

Multiplexed read out for low threshold detectors in astroparticle physics

Microwave SQUID multiplexing (uMUX) for massive cryogenic bolometers

N. Ferreiro Iachellini (unimib & INFN MiB nahuel.ferreiro@mib.infn.it)

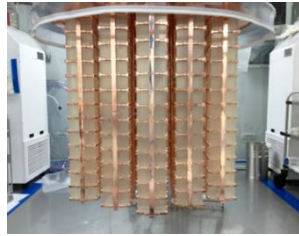
Bicoq 16.06.26

Three Physics Targets — Two Very Different Energy Scales

Neutrinoless Double Beta Decay

RoI ~ MeV

- Q-value of isotope sets the RoI: ^{130}Te at 2.528 MeV Ton-scale experiments running: CUORE (760 kg TeO_2)
- Wired readout adequate at this scale -> SOLVED

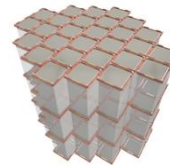


Ton scale: achieved

Coherent Elastic ν -Nucleus Scattering

RoI ~ few keV

- Rate proportional to N^2 — heavy nuclei ideal (Pb, Bi: $N=126$)
- Solar/SN neutrinos -> $O(0.1 - 1 \text{ keV})$ nuclear recoils
- Need $O(100 - 1000 \text{ kg})$, hundreds of channels at mK
- Wired readout cannot scale -> bottleneck

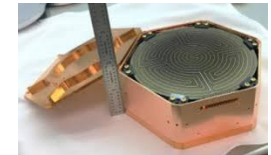
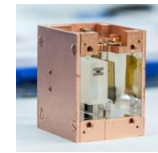


keV scale: readout limited

Sub-GeV Dark Matter

RoI ~ sub-keV to few keV

- Rate proportional to A^2 — coherent nuclear recoil
- $1 \text{ GeV}/c^2 \text{ DM}$: $< 0.8 \text{ keV}$ recoil on O
- Same mass scale as CEvNS -> same readout problem



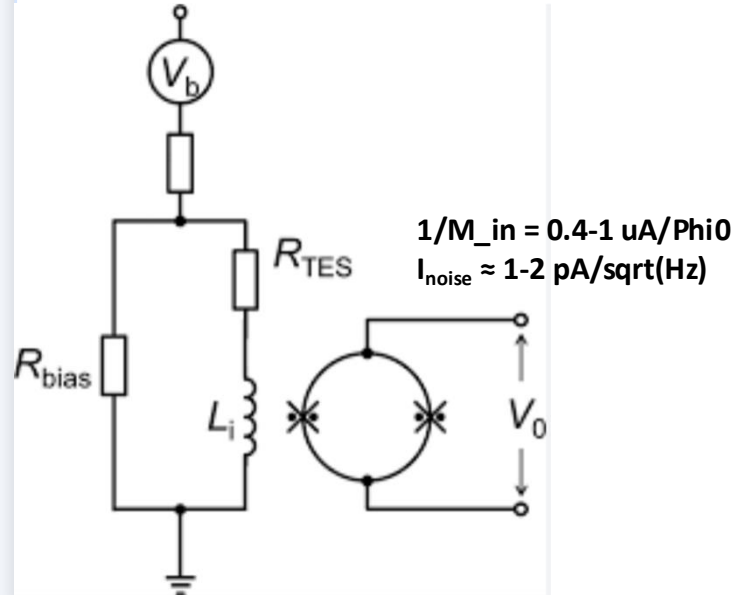
Sub-keV scale: readout limited

The Wiring Bottleneck: Conventional SQUID Readout

Problem: wire-limited SQUID readout

- 1 amplifier chain + several wires per channel
- Heat load & wire count limit arrays to ~10s of detectors
- Scaling to 100 - 1000 kg requires hundreds of channels
- Each wire = thermal load
- Wiring harness becomes the dominant engineering challenge

Simplified

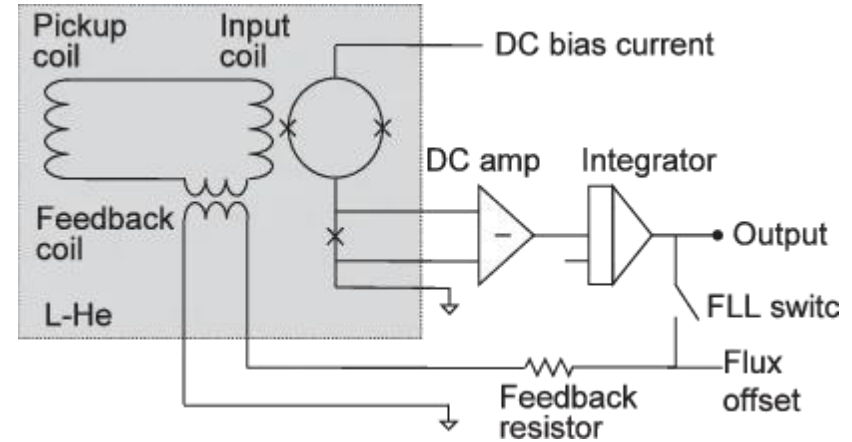


The Wiring Bottleneck: Conventional SQUID Readout

Problem: wire-limited SQUID readout

- 1 amplifier chain + several wires per channel
- Heat load & wire count limit arrays to ~10s of detectors
- Scaling to 10-100 kg requires hundreds of channels
- Each wire = thermal load
- Wiring harness becomes the dominant engineering challenge

Less simplified (still)



FLL limits the bandwidth: 1 channel -> 1 squid

The Wiring Bottleneck: Conventional SQUID Readout

Problem: wire-limited SQUID readout

- 1 amplifier chain + several wires per channel
- Heat load & wire count limit arrays to ~10s of detectors
- Scaling to 10-100 kg requires hundreds of channels
- Each wire = thermal load
- Wiring harness becomes the dominant engineering challenge

Solution: Microwave SQUID Multiplexing (uMUX)

- Each TES coupled to an rf-SQUID + high-Q resonator
- All resonators on ONE coaxial feedline
- One HEMT amplifier per array ($N_{\text{mux}} = 52-1000$)
- 4-8 GHz band: ~ 1300 resonators possible

uMUX: N wiring harnesses \rightarrow 1 coax + 1 HEMT \Rightarrow readout stops being the bottleneck

uMUX: Circuit Principle & Flux-Ramp Linearisation

TES -> rf-SQUID

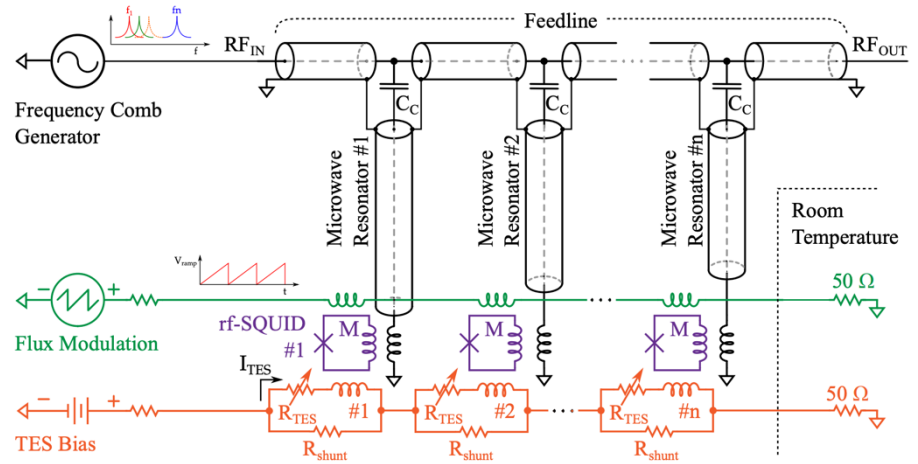
Signal current I_{TES} produces flux $\Phi = M_{\text{in}} * I$ in a dissipationless rf-SQUID. No resistive dissipation at the detector stage.

rf-SQUID -> Resonator

The SQUID acts as a tunable inductance, shifting the resonant frequency of a GHz superconducting resonator.

Flux-Ramp Demodulation

A sawtooth flux ramp drives the SQUID through $n_{\Phi_0} = 2$ flux quanta per period. The tone phase winds periodically; demodulation extracts the current sample at f_{ramp} .



$$1/M_{\text{in}} \sim 23 \text{ uA}/\Phi_0$$

HOLMES Collaboration • [D.T. Becker \(NIST, Boulder\)](#) et al.

e-Print: [1910.05217](#) [physics.ins-det]

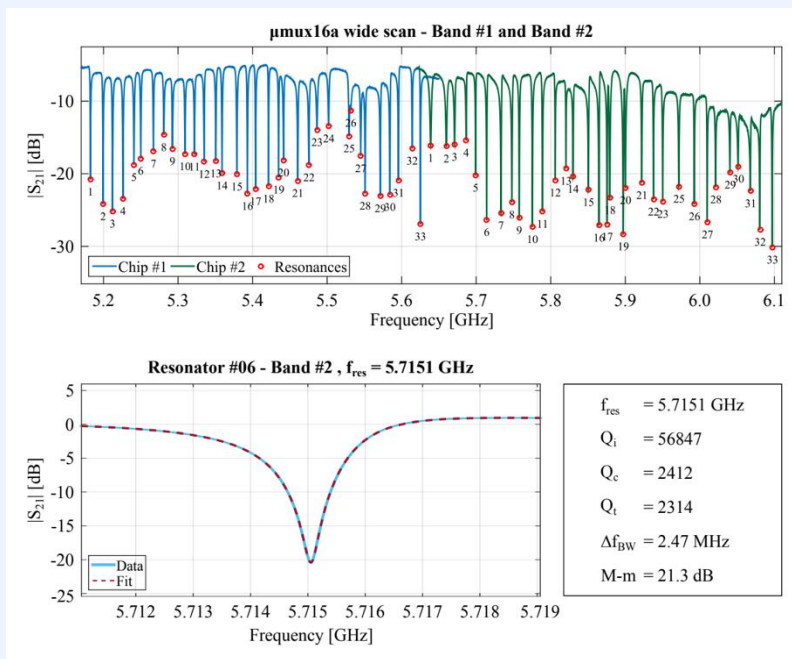
DOI: [10.1088/1748-0221/14/10/P10035](#) (publication)

Published in: JINST 14 (2019) 10, P10035

Frequency-Division: Lorentzian Resonances on a Shared Feedline

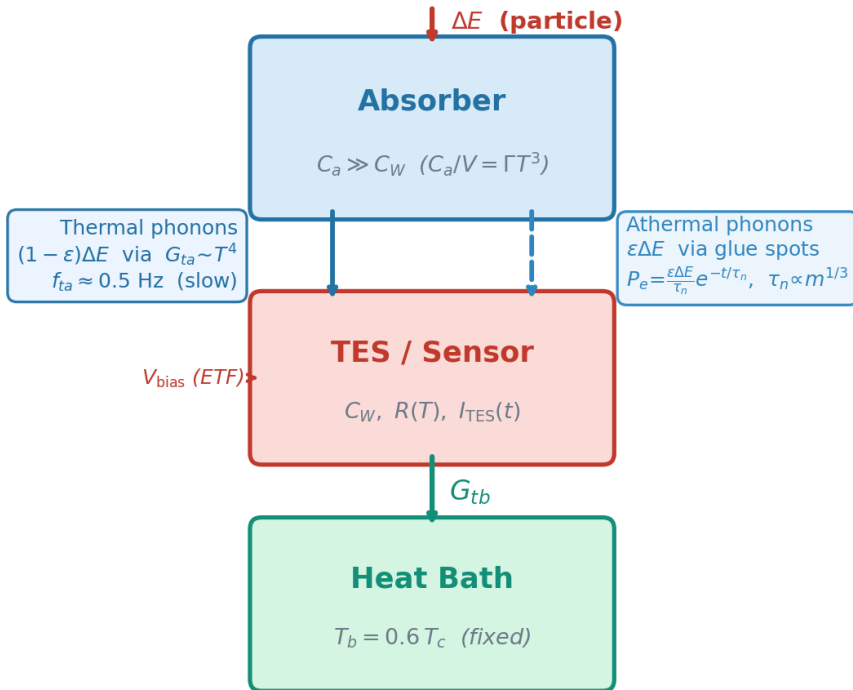
Reading the frequency comb

- Each resonator appears as a Lorentzian dip in $|S_{21}|$ vs frequency
- Resonance position f_0 shifts with TES current via rf-SQUID inductance
- bandwidth ~ 100 kHz at 4 GHz
- Channels spaced 3 MHz apart (30x bandwidth) \rightarrow negligible crosstalk
- 52-channel tower occupies only ~ 0.2 GHz of the 4-8 GHz HEMT band
- A 4 GHz band fits ~ 1300 resonators — ~ 20 towers on one readout line



Becker et al., JINST 14 P10035 (2019) — Fig. 8

The Thermal Model

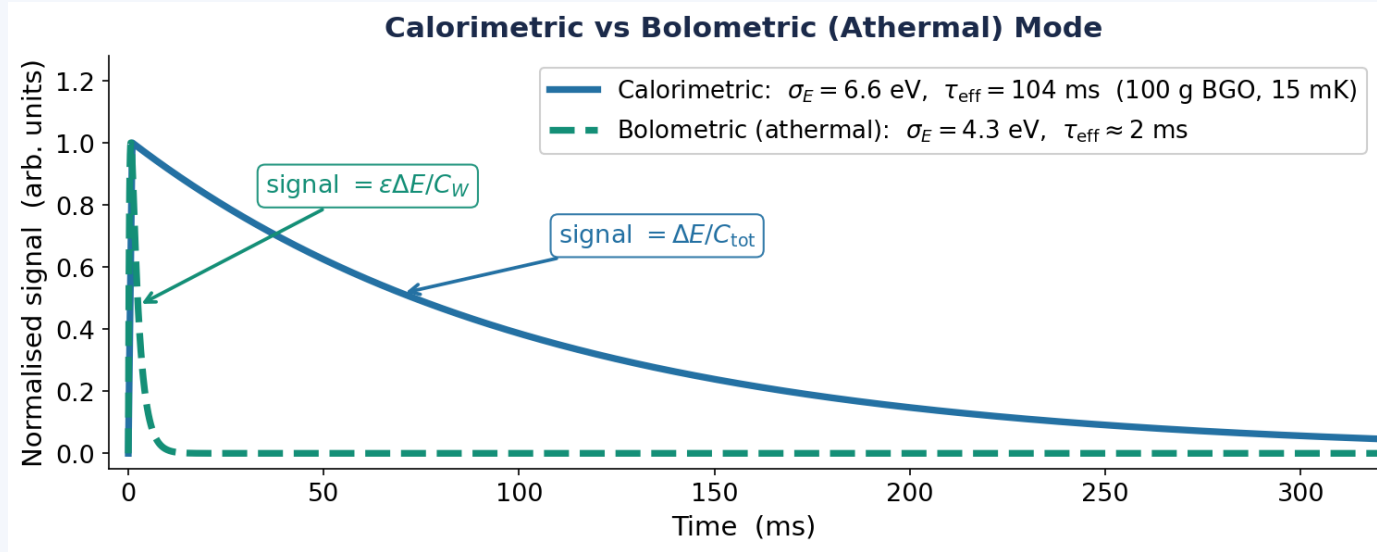


Coupled thermal equations (Pröbst, F., et al. *J Low Temp Phys* **100**, 69–104 (1995) and Pyle, M. e-Print: [1503.01200](https://arxiv.org/abs/1503.01200))

Athermal phonon

- $P_e(t) = (\epsilon \cdot \Delta E / \tau_n) \cdot \exp(-t/\tau_n)$ — power pulse to TES
- $\tau_n \propto m^{1/3}$ | $\epsilon =$ phonons thermalized in the TES
- Thermal remainder $(1-\epsilon)\Delta E$ via $G_{ta} \sim T^4$, $f_{ta} \sim 0.5$ Hz (slow channel)

Two Operating Modes: Bolometric vs Calorimetric



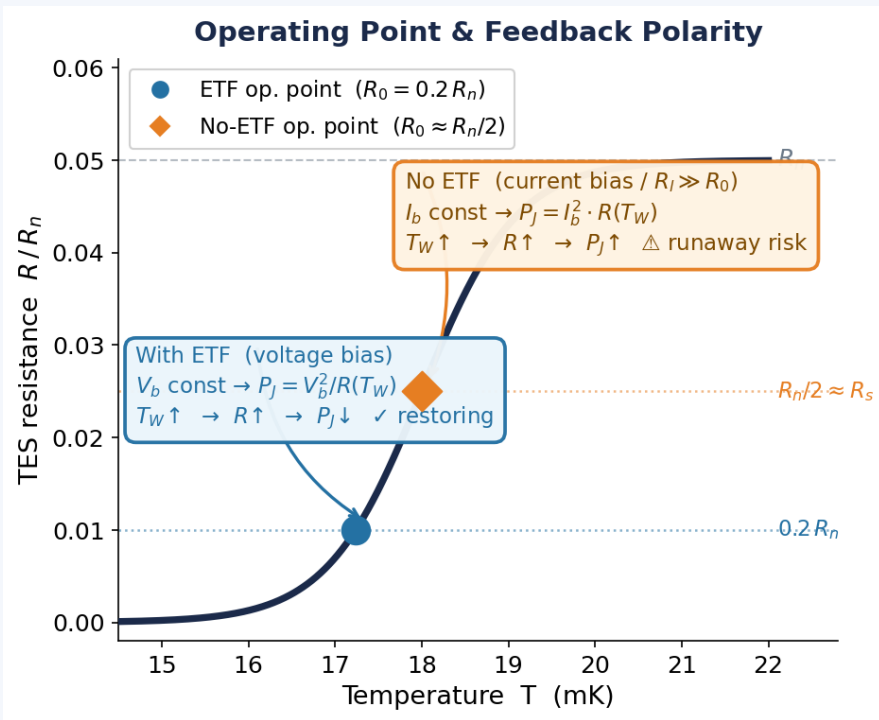
Calorimetric Mode

- Signal = $\Delta E / C_{\text{tot}}$ (total deposited energy)
- $\tau_{\text{eff}} \approx 104$ ms (slow — both athermal & thermal)
- $\sigma_E \approx 6.6$ eV (100 g BGO, 15 mK)
- ETF optional — P_j provides slow restoring force

Bolometric Athermal Mode

- Signal = $\epsilon \cdot \Delta E / C_W$ (athermal phonon fraction)
- $\tau_{\text{eff}} \approx 10$ ms (faster — ETF speed-up)
- $\sigma_E \approx 4.3$ eV (better — smaller C_W)
- **ETF essential — stabilises R(T) & compresses τ**

Electrothermal Feedback: Stable vs Unstable Operating Point



With ETF (voltage bias, $R\ell \ll R_0$)

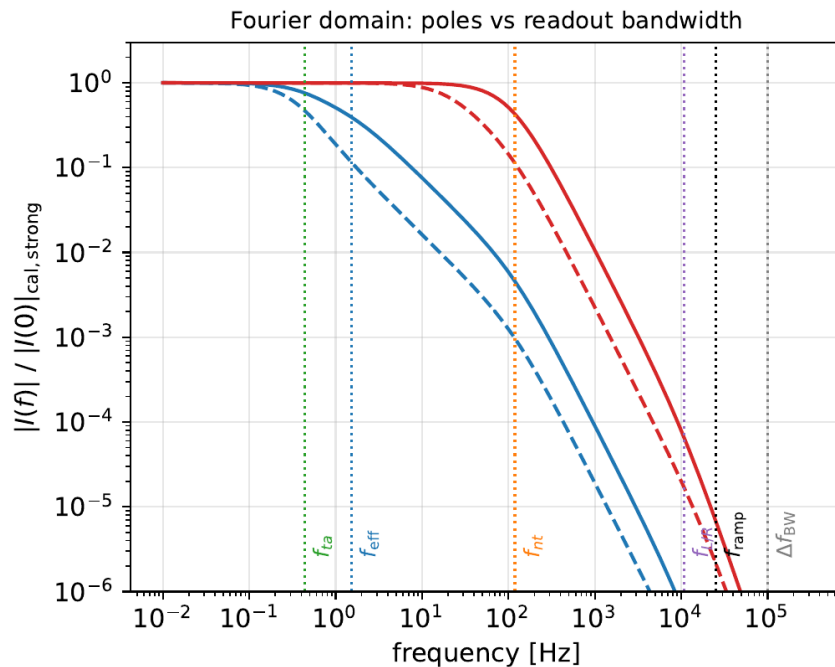
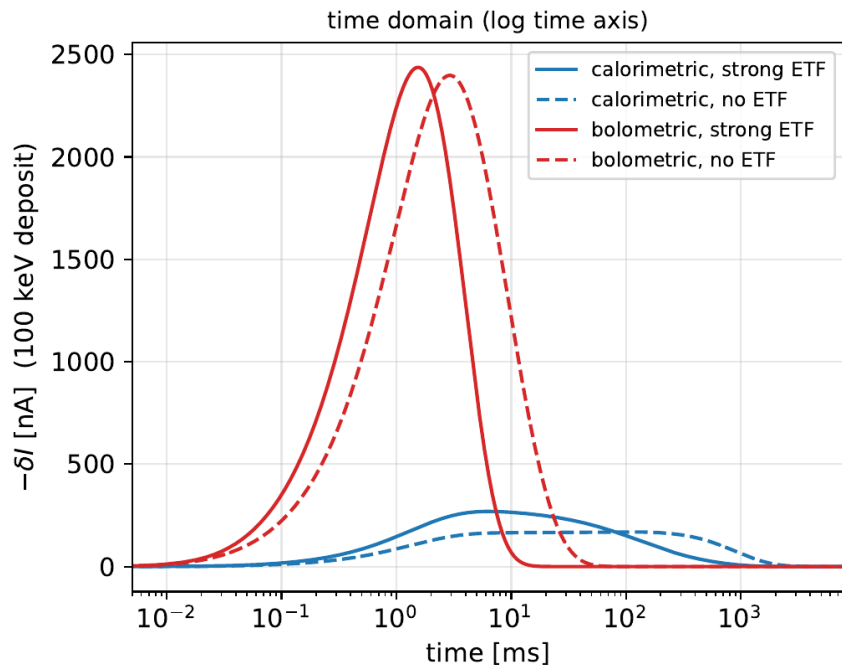
- Operating point: $R_0 \approx 0.2 R_n$ (low in transition)
- $V_b \text{ const} \rightarrow P_j = V^2 / R(T_w) \rightarrow T \uparrow \Rightarrow R \uparrow \Rightarrow P_j \downarrow \checkmark \text{ restoring}$
- $\tau_{\text{eff}} = \tau_0 / (1 + \mathcal{L}) \approx \tau_0 / 4.7$ (fast response)

No ETF (current bias, $R\ell \approx R_0$)

- Operating point: $R_0 \approx R_n/2 \approx R_s$ (mid transition)
- $I_b \text{ const} \rightarrow P_j = I^2 R(T_w) \rightarrow T \uparrow \Rightarrow R \uparrow \Rightarrow P_j \uparrow \Delta \text{ runaway risk}$
- Requires careful G_{tb} tuning to avoid thermal runaway

Pulse Formation & Key Time Constants

Pole hierarchy: f_{ta} (0.1-1 Hz) \ll $f_{S/N}$ (2 Hz) \ll f_{eff} (1-10 Hz) \ll f_{nt} (55-260 Hz) \ll $f_{L/R}$ (3.5 kHz) \ll f_{ramp} (25 kHz)



100 keV in 100 g BGO at 15 mK. Left: time-domain pulses ($-\delta/$ plotted). Right: $|f(f)|$ with poles marked vs $f_{ramp}=25$ kHz and $Df_{BW}=100$ kHz.

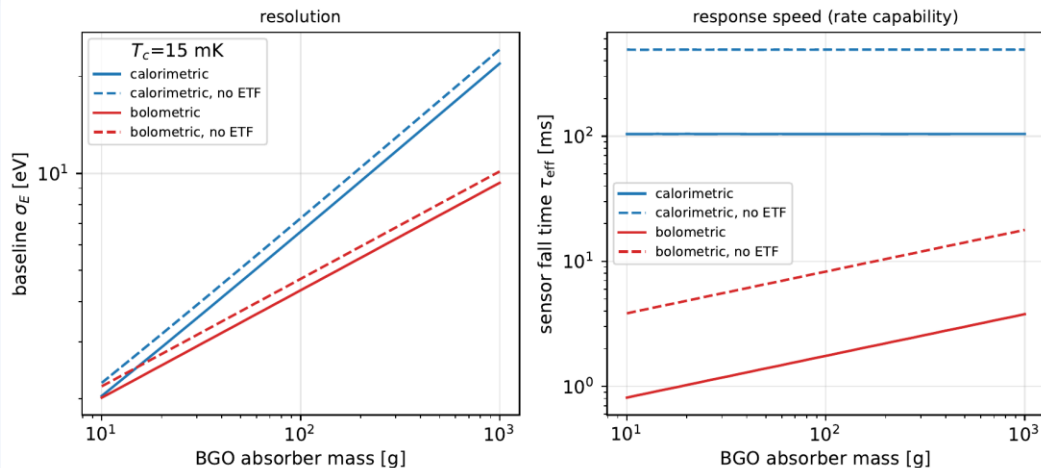
Two Operating Modes on the Same Hardware

CALORIMETRIC — integrates full energy vs C_{tot}

- G_{tb} sized for $f_{\text{S/N}} \sim 2 \text{ Hz} \ll f_{\text{nt}}$ (integrating limit)
- $\sigma_E(\text{BGO } 100\text{g}, 15\text{mK}) = 6.6 \text{ eV}$ | $\tau_{\text{eff}} \sim 104 \text{ ms}$
- Best for light crystals < 30 g; thermal component band-limited for heavy ones

BLOMETRIC (athermal) — measures $\epsilon * E$ vs C_{W}

- G_{tb} enlarged: $f_{\text{S/N}} \sim f_{\text{nt}}$ | $\tau_{\text{eff}} \sim 1.8 \text{ ms}$
- $\sigma_E(\text{BGO } 100\text{g}, 15\text{mK}) = 4.3 \text{ eV}$ — overtakes calo above $\sim 30 \text{ g}$
- Strong ETF required for speed + self-stabilization against athermal bursts

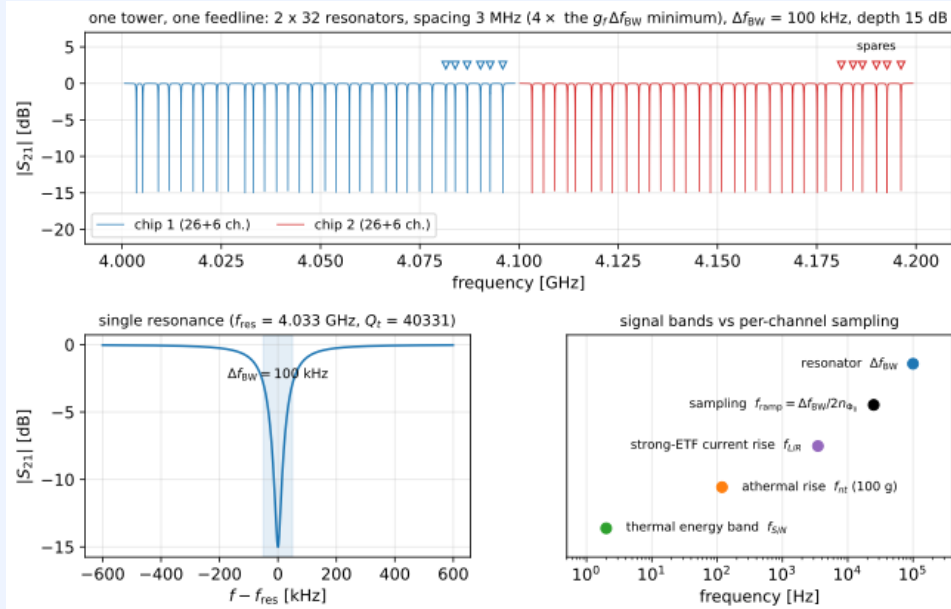


Left: resolution vs mass (bolometric overtakes calorimetric above $\sim 30 \text{ g}$). Right: sensor fall time ($\sim 100\times$ faster in bolometric mode).

Frequency-Division: Lorentzian Resonances on a Shared Feedline

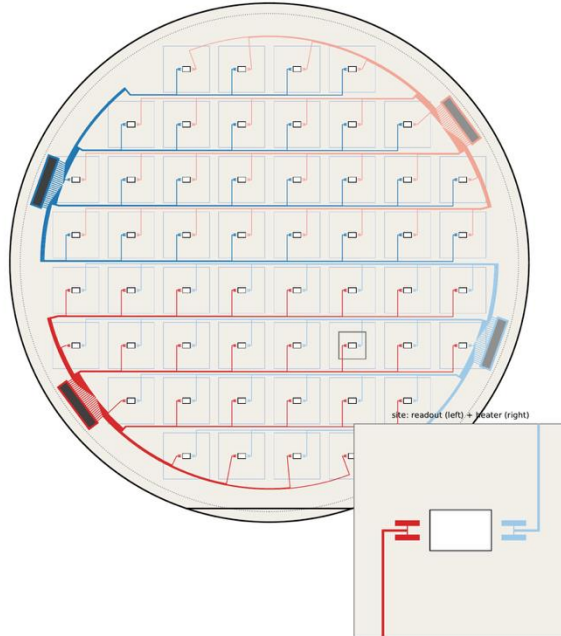
Reading the frequency comb

- Each resonator appears as a Lorentzian dip in $|S_{21}|$ vs frequency
- Resonance position f_0 shifts with TES current via rf-SQUID inductance
- bandwidth ~ 100 kHz at 4 GHz
- Channels spaced 3 MHz apart (30x bandwidth) \rightarrow negligible crosstalk
- 52-channel tower occupies only ~ 0.2 GHz of the 4-8 GHz HEMT band
- A 4 GHz band fits ~ 1300 resonators — ~ 20 towers on one readout line



Example Design: 52 BGO Crystals on a 200 mm Si Wafer

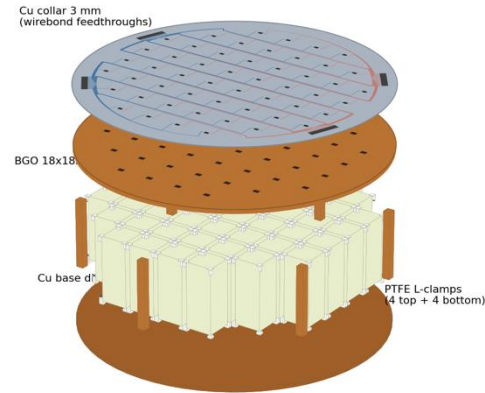
Configuration D: readout (west chips, saturated) + heater (east chips, light) -- BOTH on the top Nb layer, row-bus architecture
52 sites, 208 Nb wires | readout bus below each row / heater bus above, through the inter-row gaps | $L_{\text{wire}} = 3-66 \text{ nH}$ | crossings (all 384 wires): 0 | clearance $\geq 4.1 \text{ mm}$ | $r_{\text{max}} = 91 \text{ mm}$



Finalized single-layer Nb routing on 200 mm wafer: 52 crystal sites, readout (west) and heater (east) chips.

Si readout wafer
(traces, slots, chips)

52 x 100 g BGO = 5.20 kg (east)

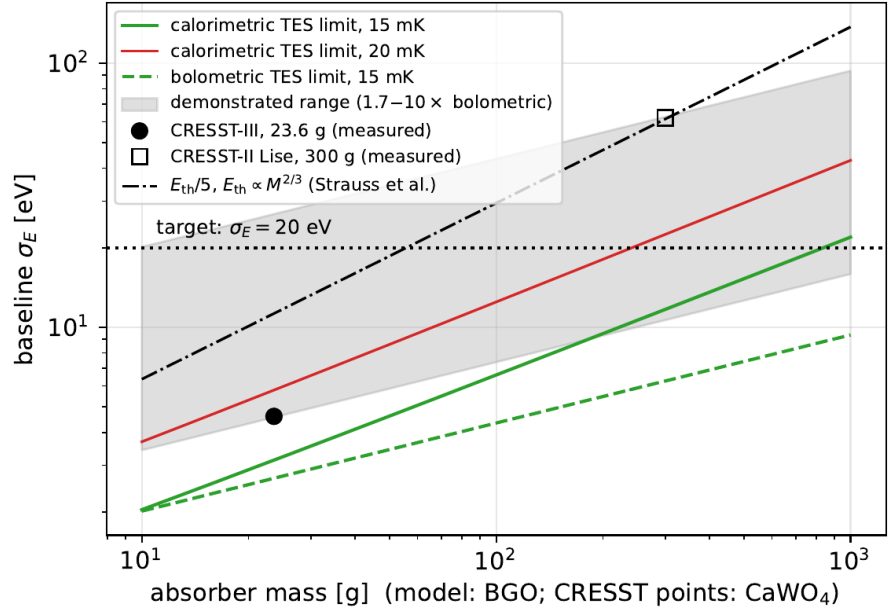
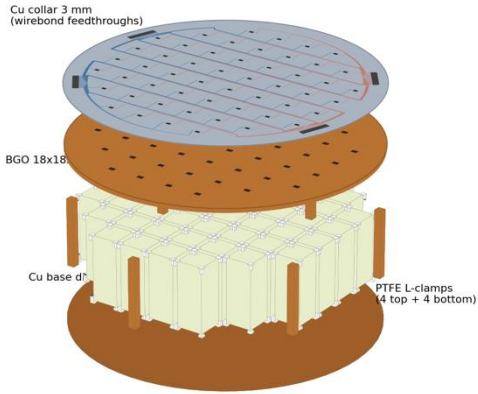


Wiring

On-wafer Nb traces: 3-66 nH \rightarrow total $L_{\text{in}} + L_{\text{wire}} < 1.1 \mu\text{H}$ \rightarrow $\tau_{L/R} \sim 46 \text{ us}$ \rightarrow resolution impact $< 10^{-4}$

Example Design: 52 BGO Crystals on a 200 mm Si Wafer

Si readout wafer (traces, slots, chips) **52 x 100 g BGO = 5.20 kg** (150)



TES-limited resolution vs mass (BGO example). Grey band: x1.7-10 above bolometric limit (CRESST anchors). Key result is material-independent: $\sigma \sim \sqrt{C_{tot}}$.

The Key Design Change: SQUID Input-Coil Sensitivity

Current uMUX devices

$$1/M_{in} \sim 23 \text{ uA}/\Phi_0$$

(bare rf-SQUID, $M_{in} \sim 90 \text{ pH}$)

$\text{sqrt}(S_{I_{ro}}) \sim 20\text{-}40 \text{ pA}/\text{rtHz}$

2-4x above detector noise -> limiting

Required for massive calorimeters

$$1/M_{in} = 0.4\text{-}1 \text{ uA}/\Phi_0$$

(multi-turn transformer, $M_{in} \sim 2\text{-}21 \text{ nH}$)

$\text{sqrt}(S_{I_{ro}}) \sim 0.4\text{-}2 \text{ pA}/\text{rtHz}$

Conclusions

uMUX is the enabler for future many channels/large scale cryogenic calorimeters

- The bandwidth can serve all TES operations:
 - Ton scale 1 keV threshold detectors
 - Many-kg scale sub-keV sensitive detectors
 - Bolometric for massive units
 - Calorimetric for light units
 - ETF for better stability & shorter signals
- Routing does not introduce a limiting L
- Need to tune the squid sensitivity

