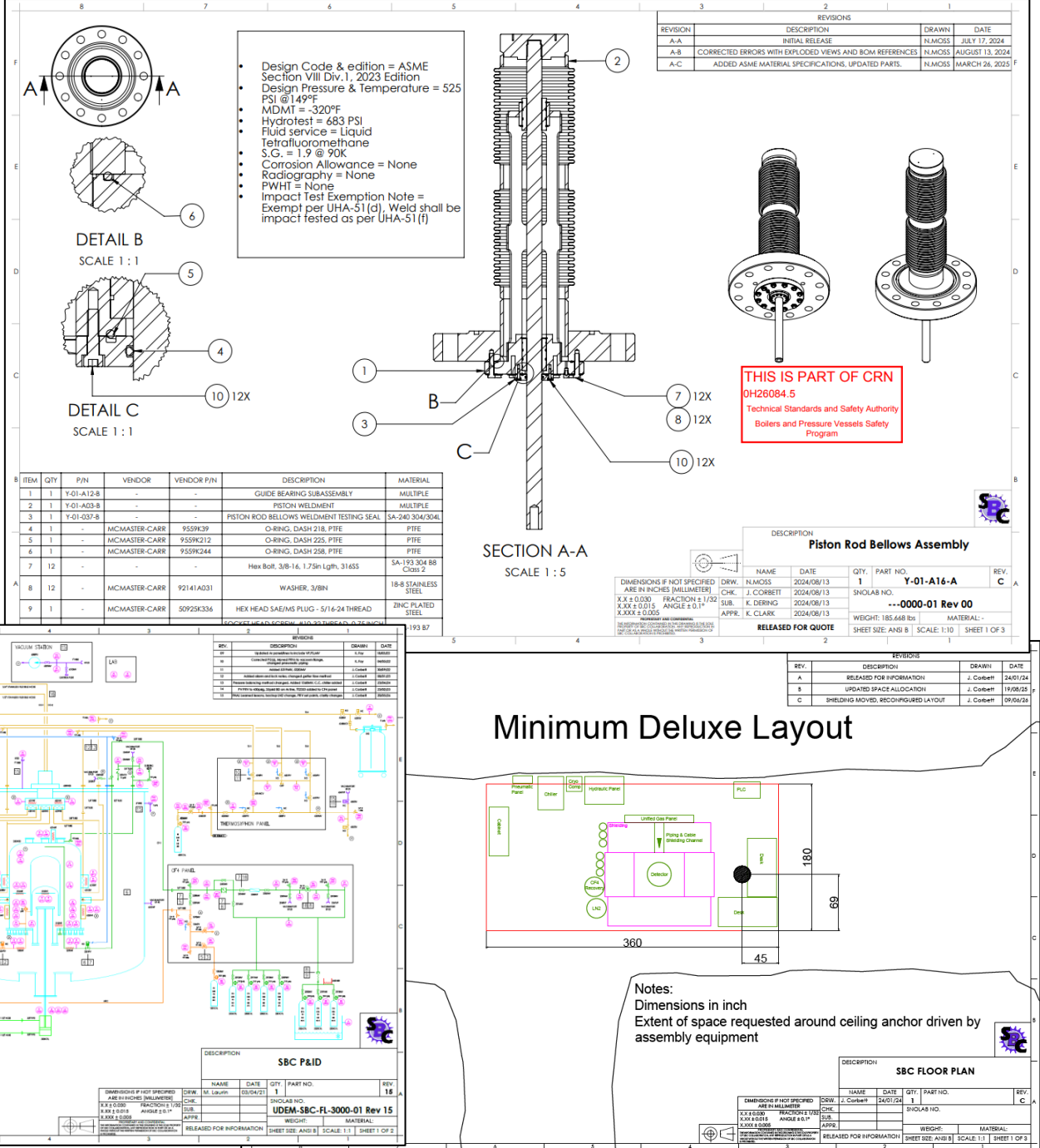
This is the likely time when disk will rupture. Inner jar low enough that Ar pressure remains high enough that when PRV blows down to ~420psig in CF4 space we have a 25psid

"Short, precise blow-down" → ASME dictates blowdown must be < 7% (for "adjustable blowdown valves")... 450psig * 7% = **31.5psid**

4. Pressurize outlet side slowly, force relief & blowdown (X-25) - should trigger rupture



Test setup could also be vertical...



PICO-500



- PV contract, design, registration
- Fluid carts
- Field Piping
- Cold plate
- Insulation & heaters*
- R.R.s & C.C.s*
- ... and more

*See **William's** talk this afternoon*



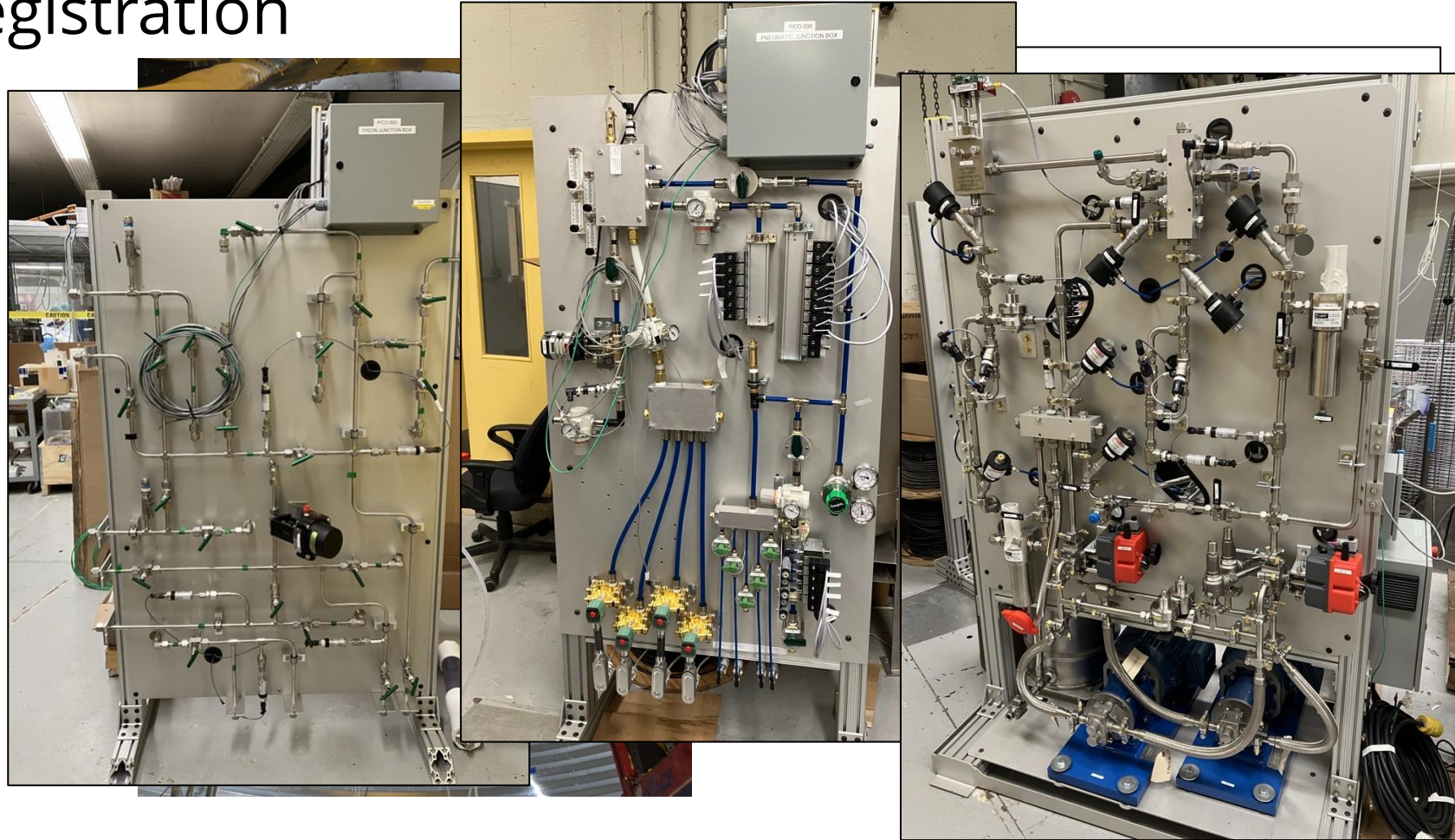
Files in Document:	
• (1A) PV drawings (QUDO-PFH-AR-2001-00_Rev_0.pdf, 39.4 MB)	
• (1B) PV attachments drawings (QUDO-PFH-AR-2002-00_Rev_0.pdf, 5.9 MB)	
• (1C) Sight window drawings (QUDO-PFH-AR-2003-00_Rev_0.pdf, 356.8 kB)	
• (1D) Shipping frame drawings (2023-07-18 - Shipping Frames.pdf, 18.5 MB)	
• (1E) Modified guardrail dwg (QUDO-PFH-AR-2005-00_Rev_0.pdf, 665.5 kB)	
• (2A) PV code calculations (16468c-1 R1.pdf, 3.8 MB)	
• (2B) Bottom flange code calculations (3b. 16468c-3 R0 (40in blind with nozzles on it).pdf, 2.1 MB)	
• (2C) Vacuum jacket code calculations (16468c-2 R0.pdf, 4.1 MB)	
• (2D) Top centre lug calculations (3c. 16468c-4 R0.pdf, 1022.0 kB)	
• (2E) Original seismic analysis (18525f-1 R1.pdf, 2.6 MB)	
• (2F) Cyclic analysis (16468f-1 R1.pdf, 1.8 MB)	
• (2G) Nozzle schedule used for calculations (Extracted pages from 2022-07-22 - PICO-500 PV drawings.pdf, 2.5 MB)	
• (2H) Final seismic analysis (new suspension design) (21180f-1 R2.pdf, 6.7 MB)	
• (2I) Final seismic analysis addendum (compression case with no pressure) (2024-09-30 - PICO-500 suspension PVEng lug local study...pdf, 496.8 kB)	
• (2J) Scope definition for PVEng final seismic analysis (2024-07-05 - PICO-500 PVEng Scope.pdf, 109.1 kB)	
• (3A) Design reference sheets (amendments to specifications) (PICO-500 PV Design Reference Sheet.pdf, 145.7 kB)	
• (3B) Final technical specifications (Pressure Vessel Specifications Final.docx, 72.1 kB)	
• (3B) Final technical specifications (PDE) (Pressure Vessel Specifications Final.pdf, 343.8 kB)	
• (3C) Design specification drawings (Queens Pressure Vessel Design data.pdf, 1.6 MB)	
• (3D) RFP addendum questions and answers (RFP Q-2020-044-SM Addendum #2.pdf, 298.9 kB)	
• (4A) TSSA registration letter for PV (05-ON-R8904.5 LTR.pdf, 94.4 kB)	
• (4B) TSSA registration drawing for PV (05-ON-R8904.5 DWG.pdf, 8.6 MB)	
• (4C) TSSA registration letter for sight window (0F9637.5ADD12 Registration Letter and Statutory Declar...pdf, 1.6 MB)	
• (4D) TSSA registration letter for PV attachments (Specialty Alloys, 20230918_132722.pdf, 1.4 MB)	
• (4E) TSSA registration letter for Dvtran and Pall purifier (General Registration Letter - 14607374.pdf, 202.4 kB)	
• (4F) TSSA registration scope for Dvtran and Pall purifier (5 - 19592s-1 R0 ACCEP1610.pdf, 261.2 kB)	
• (4G) Manufacturers Data Report for PV (2025-10-27 - 2025QUEENS UNIVERSITY PICO 500 MDR.pdf, 1.1 MB)	
• (5A) Sight glass assembly instructions (PICO-500 Sight Glass Assembly Instructions Rev 2.pdf, 2.7 MB)	
• (5B) Fused silica disc material documentation (PICO-500 quartz disc documentation.pdf, 3.9 MB)	
• (5C) List of materials and heat numbers used to make the PV (PV Material List.JPG, 2.5 MB)	
• (5D) PICO-500 NDE Reports (PICO-500 NDE Reports.pdf, 3.4 MB)	
• (5E) Documentation allowing substitution of bolt: 1.5"-12tpi with 1.5"-8tpi (2024-07-23 - PICO-500 PV bottom flange 1.5 bolt substi...pdf, 19.8 MB)	
• (5F) Material screening summary (2024-10-08 - PICO-500 PV Material Screening Summary.pdf, 116.1 kB)	
• (5G) SAS Weld QA Documents (2024-11-19 - SAS Weld QA Documents.pdf, 3.6 MB)	
• (5H) PV Nameplates (2025-09-25 - PICO-500 PV Nameplates.pdf, 8.8 MB)	
• (5I) PV hydrotest pressure memo (2025-09-23 - PICO-500 PV Hydrotest Pressure Monitoring.pdf, 397.1 kB)	
• (5J) PV leak checking procedure with markups (Completed - PICO-PFH-DET-2011 Rev 0 - PV Leak Checking...pdf, 1.2 MB)	
• (5K) Thoughts on PV leak rate (2025-07-15 - Thoughts on PV leak rate.pdf, 112.6 kB)	
• (5L) PV attachments pressure test certificate (Specialty Alloys, 20251106_152237.pdf, 248.7 kB)	
• (6A) PV Assembly Map - Fittings, Nozzles, and Fasteners (PICO-PFH-DET-2006_Rev_F - PICO-500 PV fastener and sea...pdf, 335.8 kB)	
• (6B) PV fastener and seal list (PICO-PFH-DET-2006 Rev 0 - PICO-500 PV fastener and sea...pdf, 383.4 kB)	

PICO-500



- PV contract, design, registration
- Fluid carts
- Field Piping
- Cold plate
- Insulation & heaters*
- R.R.s & C.C.s*
- ... and more

*See **William's** talk this afternoon*

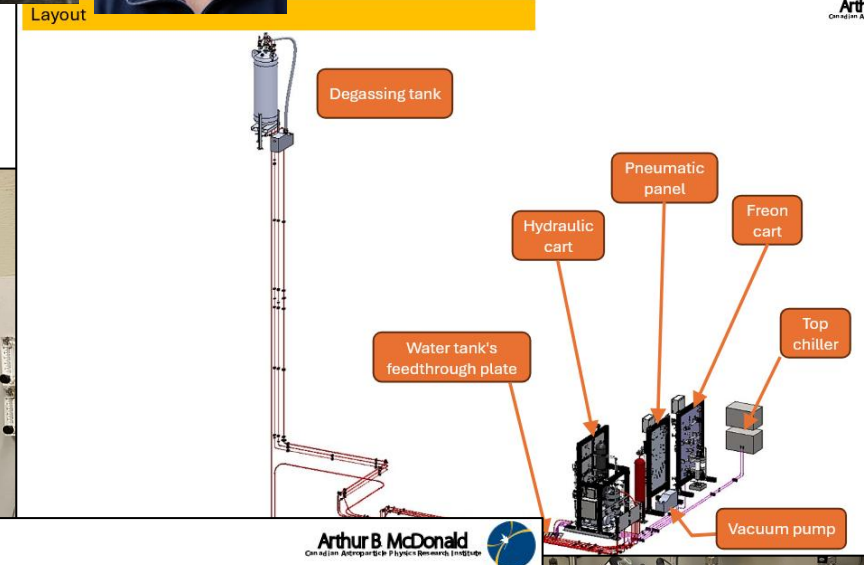


PICO-500



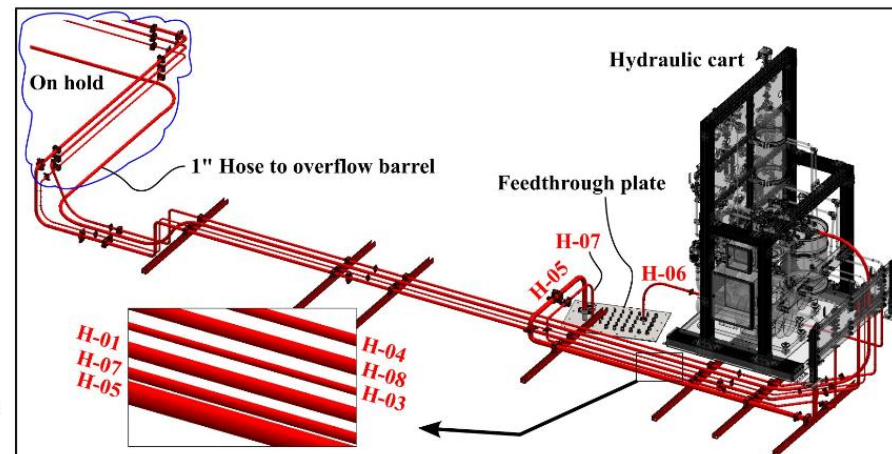
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- ... and more

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Organization of piping

- Between Hydraulic Cart & Water Tank Feedthrough Plate & Degassing Tank



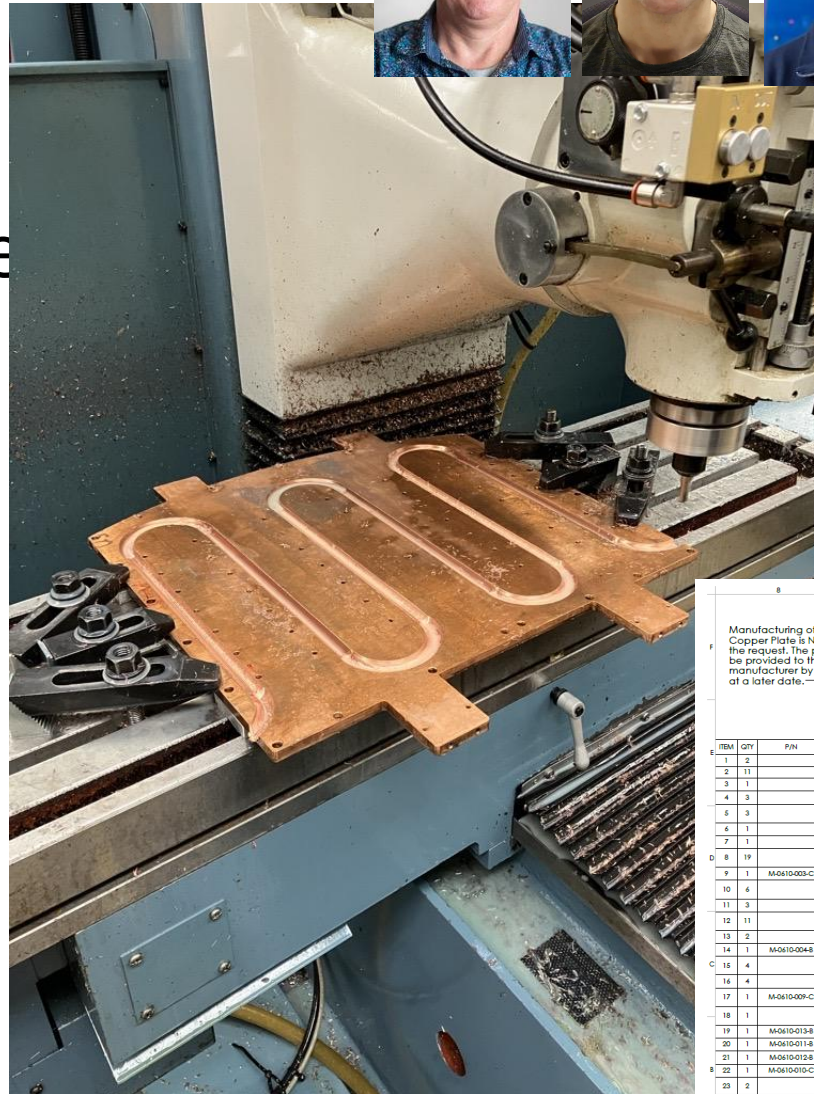
- ½", ¾", 1" & 1-½" size
- SS tubing + drain hose
- Tri-clamp fittings



PICO-500

- PV contract, design, re
- Fluid carts
- Field Piping
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- Insulation & heaters*
- R.R.s & C.C.s*
- ... and more

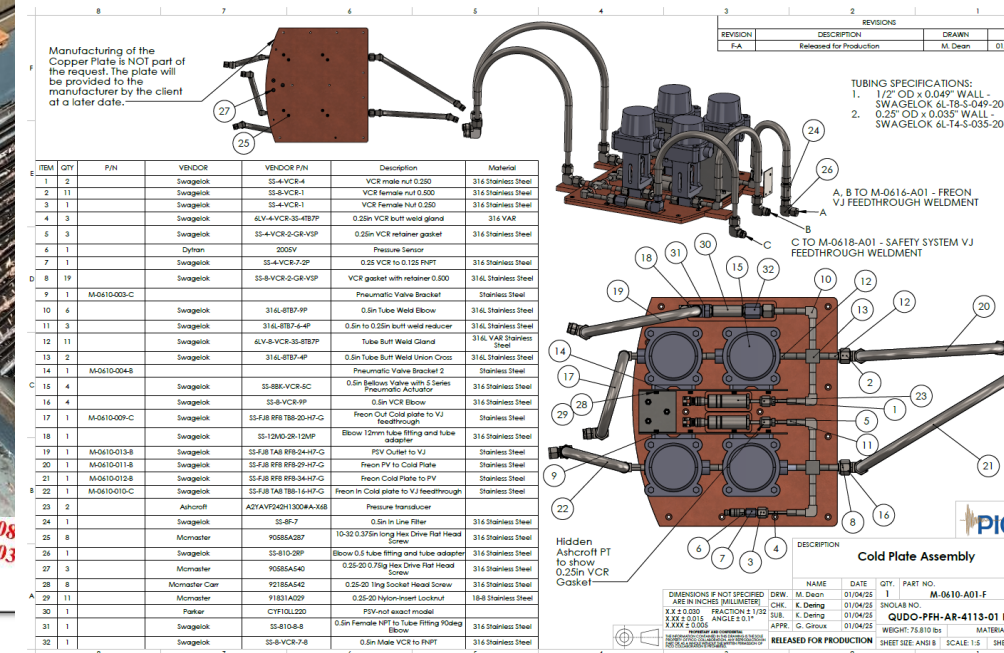
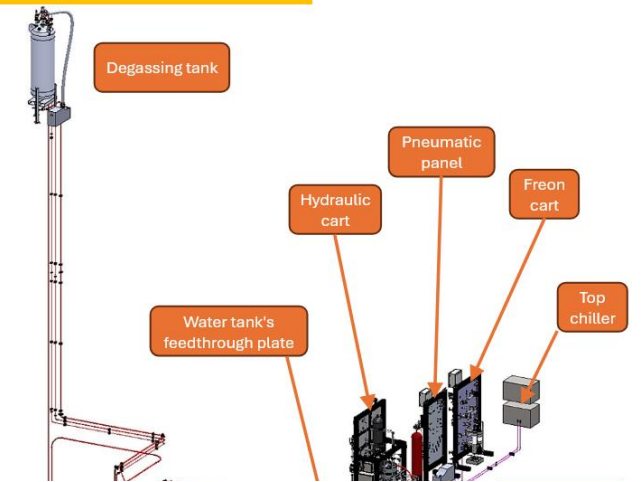
*See **William's** talk this afternoon*



- ½", ¾", 1" & 1-½" size
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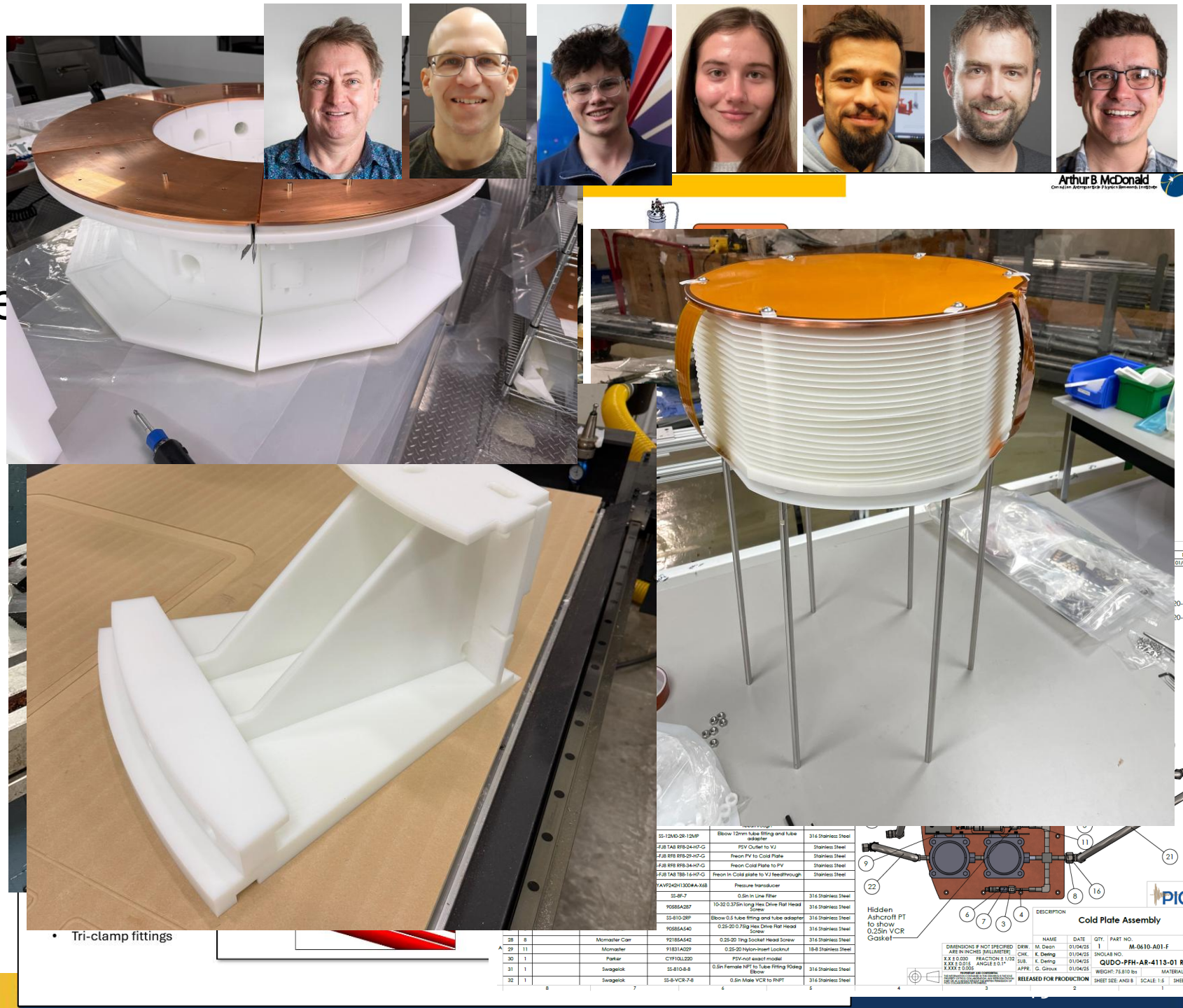
Arthur B. McDonald
Operation Astrophysics Physics Learning Institute



PICO-500

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- R.R.s & C.C.s*
- ... and more

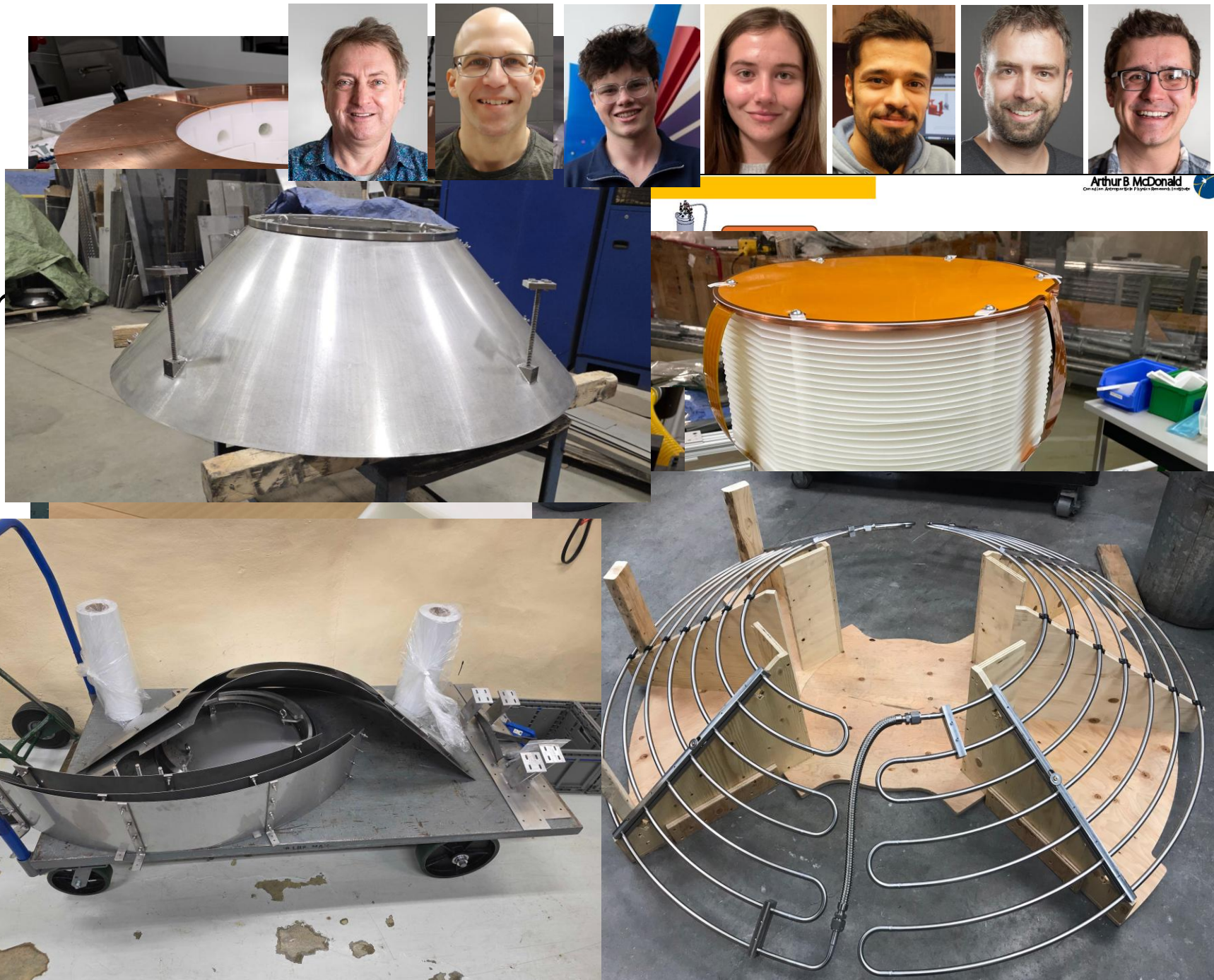
*See **William's** talk this afternoon*



PICO-500

- PV contract, design, m
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- ... and more

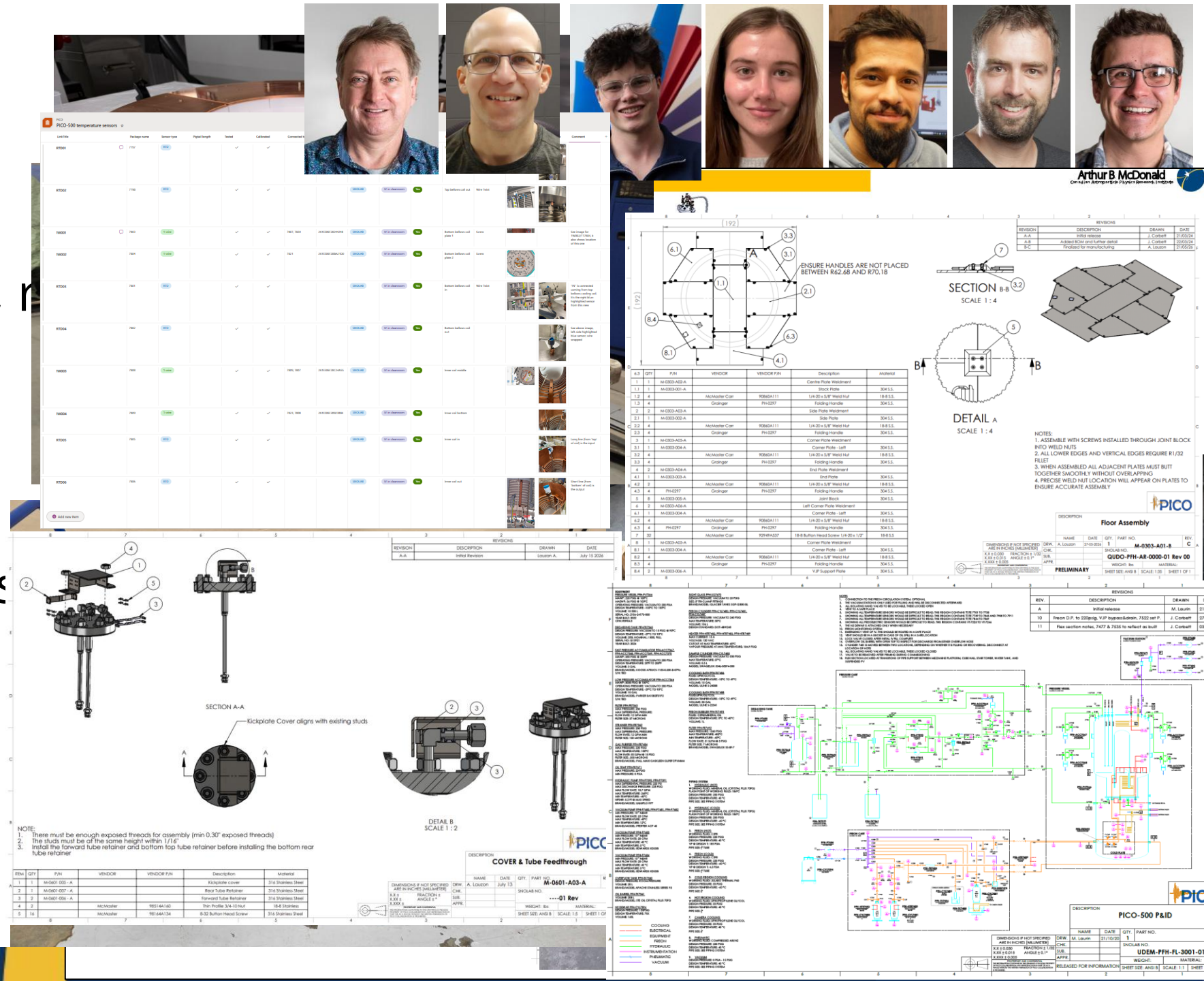
*See **William's** talk this afternoon*



PICO-500

- PV contract, design, mfg
- Fluid carts
- Field Piping
- Cold plate
- Insulation & heaters
- R.R.s & C.C.s*
- ... and more

*See **William's** talk this afternoon*



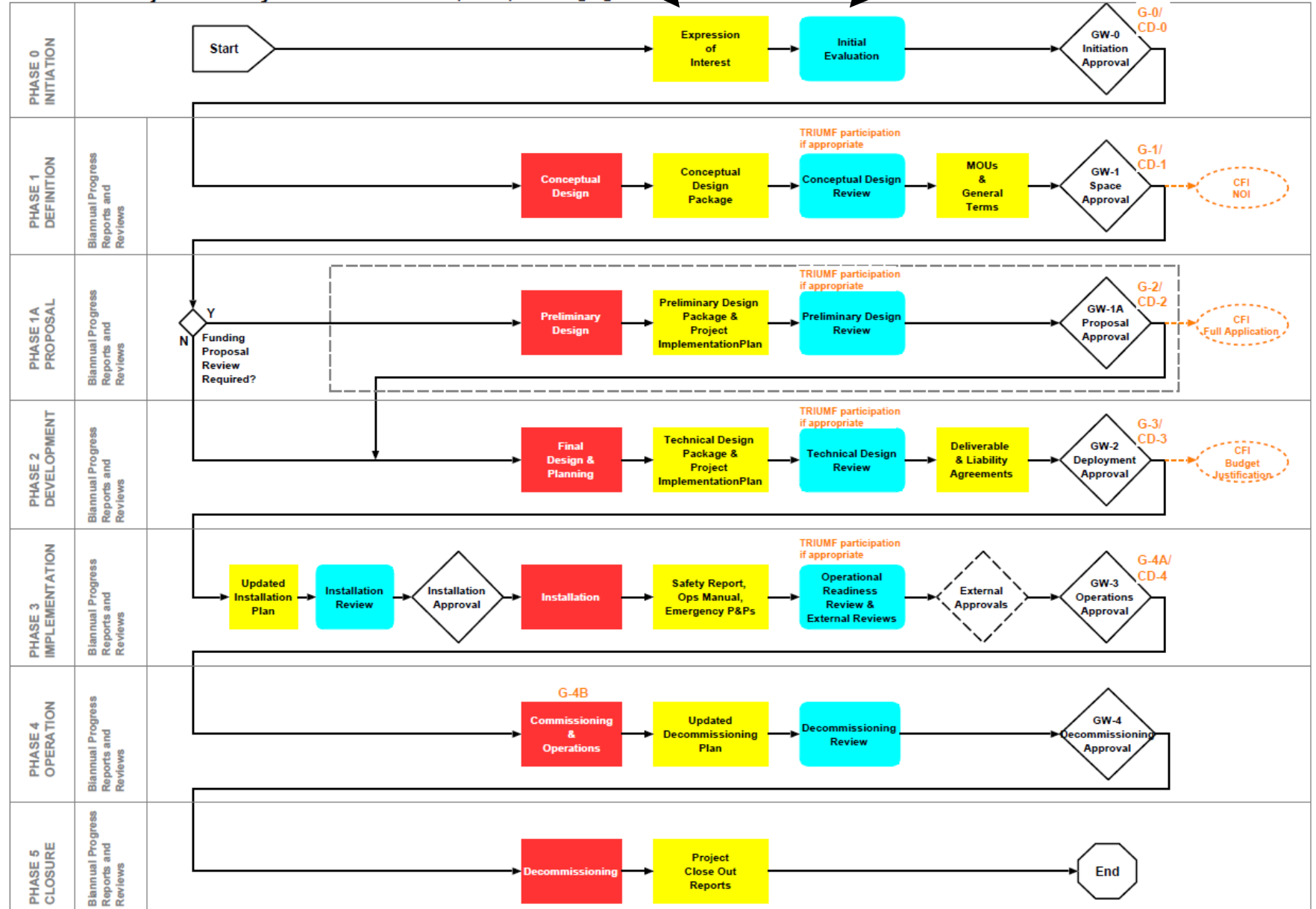
SNOLAB Project Life Cycle

I've seen/participated in this process, but for multi-year design processes!

Requires good organization, project management, detail focus and methodical follow up

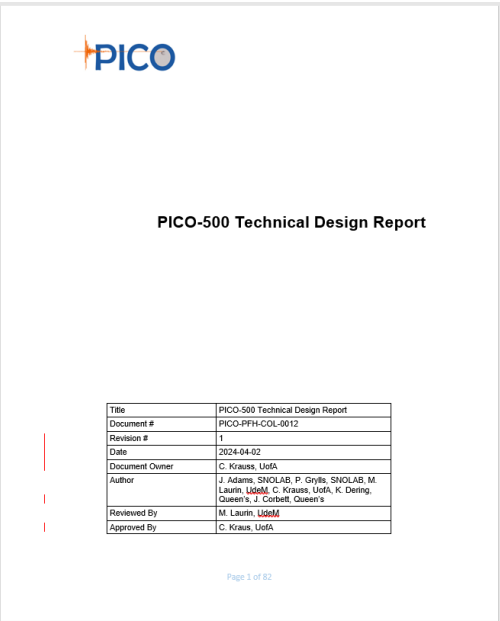
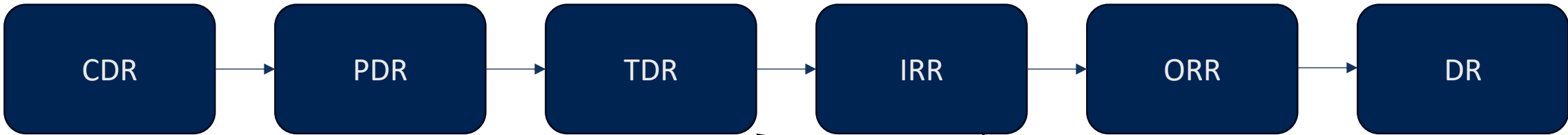
SNOLAB Project Life Cycle

SL-SCI-RES-80-001-F01-Project-Life-Cycle-Flowchart_Rev_01





Queen's-IPDC GW Involvement



File Number	Name	Folder	Last Update	Responsible	Done	Uploaded
PICO-PFH-COL-0012	PICO-500 TDR	Top Level	TDR	Jonathan	Yes	Yes
PICO-PFH-DET-0013	Initial installation plan	Technical Documents	TDR	Jonathan	Yes	Yes
	PV 2D drawing package	Technical Drawings	TDR	SAS/Paul	Yes	Yes
	IV quartz 2D drawing package	Technical Drawings	PDR		Yes	Yes
	IV 2D drawing package	Technical Drawings	TDR	Mitch	Yes	Yes
PICO-PFH-DET-8000	Background simulation	Technical Documents	PDR		Yes	Yes
PICO-PFH-DET-3001	Pressure vessel overpressure protection	Technical Documents	TDR	Koby	Yes	Yes
PICO-PFH-DET-2000	PICO-500 pressure vessel specification	Technical Documents	PDR	Koby	Yes	Yes
	PV documentation (PVEng code calcs, drawings, QA)	Technical Drawings	PDR	Koby	Yes	Yes
PICO-PFH-DET-1005	Seal and clamping design	Technical Documents	PDR	Koby	Yes	Yes
PICO-PFH-DET-1004	Jar and seal design	Technical Documents	PDR	Koby	Yes	Yes
UDEM-PFH-FL-3001	PICO-500 P&ID	Technical Drawings	TDR	Jonathan	Yes	Yes
PICO-PFH-DET-0011	PICO-500 Master equipment list	Equipment & Utilities	TDR	Mathieu	Yes	Yes
PICO-PFH-DET-4001	PICO-500 Thermal simulation report	Technical Documents	PDR	Carsten	Yes	Yes
PICO-PFH-DET-6600	PICO-500 Control and acquisition system	Technical Documents	PDR	Mathieu	Yes	Yes
UDEM-PFH-SK-0010	PICO-500 floor plan	Technical Drawings	TDR	Mathieu	Yes	Yes
	Cube hall deck study report (Makami)	Technical Documents	PDR		Yes	Yes
	2020-08-24 - PICO 500 Tank Seismic Memo	Technical Documents	PDR		Yes	Yes
PICO-PFH-DET-0100	PICO-500 utility requirements	Equipment & Utilities	PDR	Mathieu	Yes	Yes
PICO-PFH-DET-1006	IV seismic	Technical Documents	PDR		Yes	Yes
PLC-SNOLAB-P2046-PICO-500-FHA-0	PICO-500 Fire hazard assessment	Technical Documents	PDR		Yes	Yes
PLC-QueenU-P2350-PICO-500-FHA-0	PICO-500 Fire hazard assessment review	Technical Documents	TDR		Yes	Yes
PICO-PFH-DET-0015	PICO-500 Commissioning Fire assessment	Technical Documents	TDR	Koby	Yes	Yes
	HAZOP report	Risk and Hazard	PDR		Yes	Yes
	SNOLAB PICO-500 Project Budget	Project Management	TDR	Paul	Yes	Yes
	PICO-500 Schedule	Project Management	TDR	Paul	Yes	Yes
	Hazard table	Risk and Hazard	PDR		Yes	Yes
PICO-GEN-COL-9005	EDI	EDI & Code of Conduct	TDR	Jeremy	Yes	Yes
PICO-PFH-DET-0010	PICO-500 HAZOP	Risk and Hazard	PDR		Yes	Yes
PICO-PFH-DET-0700	PICO-500 ODH analysis	Risk and Hazard	PDR		Yes	Yes
PICO-PFH-DET-0701	PICO-500 ODH calculation	Risk and Hazard	PDR		Yes	Yes
SLDO-PFH-AR-0402	PICO-500 PV Placement Overview	Technical Drawings	PDR	Paul	Yes	Yes
SLDO-PFH-FL-0600	PICO-500 Shield Tank Circulation and Purification Flowsheet	Technical Drawings	PDR	Paul	Yes	Yes
SLDO-PFH-E-0100	PICO-500 Utilities Electrical Installation Package	Technical Drawings	PDR	Paul	Yes	Yes
SLDO-UGL-E-4105	SNOLAB Single Line Diagram Ladders Labs 413-MCC-04	Technical Drawings	PDR	Paul	Yes	Yes
SLDO-UGL-FL-1200	Forced Draining P&ID	Technical Drawings	PDR	Paul	Yes	Yes
SLDO-UPW-FL-0106	New Lab Area UPW Distribution Flowsheet	Technical Drawings	TDR	Paul	Yes	Yes
SLDO-UGL-FL-2009	Compressed Air System Flowsheet for New Lab Area	Technical Drawings	PDR	Paul	Yes	Yes
PICO-PFH-COL-0002	Project charter	Project Management	TDR	Paul		
PICO-GEN-COL-0002	QA Management Plan	Project Management	TDR		Yes	Yes
PICO-GEN-COL-9000	Code of conduct	EDI & Code of Conduct	PDR		Yes	Yes
PICO-PFH-DET-0017	PICO-500 Run plan	Project Management	PDR	No Change	Yes	Yes
PICO-PFH-DET-0014	PICO-500 decommissioning plan	Project Management	PDR	No Change	Yes	Yes
PICO-PFH-DET-5000	PICO-500 Fluid Systems	Technical Documents	TDR	Mathieu	Yes	Yes
PICO-PFH-DET-4000	PICO-500 Heaters	Technical Documents	TDR	Michael	Yes	Yes
PICO-PFH-DET-6601	Alarms & Interlocks	Technical Documents	TDR	Mathieu	Yes	Yes
	Itaska 2023 Seismicity Data	Technical Documents	TDR		Yes	Yes
PICO-PFH-COL-9000	PICO-500 WBS	Project Management	TDR	Paul	Yes	Yes
PICO-PFH-DET-2004	Welding Cleanliness Procedure	Project Management	TDR	Mel	Yes	Yes
PICO-PFH-DET-2005	PV Logistics Plan	Project Management	TDR	Mel	Yes	Yes
PICO-PFH-COL-0005	PICO-500 Risk Management Plan	Risk and Hazard	TDR	Paul	Yes	Yes
PICO-PFH-COL-0006	PICO-500 Hazard Management Plan	Risk and Hazard	TDR	Paul	Yes	Yes
PICO-PFH-COL-0008	PICO-500 Project Hazard Register	Risk and Hazard	TDR	Paul	Yes	Yes
PICO-PFH-COL-0016	PICO-500 Risk Register	Risk and Hazard	TDR	Paul	Yes	Yes

From Aug 2025-Present our team helped prepare documentation for/presented at...

3x of these

1x of these

Example of a document submittal list (PICO-500 TDR)

... and >150 2D drawings



PICO-500 Fluid systems

Title	PICO-500 Fluid systems
Document #	PICO-PFH-DET-5000
Revision #	0
Date	2024-03-11
Document Owner	Guillaume Giroux, Queen's
Author	Guillaume Giroux, Queen's, Mathieu Udem, Jonathan Corbett, Queen's, Adams, Queen's, Mackenzie Dean, Queen's, Madelyn Bratuz, Queen's
Reviewed By	Koby Dering, Queen's
Approved By	Guillaume Giroux, Queen's

2 Hydraulic system

The hydraulic control system is an essential part of the PICO-500 detector. This system is responsible for controlling the pressure of the pressure vessel, and thus the freon pressure. It is also used for detector filling and draining. It consists of a hydraulic cart, a degassing tank, 4 fast pressure accumulators (FPA), and one low pressure accumulator (LPA). Since this system uses STE Crystal Plus 70FG mineral oil under 250 g/gig and 150 °F, it complies with TSSA exception O. Reg. 220/01 2.2(e) regarding the use of "Liquid no more hazardous than water", meaning the system, with some equipment exceptions described below, doesn't require TSSA registration. PICO-40L previously retained PVEng for a professional opinion of the applicability of this exemption for mineral oil, and PVEng agreed that the piping system conveying mineral oil is exempt. The accumulators (low pressure accumulator and fast pressure accumulators) will have a CRN.

During operation the general sequence of steps requires priming the freon in the PV in its superheated state, at a low pressure (nominally around 25 psia) with a 2-stage expansion; a gross expansion directly to the degassing tank followed by a slower careful expansion into the LPA. When an event occurs, there is a rapid compression of the PV from the FPAs followed by pumping which resets the FPAs and brings the PV back up to its fully compressed state. The cycle then repeats to prepare the detector for another event. This sequence is summarized in Figure 1 below where the degassing tank is referred to as the storage tank.

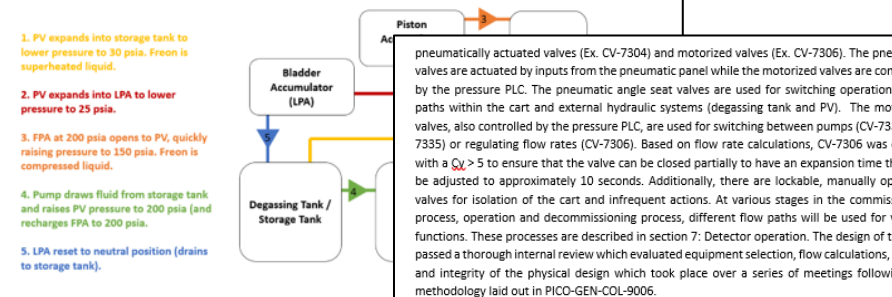


Figure 1 Compression cycle sequence summary.

2.1 Hydraulic cart

The hydraulic cart contains elements that control the movement of the pressure vessel during all stages of the project lifecycle. Elements on the cart include a bladder accumulator, filters, and sensors. The hydraulic cart will be brought to SNOLAB as one assembled package, just needing to become integrated to the experiment. Several types of valves

are pneumatically actuated valves (Ex. CV-7304) and motorized valves (Ex. CV-7306). The pneumatic valves are actuated by inputs from the pneumatic panel while the motorized valves are controlled by the pressure PLC. The pneumatic angle seat valves are used for switching operational paths within the cart and external hydraulic systems (degassing tank and PV). The motorized valves, also controlled by the pressure PLC, are used for switching between pumps (CV-7334, CV-7335) or regulating flow rates (CV-7306). Based on flow rate calculations, CV-7306 was chosen with a $C_v > 5$ to ensure that the valve can be closed partially to have an expansion time that is adjusted to approximately 10 seconds. Additionally, there are lockable, manually operated valves for isolation of the cart and infrequent actions. At various stages in the commissioning process, operation and decommissioning process, different flow paths will be used for various functions. These processes are described in section 7: Detector operation. The design of the cart has passed a thorough internal review which evaluated equipment selection, flow calculations, layout, and integrity of the physical design which took place over a series of meetings following methodology laid out in PICO-GEN-COL-9006.

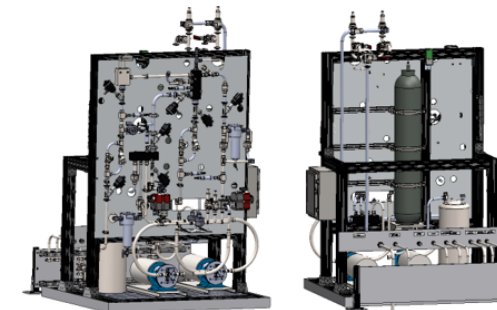


Figure 2 Hydraulic cart preliminary CAD model. Front and back views.

2.1.1 Pump Assembly

The hydraulic cart contains two magnetic drive gear pumps to fill/empty, cycle, and gradually increase pressure of the system when needed. Although two pumps are available, only one pump will be used at a time. The pumps are connected in parallel using two 3-way motorized valves with which a switching relay circuit will forbid both pumps from running at the same time. In the event of a pump failure happens, the system can easily (and remotely) be switched over to the second pump by actuating motorized valves without significantly delaying operational time. The relay circuit has been designed to prevent improper operation of the valves and pumps, like wrong valve

7 Detector operation

Final flow path drawings for each of the operations will be produced and reviewed at the time of the Operations Readiness Review, but the following gives an overview of the anticipated detector operations.

7.1 Detector fill

The order of the subsequent steps are listed in the rough sequencing order, however some steps can happen in parallel, and may be subject to change after a more thorough review is done at the time of the Operations Readiness Review.

7.1.1 Vacuum

The filling process begins at the hydraulic cart. All lines will be vacuum pumped to prepare the detector for filling. For the degassing tank, hydraulic cart and PV this is pumped through CV-7634 at the degassing tank, through V-7630 on the PV directly, and for the freon system through V-7636. To vacuum prime the system, all valves on the hydraulic and freon carts and valves on the PV are open except the ones listed below. Note that this implies all pneumatic normally closed valves must be actuated to be open. The 3-way valves in the systems (V-7315, V-7334, V7335) will be cycled between their different states to ensure that vacuum is adequately pulled in all volumes. Vacuum pumps are then run until the pressure is on the order of 10^{-2} mbar. Pumps are shut off and all remaining valves closed.

Hydraulic System closed valves: V-7300, V-7301, V-7307, V-7312, V-7313, V-7317, V-7333, V-7336, V-7337, V-7338, V-7345, V-7635

Freon System closed valves: V-7452, V-7453, V-7457, V-7463, V-7464, V-7465, V-7466, V-7471, V-7472, V-7473, V-7477, V-7637

7.1.2 Degas tank fill and initial oil filtration

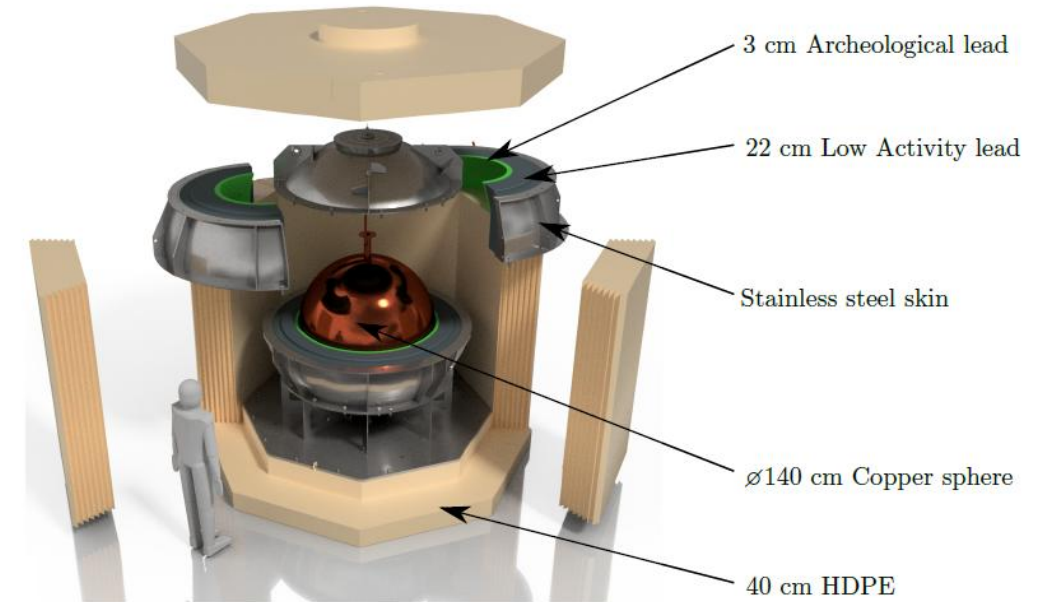
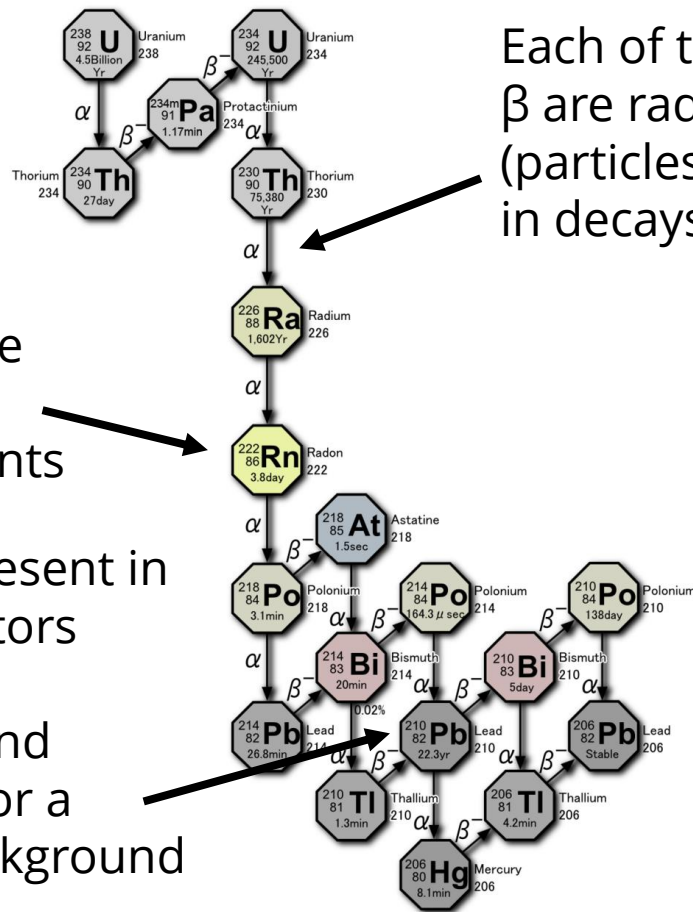
The degassing tank is filled from an oil barrel using the pump, strainer, and filter on the hydraulic cart. The strainer filters the oil of particulates greater than 149 microns before it enters the pump. After the pump, oil is filtered a second time to 25-micron purity before travelling to the degas tank. The capacity of one oil barrel should completely fit inside the degas tank which has a capacity of approximately 250 L. This is done while continuously degassing with the vacuum pump on the degassing tank. The transfer will end before the oil level in the barrel reaches the intake tube to prevent accidental suction of lab air into the hydraulic cart.

Level transducer LT-7219 monitors the oil level in the degas tank and PT-7601 monitors the pressure. Additionally, level threshold sensors LS-7249 (top) and LS-7250 (bottom) will trigger alarms indicating if the oil level becomes too high or too low. The vacuum pump will continue to degas the oil until the pressure reaches the oil vapour pressure.

Lots of documentation

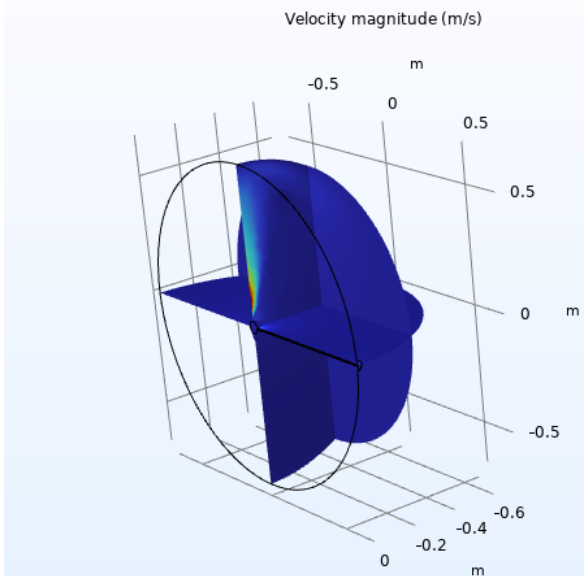
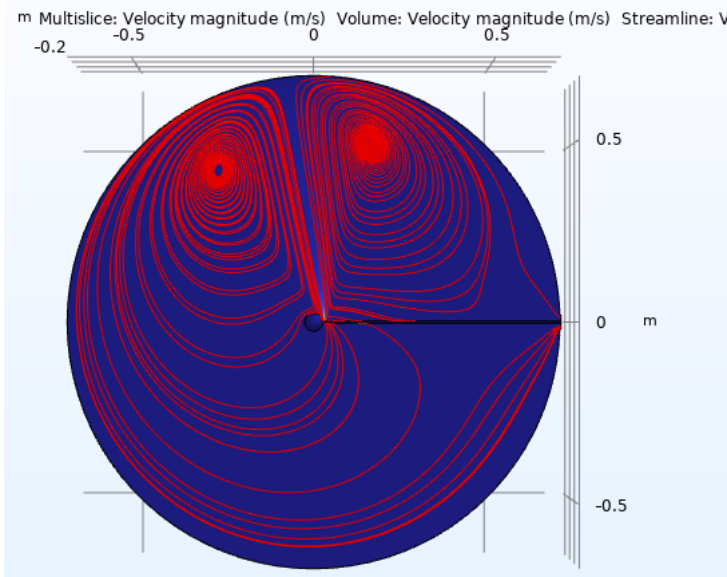
NEWS-G Radon Removal

*UG Rn concentration is $\sim 100 \text{ Bq/m}^3$ (decays/s/m³)

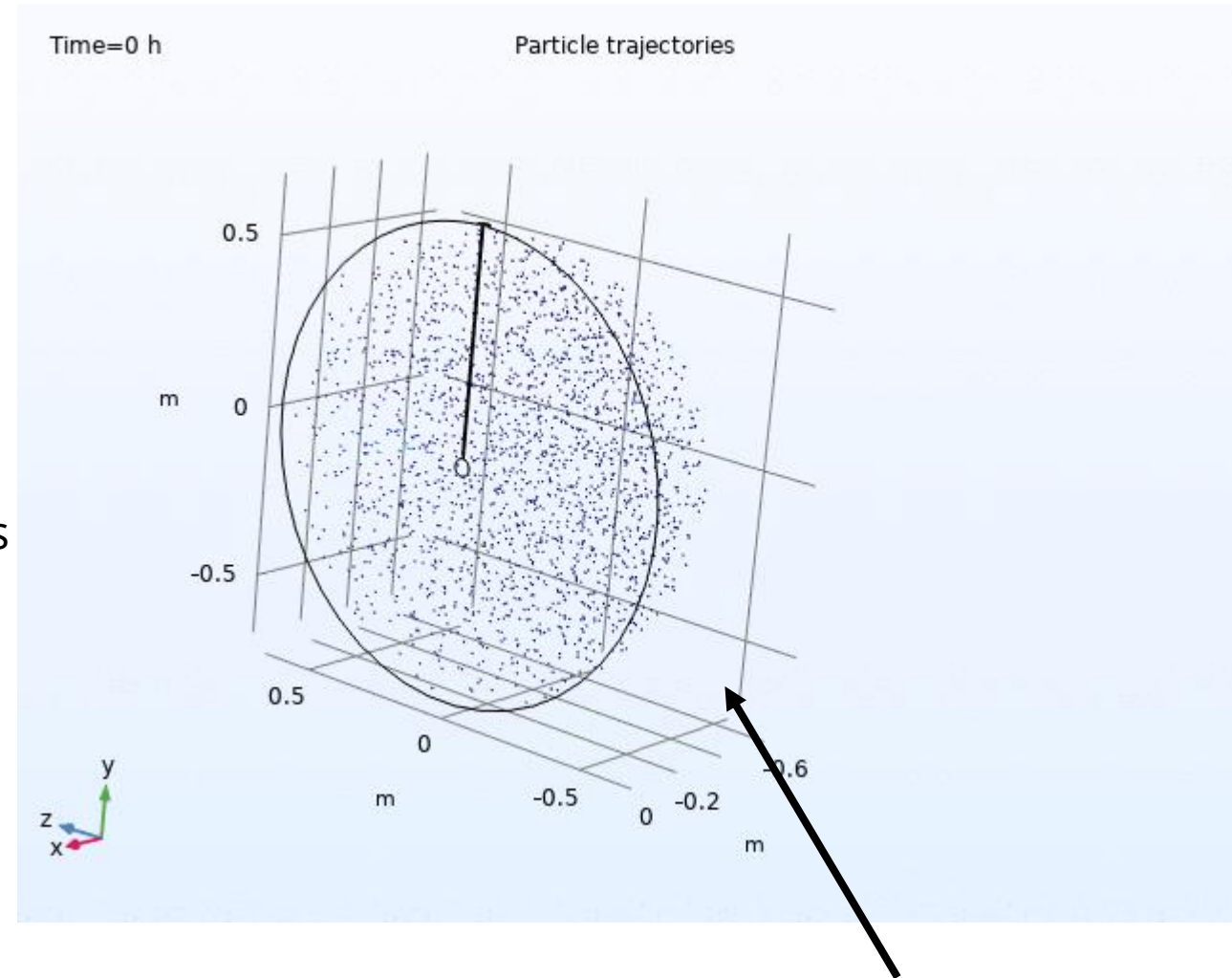


Experiments build shielding to protect detectors from *external* radiation. Many efforts (cleaning/etching surfaces) to reduce particle decays coming from within

NEWS-G Radon Removal



Current progress:
Model existing
experiment
recirculation
method, how
effective is it at
removing particles
from inside?



Next steps: What modifications can we make to design to improve that

Fabrication & Assembly

IPDC Members!



These guys would have appeared on pretty much *every* slide with fabrication. They are integral part of our ability to deliver. Thank you Jeff, Rob, Pat, and Chuck (retired)

Machine Shop

- Machining services available at Queen's shop supporting MI-AP projects
 - **Not currently charging for time**
 - Billing for materials and consumables
 - Prioritization based on current shop load, suitability, requested schedule – fold this into the management responsibilities for IPDC
- CNC mill/lathe, some welding, manual tools (mill, lathe, drill press, bandsaw, shear, press brake, press), 3D printer, water jet
- Reach out for details



Deckel DMU 50T CNC Mill

- 3 axis plus 2 milling machine
- 3 axis (XYZ) controlled by CNC and 2 axis of table can be manually rotated
- Capable of machining parts 19.5 inches x 15.75 inches and 17 inches in height
- Spindle RPM range of 10 to 9000 RPM
- Automatic tool changer holds 16 tools
- Well suited to producing multiple intricate parts



ProtoTrak RMX DPM RX5 CNC Mill

- 3 axis milling machine
- Combination of a conventional mill and a CNC
- Programmed by Mastercam or Trak software at the controller
- Capable of machining parts 40 inches x 20 inches and 20 inches in height
- Spindle RPM range of 40 to 5000 RPM
- Max of 400IPM in X and Y axis table movements. Z axis 250 IPM max



ProtoTrak RLX CNC Lathe

- Combination of a conventional lathe and a CNC
- Programmed by Mastercam or Trak software at the controller
- 18" diameter swing and 40" length. 9.0" diameter round parts at full working length
- Spindle through hole 2.36" diameter
- 10 hp motor with a max of 2500 RPM



Teaching/Consulting student projects, mentoring, lab work, L0

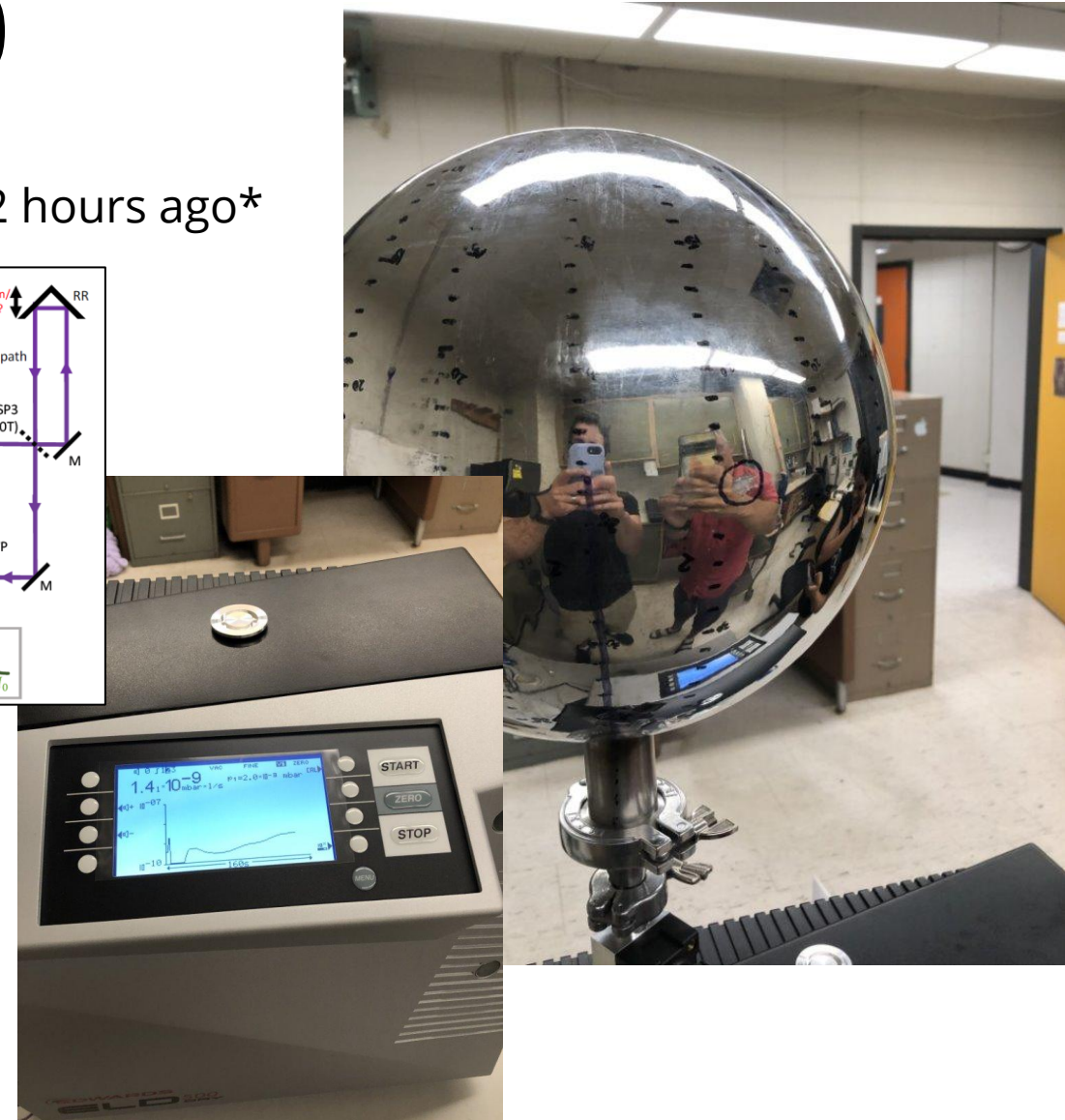
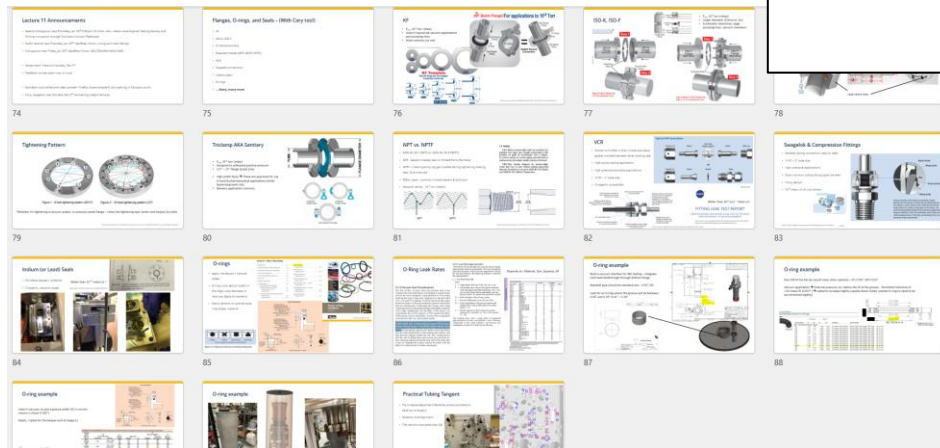
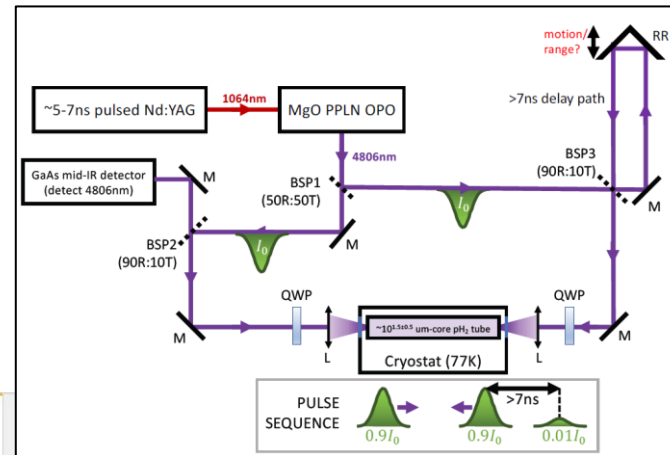
ENPH 459: Practical Cryogenic Engineering

Jonathan Corbett

Winter 2026



*See **Avani's** talk 2 hours ago*





Arthur B. McDonald

Canadian Astroparticle Physics Research Institute





Thank you

Contact me at: jtc7@queensu.ca

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