

Evaluation of two-loop EW box diagrams for $e^+e^- \rightarrow ZH$

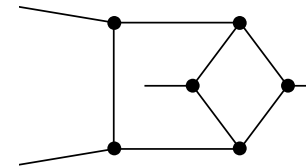
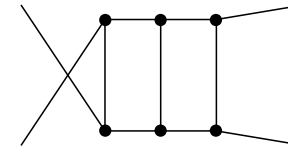
Qian Song

Ayres Freitas

17 May, Monday

Content

- Introduction
- Evaluation method: planar box diagram
non-planar box diagram
- Numerical result
- Summary



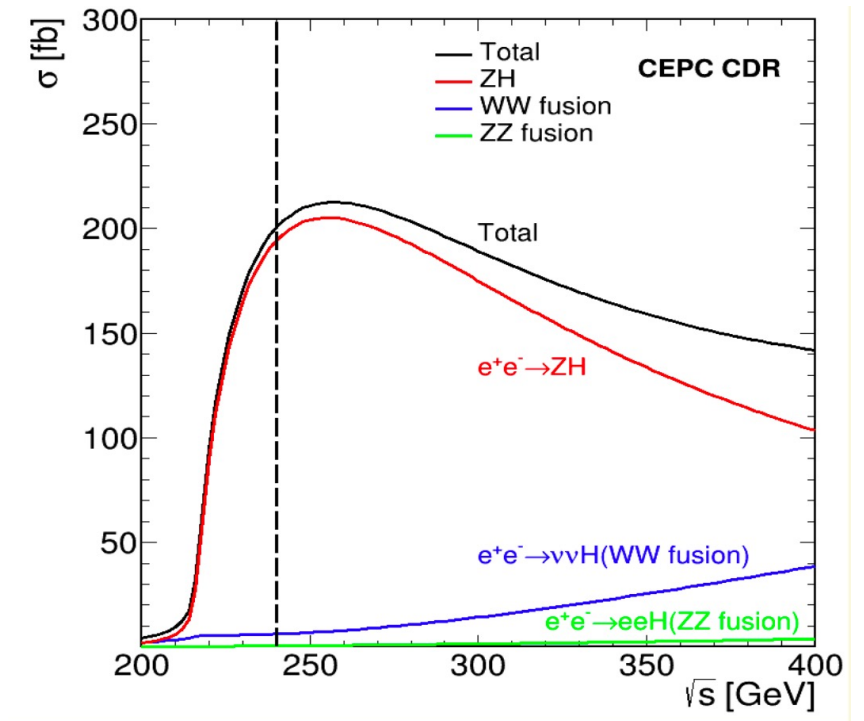
1. Introduction

- Discovery of Higgs boson(2012,LHC): last fundamental particle in SM
- Experiments at the ATLAS and CMS: agrees with the result SM predicted
- Problems not solved: electroweak symmetry breaking, Higgs coupling to SM particles/DM, hierarchy problem... Require new physics beyond SM
- One promising way probing new physics: precision measurements of the properties of H
- LHC is difficult to reach very high precision due to complicated background



1. Introduction

- FCC-ee, CEPC, ILC: e+e- collider, large statistics, high luminosity, clean environment, measure H properties with very high precision ($\sqrt{s}=240\text{-}250\text{GeV}$)
- ILC: $\sigma_{ZH} \sim 1.2\%$, 250fb^{-1} (H. Baer et al. [arXiv:1306.6352 [hep-ph]])
- FCC-ee: $\sigma_{ZH} \sim 0.4\%$, 5ab^{-1} (A. Abada et al [FCC Collaboration])
- CEPC: $\sigma_{ZH} \sim 0.5\%$, 5.6ab^{-1} (arXiv:1811.10545)



1. Introduction

- LO on $\sigma(e^+e^- \rightarrow ZH)$:
only consider s channel
t,u channel amplitude is zero due to
small Yukawa coupling
- NLO on $\sigma(e^+e^- \rightarrow ZH)$:
unpolarized beam: 5-10%;
(A. Denner et al, Phys. C 56, 261(1992))
polarized beam: 10-20%;
(S. Bondarenko, Phys. Rev. D 100, 073002(2019))

$$\sigma(P_{e^-}, P_{e^+}) = \frac{1}{4} \sum_{\chi_1 \chi_2} (1 + \chi_1 P_{e^+})(1 + \chi_2 P_{e^-}) \sigma_{\chi_1 \chi_2},$$

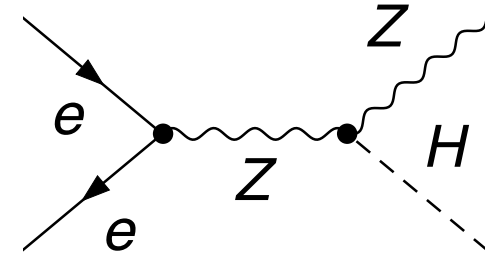


TABLE I. Hard ($E_\gamma > 1$ GeV), Born, and one-loop cross sections in fb and relative corrections δ in % for the c.m. energy $\sqrt{s} = 250$ GeV and various polarization degrees of the initial particles.

P_{e^-}	P_{e^+}	$\sigma^{\text{hard}}, \text{fb}$	$\sigma^{\text{Born}}, \text{fb}$	$\sigma^{\text{one-loop}}, \text{fb}$	$\delta, \%$
0	0	82.0(1)	225.59(1)	206.77(1)	-8.3(1)
-0.8	0	96.7(1)	266.05(1)	223.33(2)	-16.1(1)
-0.8	-0.6	46.3(1)	127.42(1)	111.67(2)	-12.4(1)
-0.8	0.6	147.1(1)	404.69(1)	334.99(1)	-17.2(1)

1. Introduction

- NNLO:(s= 240-250GeV)

EW+QCD:0.4-1.3% ($\alpha(0)$, $\alpha(M_Z)$, G_μ)

(Q.F.Sun, Phys.Rev.D 96,051301(2017))

EW+QCD:1.3% (\overline{MS} , $\alpha(M_Z)$)

(Q.F.Sun, Phys.Rev.D 96,051301(2017))

\sqrt{s}	schemes	σ_{LO} (fb)	σ_{NLO} (fb)	σ_{NNLO} (fb)
240	$\alpha(0)$	223.14 ± 0.47	229.78 ± 0.77	$232.21^{+0.75+0.10}_{-0.75-0.21}$
	$\alpha(M_Z)$	252.03 ± 0.60	$228.36^{+0.82}_{-0.81}$	$231.28^{+0.80+0.12}_{-0.79-0.25}$
	G_μ	239.64 ± 0.06	$232.46^{+0.07}_{-0.07}$	$233.29^{+0.07+0.03}_{-0.06-0.07}$
250	$\alpha(0)$	223.12 ± 0.47	229.20 ± 0.77	$231.63^{+0.75+0.12}_{-0.75-0.21}$
	$\alpha(M_Z)$	252.01 ± 0.60	$227.67^{+0.82}_{-0.81}$	$230.58^{+0.80+0.14}_{-0.79-0.25}$
	G_μ	239.62 ± 0.06	231.82 ± 0.07	$232.65^{+0.07+0.04}_{-0.07-0.07}$

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TABLE II. Total cross sections at various collider energies in the $\alpha(m_Z)$ scheme.

\sqrt{s} (GeV)	σ_{LO} (fb)	σ_{NLO} (fb)	σ_{NNLO} (fb)	$\sigma_{\text{NNLO}}^{\text{exp}}$ (fb)
240	252.0	228.6	231.5	231.5
250	252.0	227.9	230.8	230.8
300	190.0	170.7	172.9	172.9
350	135.6	122.5	124.2	124.0
500	60.12	54.03	54.42	54.81

1. Introduction

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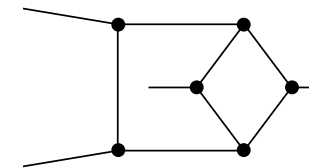
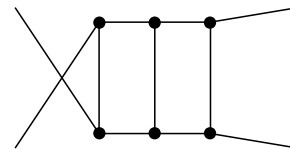
- EW+EW: $\sim 1\%$ (arXiv:1906.05379) (25377 diagrams (arXiv:2102.15213))

challenging type: 2250 diagrams with 7 denominators, 4 independent mass scale, 2 independent energy scale

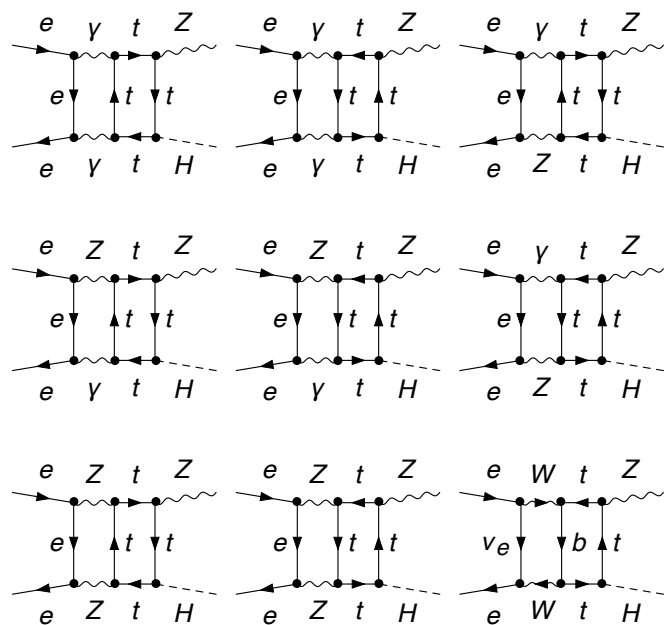
diagrams with closed fermion loop dominant due to large top-quark Yukawa coupling and large number of fermions in SM

→ planar & Non-planar diagrams with closed top-quark loop (18+9)

1. Introduction

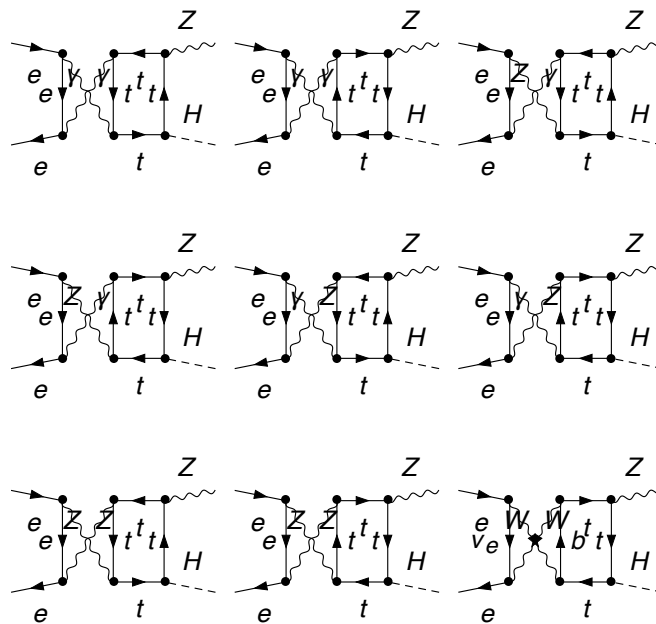


$e e \rightarrow Z H$

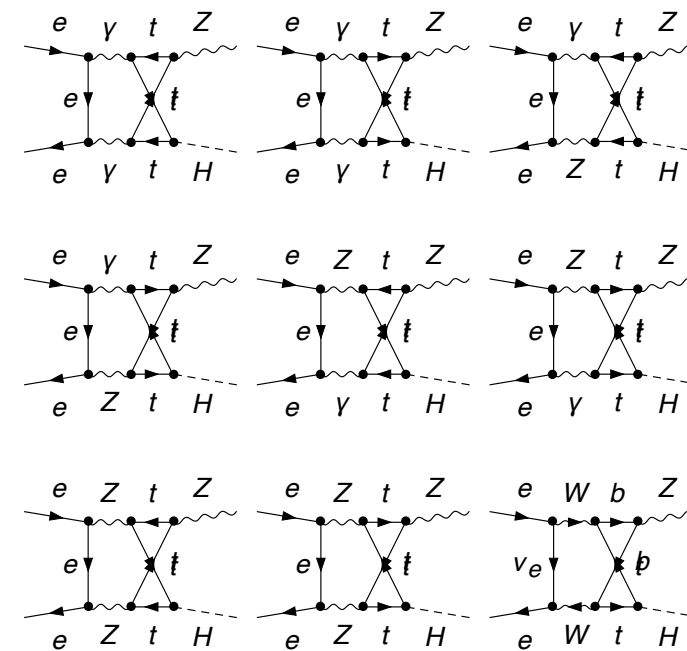


Planar double-box diagrams

$e e \rightarrow Z H$



$e e \rightarrow Z H$



Non-planar double-box diagrams

1. Introduction

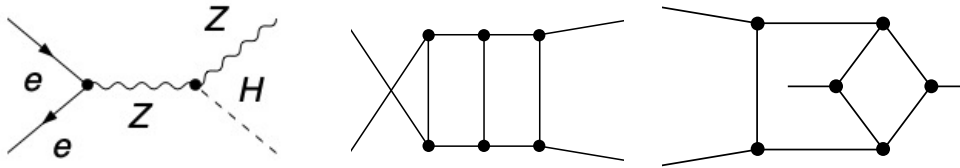
- Analytical calculation: can be done for 1-loop, but difficult in 2-loop: require more knowledge about special functions(harmonic polylogarithmic functions, iterated elliptic integrals)
- Numerical calculation: use Feynman parametrization. Box diagram is equal to integration over 6 Feynman parameters. It requires large computing resources and takes few days because the integrand converges slowly

(F. Yuasa et al; Comput. Phys. Commun. 183, 2136-2144 (2012))

$$I_{planar} = - \int_0^1 d\rho \int_0^1 d\xi \int_0^1 du_1 \int_0^{1-u_1} du_2 \int_0^1 du_3 \int_0^{1-u_3} du_4 \frac{\mathcal{C}}{(\mathcal{D} - i\epsilon\mathcal{C})^3} \rho^3 \xi^2 (1 - \xi)^2,$$

- Our method: simplify the integrand with Feynman parametrization and dispersion relation. The box diagram is reduced to 3-fold integration, which takes few minutes to calculate.

1. Introduction



- Feynman diagrams → FeynArts (T. Hahn, Comput. Phys. Commun. 140, 418 (2001). [hep-ph/0012260])

- Square amplitude → FeynCalc (dim =4)

(V. Shtabovenko, R. Mertig and F. Orellana, "FeynCalc 9.3: New features and improvements", arXiv:2001.04407.)

- (...) → dispersion relation and Feynman parameterization (Mathematica)

- Numerical calculation → C++, LoopTools, Gauss-Kronrod quadrature In Boost package

(Comput.Phys.Commun.118(1999)153)

(<https://www.boost.org/doc/libs/master/libs/math/doc/html/index.html>)

$$M_0 M_2^* = \iiint dx dy d\sigma (\dots)$$

2. Evaluation Method – planar diagram

According to Feynman rules, the amplitude for planar diagram can be written as I_{plan} .

Use Feynman parametrization to simplify the denominators only involve q_2

$$\text{Feynman parametrization: } \frac{1}{abc} = \int_0^1 dx \int_0^{1-x} dy \frac{1}{(ax + by + c(1-x-y))^3}$$

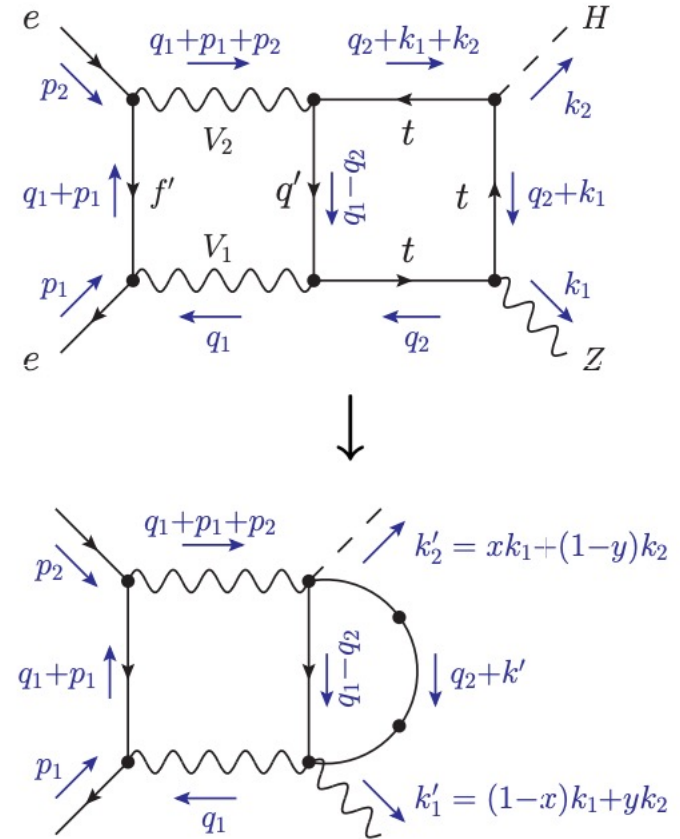
$$I_{plan} = \int d_{q_1}^D d_{q_2}^D \frac{1}{(q_1^2 - m_{V_1}^2)((q_1 + p_1)^2 - m_{f'}^2)((q_1 + p_1 + p_2)^2 - m_{V_2}^2)(q_1 - q_2)^2 - m_{q'}^2} \frac{1}{(q_2^2 - m_t^2)((q_2 + k_1)^2 - m_t^2)((q_2 + k_1 + k_2)^2 - m_t^2)}$$

$$\int_0^1 dx \int_0^{1-x} dy \frac{1}{((q_2 + k')^2 - m'^2)^3} = \int_0^1 dx \int_0^{1-x} dy \partial_{m'^2}^2 \frac{1}{(q_2 + k')^2 - m'^2}$$

$$= \int_0^1 dx \int_0^{1-x} dy \partial_{m'^2}^2 \int d_{q_1}^D \frac{B_0((q_1 + k')^2, m_{q'}^2, m'^2)}{(q_1^2 - m_{V_1}^2)((q_1 + p_1)^2 - m_{f'}^2)((q_1 + p_1 + p_2)^2 - m_{V_2}^2)}$$

Loop momentum q_1 appears in B0 functions, so cannot integrate over q_1 .

→ use dispersion relation to put q_1 outside B0 function



2. Evaluation Method – planar diagram

dispersion relation:

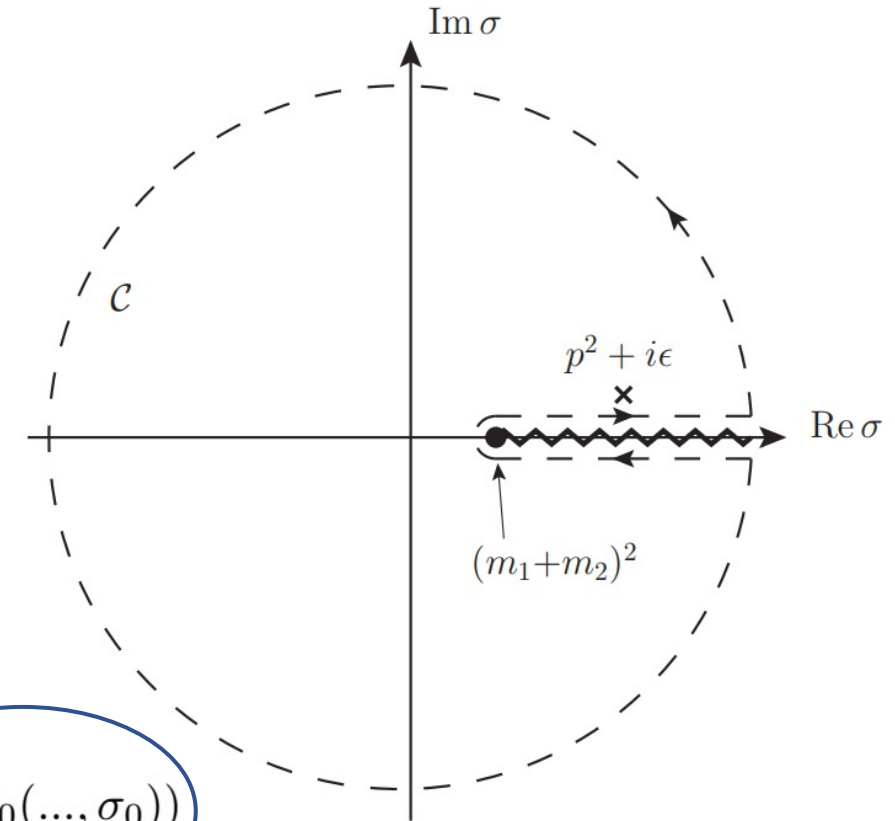
$$\begin{aligned}
 B_0(p^2, m_1^2, m_2^2) &= \frac{1}{2\pi i} \oint_C d\sigma \frac{B_0(\sigma, m_1^2, m_2^2)}{\sigma - p^2 - i\epsilon} \\
 &= \int_{(m_1+m_2)^2}^{\infty} d\sigma \frac{\Delta B_0(\sigma, m_1^2, m_2^2)}{\sigma - p^2 - i\epsilon} \\
 &= \int_{(m_1+m_2)^2}^{\infty} d\sigma \frac{1}{\pi} \frac{\text{Im} B_0(\sigma, m_1^2, m_2^2)}{\sigma - p^2 - i\epsilon}
 \end{aligned}$$

$$I_{\text{plan}} = \int_0^1 dx \int_0^{1-x} dy \partial_{m'^2}^2 \int_{(m'+m_{q'})^2}^{\infty} d\sigma \Delta B_0(s, m'^2, m_{q'}^2) D_0(\dots, \sigma)$$

$$= \int_0^1 dx \int_0^{1-x} dy \int_{(m'+m_{q'})^2}^{\infty} d\sigma \partial_{m'^2}^2 \Delta B_0(s, m'^2, m_{q'}^2) (D_0(\dots, \sigma) - \frac{\sigma_0}{\sigma} D_0(\dots, \sigma_0))$$

$$+ \int_0^1 dx \int_0^{1-x} dy \sigma_0 D_0(\dots, \sigma_0) \partial_{m'^2}^2 B_0(0, m'^2, m_{q'}^2)$$

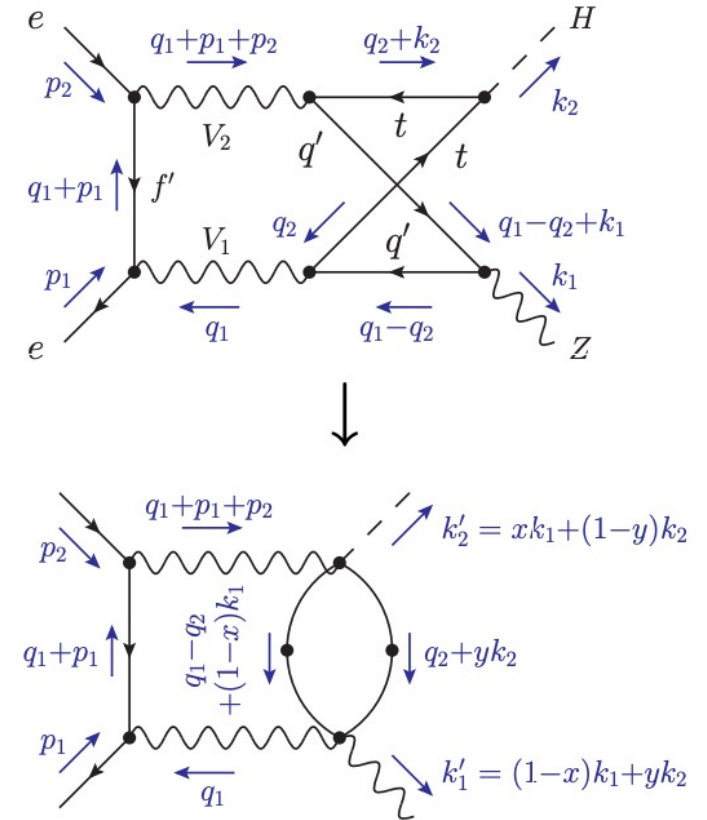
cancel the divergence at lower bound



2. Evaluation Method – non-planar diagram

Similarly, use Feynman parametrization to simplify the denominators including q_2 and integrating loop momentum q_2 gives B0 function

$$\begin{aligned}
 I_{NP} &= \int d_{q_1}^D d_{q_2}^D \frac{1}{(q_1^2 - m_{V_1}^2)((q_1 + p_1)^2 - m_{f'}^2)((q_1 + p_1 + p_2)^2 - m_{V_2}^2)} \\
 &\quad \frac{1}{\underbrace{((q_1 - q_2)^2 - m_{q'}^2)((q_1 - q_2 + k_1)^2 - m_{q'}^2)}_{\int_0^1 dx \partial_{m_1'^2} \frac{1}{(q_1 - q_2 + (1-x)k_1)^2 - m_1'^2}} \underbrace{(q_2^2 - m_t^2)((q_2 + k_2)^2 - m_t^2)}_{\int_0^1 dy \partial_{m_2'^2} \frac{1}{(q_2 + yk_2)^2 - m_2'^2}}} \\
 &= \int_0^1 dx \int_0^1 dy \partial_{m_1'^2} \partial_{m_2'^2} \int d_{q_1}^D B_0((q_1 + (1-x)k_1 + yk_2)^2, m_1'^2, m_2'^2) \\
 &\quad \frac{1}{(q_1^2 - m_{V_1}^2)((q_1 + p_1)^2 - m_{f'}^2)((q_1 + p_1 + p_2)^2 - m_{V_2}^2)}
 \end{aligned}$$



2. Evaluation Method – non-planar diagram

- For non-planar double box including $\gamma\gamma, \gamma Z, ZZ$, use the same dispersion relation as planar diagram
- For non-planar double-box including WW:

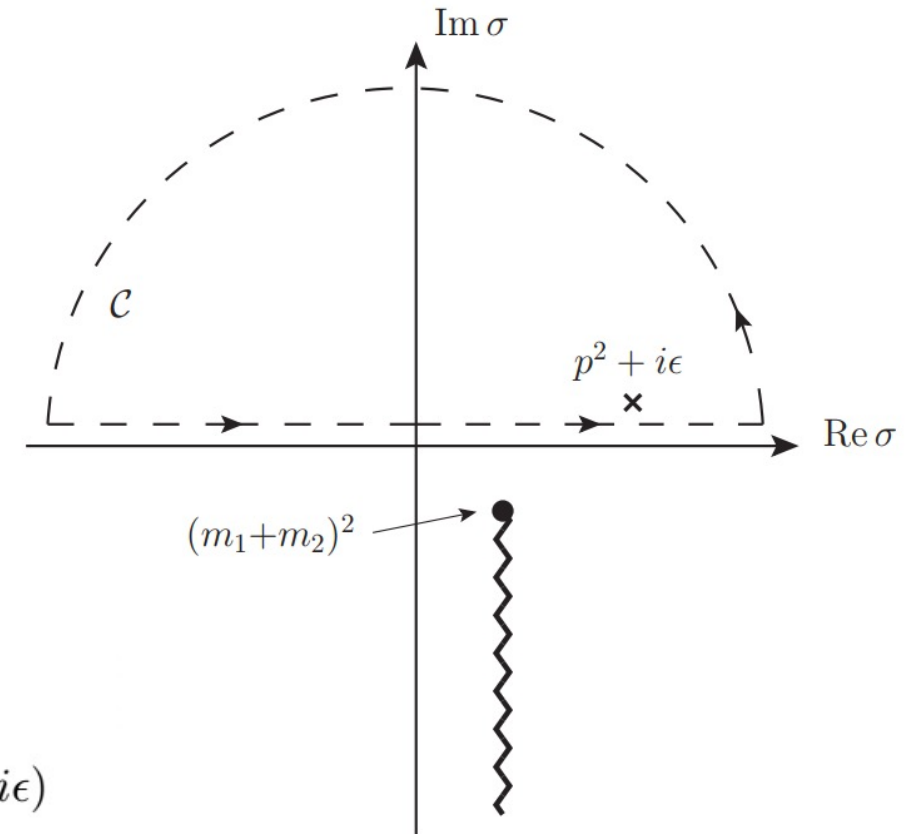
$$m_1'^2 = m_b^2 - x(1-x)m_Z^2 < 0$$

Branch cut changes , we use a new dispersion relation

$$B_0(p^2, m_1'^2, m_2'^2) = \frac{1}{2\pi i} \oint_C d\sigma \frac{B_0(\sigma, m_1'^2, m_2'^2)}{\sigma - p^2 - i\epsilon}$$

$$= \frac{1}{2\pi i} \int_{-\infty}^{\infty} d\sigma \frac{B_0(\sigma, m_1'^2, m_2'^2)}{\sigma - p^2 - i\epsilon}$$

$$I_{NP-WW} = \frac{-1}{2\pi i} \int_0^1 dx \int_0^1 dy \int_{-\infty}^{\infty} d\sigma \partial_{m_1'^2} \partial_{m_2'^2} B_0(\sigma, m_1'^2, m_2'^2) D_0(\dots, \sigma - i\epsilon)$$



2. Evaluation Method

$$I = \underbrace{\int dx \int dy \int d\sigma}_{\text{Gauss-kronrod quadrature(Boost)}} \underbrace{B_0(\sigma, m_1^2, m_2^2) \text{ or } \Delta B_0(\sigma, m_1^2, m_2^2)}_{\text{analytical expression is known}} \times \underbrace{(c_A A_0 + c_B B_0 + c_C C_0 \dots)}_{\text{LoopTools package}}$$

- Programming using C++
- Running time: few minutes to half an hour(non-planar WW)
- Advantages: low requirement of computer,
short running time
- Precision: 4-digit, the precision is confined by the LoopTools(double-precision)
- Stability: integrand is smooth

3. Result: instability

- Upper and lower bound of the integrand, $\delta \sim 10^{-3}$, $\Lambda \sim 10^8$

$$\int_{\sigma_0}^{\infty} f(\sigma) = \int_{\sigma_0(1+\delta)}^{\Lambda} f(\sigma) + 2\sigma_0\delta f(\sigma_0\delta) + \Lambda f(\Lambda)$$

- For non-planar diagram, the Gram determinants (tensor decomposition [arXiv:0812.2134](https://arxiv.org/abs/0812.2134) [hep-ph]) for some Passarino-Veltman tensor functions vanish when x is equal to y , and LoopTools is not able to give a number.

a) separate the integration region of x : $(0, 0.5)$ $(0.5, 1)$

b) separate the integration region of y : $(0, x-\delta)$, $(x-\delta, x+\delta)$, $(x+\delta, 1)$ $\delta = 10^{-2, -3, \dots}$

- For non-planar diagram with W bosons, $\sigma - i\epsilon$, $\epsilon \sim 10^{-9}|\sigma|$ or $\epsilon \sim 10^{-5}$

3. Result

Parameter	Value
M_Z	91.1876 GeV
M_W	80.379 GeV
M_H	125.1 GeV
m_t	172.76 GeV
α	1/137
E_{CM}	240 GeV
m_γ	10^{-6} GeV
θ	$\pi/2$

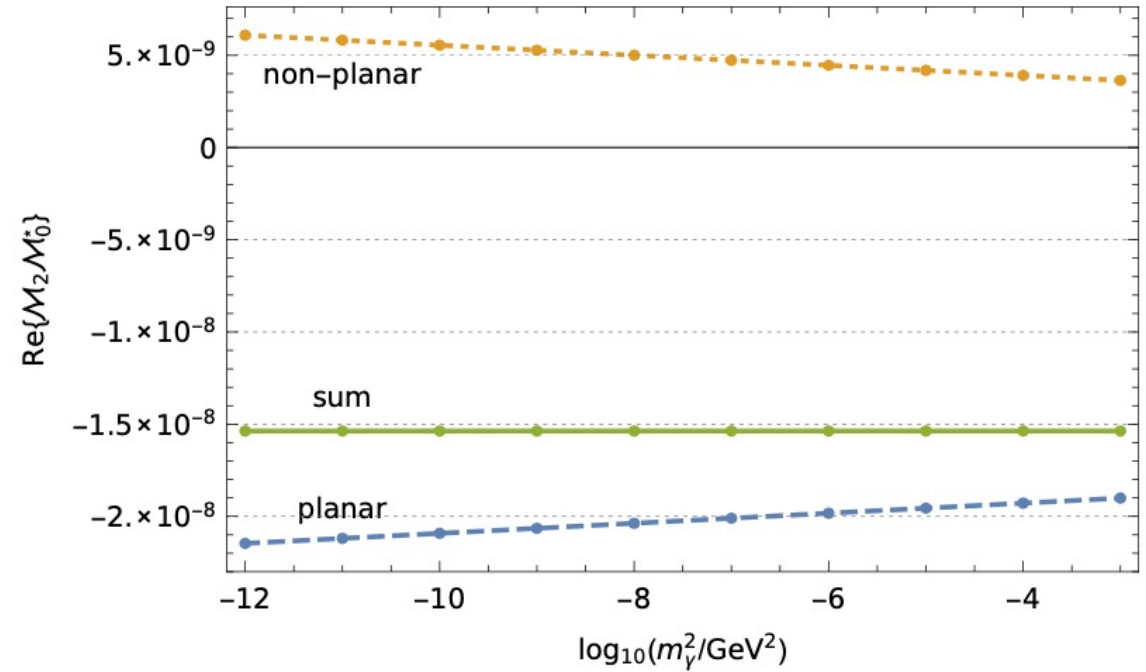
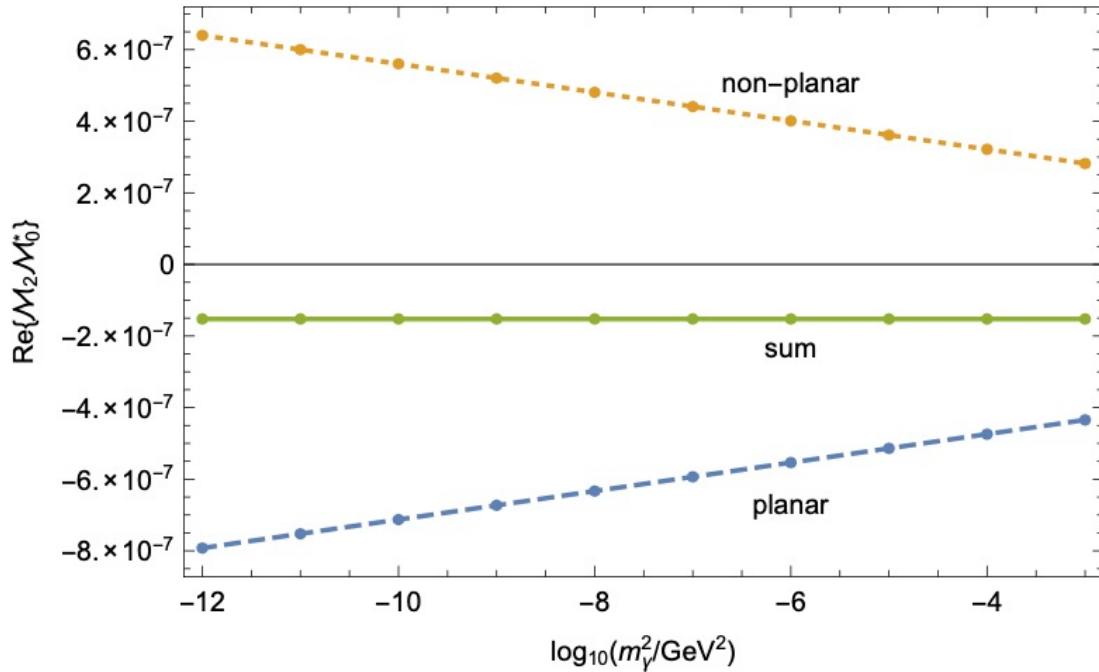
regulate the IR divergence,
no UV divergence

few minutes

$V_1 V_2$ diagr. class	$\text{Re}\{\mathcal{M}_2 \mathcal{M}_0^*\}$
$\gamma\gamma$	$-1.524(1) \times 10^{-7}$
γZ	$-1.537(1) \times 10^{-8}$
ZZ planar	$-4.402(4) \times 10^{-8}$
ZZ non-planar	$1.724(2) \times 10^{-8}$
WW planar	$-1.1392(8) \times 10^{-6}$
WW non-planar	$-5.577(5) \times 10^{-7}$

~ 30 minutes

3. Result



Dependence of the $\gamma\gamma$ (left) and γZ (right) two-loop boxes on the photon mass m_γ

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3. Summary

- Double-box diagrams can be efficiently evaluated by Feynman parametrization and dispersion relation (For non-planar diagrams with 2 W bosons, dispersion relation is different from other diagrams)
- Takes few minutes for numerical calculation. For non-planar diagrams with 2 W bosons, takes half an hour.
- IR divergence is controlled by giving photon a small mass without loss of numerical precision.
- The evaluation method can also be applied for the calculation of electroweak corrections to other $2 \rightarrow 2$ process, such as $e^+ e^- \rightarrow W^+ W^-$

Thank you!

2. Evaluation Method – planar diagram

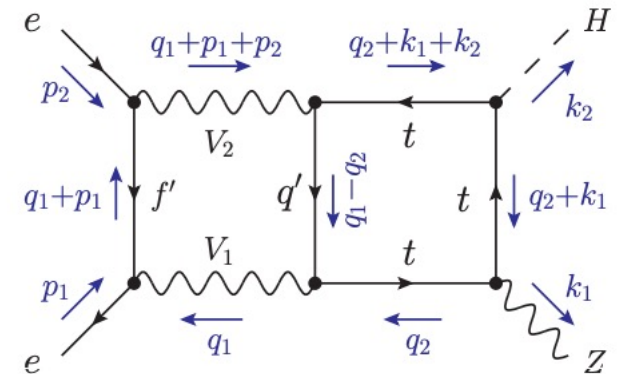
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Use Feynman parametrization to simplify the denominators only involve q^2

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$$\frac{1}{\underbrace{(q_2^2 - m_t^2)((q_2 + k_1)^2 - m_t^2)((q_2 + k_1 + k_2)^2 - m_t^2)}}_{\int_0^1 dx \int_0^{1-x} dy \frac{1}{((q_2 + k')^2 - m'^2)^3} = \int_0^1 dx \int_0^{1-x} dy \frac{1}{m'^2 (q_2 + k')^2 - m'^2}}$$

Feynman parametrization: $\frac{1}{abc} = \int_0^1 dx \int_0^{1-x} dy \frac{1}{(ax + by + c(1-x-y))^3}$



2. Evaluation Method – planar diagram

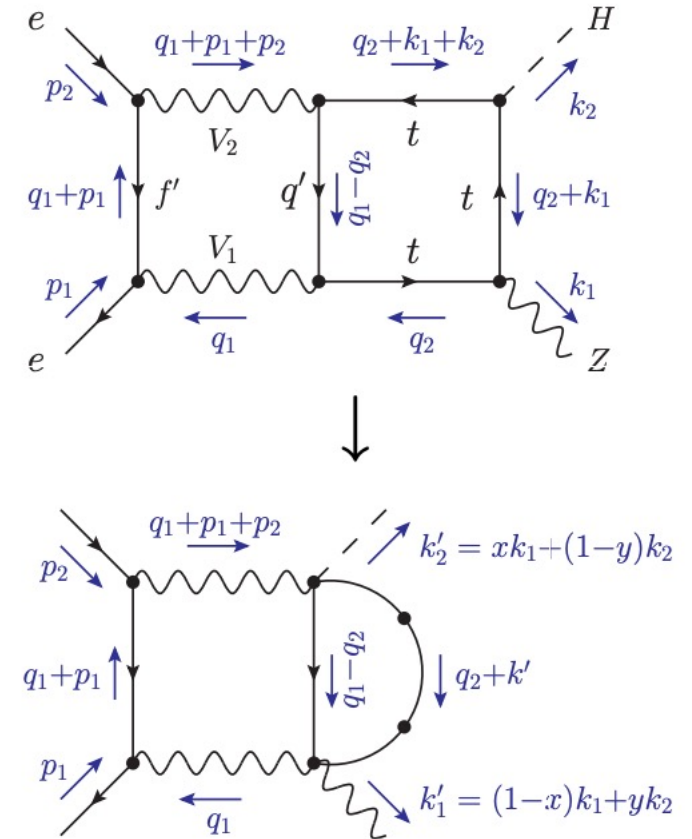
Integrating over loop momentum q_2 gets B0 function:

$$I_{plan} = \int_0^1 dx \int_0^{1-x} dy \partial_{m'^2}^2 \int d_{q_1}^D d_{q_2}^D \frac{1}{(q_1^2 - m_{V_1}^2)((q_1 + p_1)^2 - m_{f'}^2)((q_1 + p_1 + p_2)^2 - m_{V_2}^2)}$$

$$\frac{1}{((q_1 - q_2)^2 - m_{q'}^2)} \frac{1}{(q_2 + k')^2 - m'^2}$$

$$= \int_0^1 dx \int_0^{1-x} dy \partial_{m'^2}^2 \int d_{q_1}^D \frac{B_0((q_1 + k')^2, m_{q'}^2, m'^2)}{(q_1^2 - m_{V_1}^2)((q_1 + p_1)^2 - m_{f'}^2)((q_1 + p_1 + p_2)^2 - m_{V_2}^2)}$$

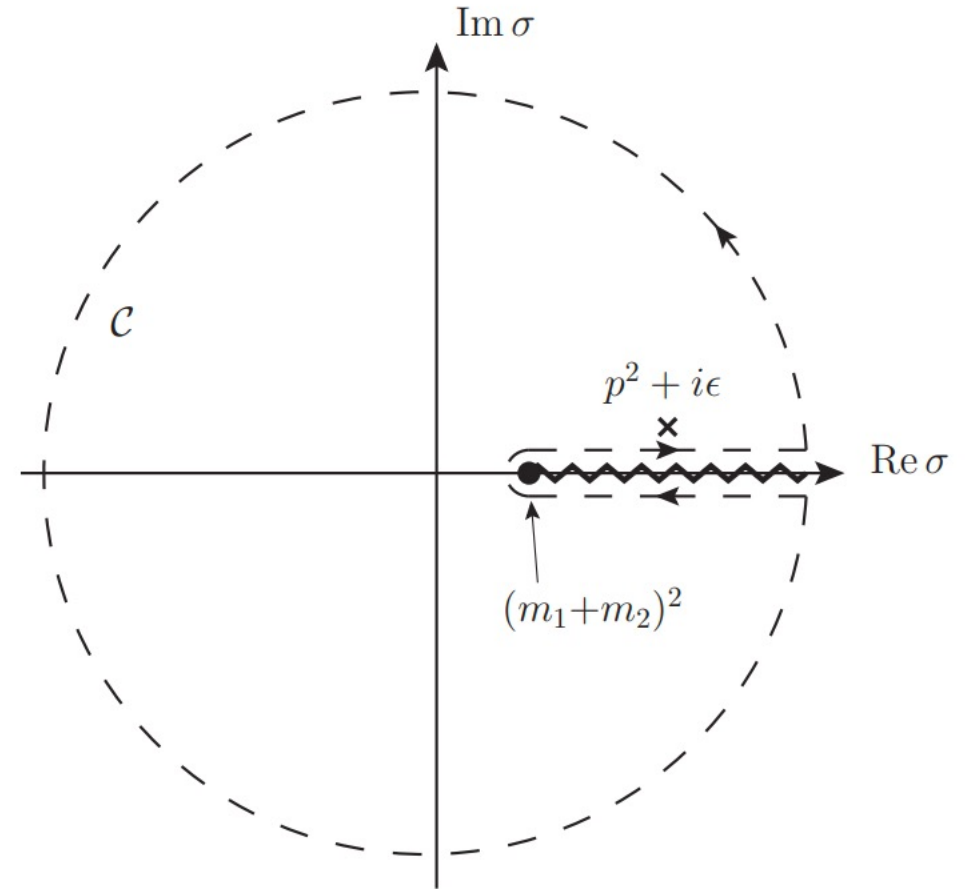
Loop momentum q_1 appears in B0 functions, so cannot integrate over q_1 .
 → use dispersion relation to put q_1 outside B0 function



2. Evaluation Method – planar diagram

dispersion relation:

$$\begin{aligned} B_0(p^2, m_1^2, m_2^2) &= \frac{1}{2\pi i} \oint_C d\sigma \frac{B_0(\sigma, m_1^2, m_2^2)}{\sigma - p^2 - i\epsilon} \\ &= \int_{(m_1+m_2)^2}^{\infty} d\sigma \frac{\Delta B_0(\sigma, m_1^2, m_2^2)}{\sigma - p^2 - i\epsilon} \\ &= \int_{(m_1+m_2)^2}^{\infty} d\sigma \frac{1}{\pi} \frac{\text{Im} B_0(\sigma, m_1^2, m_2^2)}{\sigma - p^2 - i\epsilon} \end{aligned}$$



2. Evaluation Method – planar diagram

Integrating over q_1 gets the D0 function.

Use Leibiniz's rule to put the derivative inside the integral: ΔB_0 is divergent at the lower bound, it can be fixed by subtracting one term to make the integrand become 0 at the lower bound.

$$\begin{aligned}
 I_{plan} &= \int_0^1 dx \int_0^{1-x} dy \partial_{m'2}^2 \int_{(m'+m_{q'})^2}^{\infty} d\sigma \int d_{q_1}^D \Delta B_0(s, m'^2, m_{q'}^2) \\
 &\quad \frac{1}{(q_1^2 - m_{V_1}^2)((q_1 + p_1)^2 - m_{f'}^2)((q_1 + p_1 + p_2)^2 - m_{V_2}^2)(s - (q_1 + k')^2)} \\
 &= - \int_0^1 dx \int_0^{1-x} \partial_{m'2}^2 \int_{(m'+m_{q'})^2}^{\infty} d\sigma \Delta B_0(\sigma, m'^2, m_{q'}^2) D_0(p_1^2, p_2^2, k'_2, k'_1, s, t, m_{V_1}^2, m_{f'}^2, m_{V_2}^2, \sigma)
 \end{aligned}$$

Leibiniz's rule:

$$\frac{d}{dx} \left(\int_{a(x)}^{b(x)} f(x, t) dt \right) = \int_{a(x)}^{b(x)} \frac{\partial}{\partial x} f(x, t) dt + f(x, b(x)) \frac{db(x)}{dx} - f(x, a(x)) \frac{da(x)}{dx}$$

2. Evaluation Method – planar diagram

$$\begin{aligned}
 & \partial_{m'^2}^2 \int_{(m'+m_{q'})^2}^{\infty} d\sigma \Delta B_0(\sigma, m'^2, m_{q'}^2) (D_0(\dots, \sigma) - \frac{\sigma_0}{\sigma} D_0(\dots, \sigma_0) + \frac{\sigma_0}{\sigma} D_0(\dots, \sigma_0)) \\
 &= \partial_{m'^2}^2 \int_{(m'+m_{q'})^2}^{\infty} d\sigma \Delta B_0(\sigma, m'^2, m_{q'}^2) (D_0(\dots, \sigma) - \frac{\sigma_0}{\sigma} D_0(\dots, \sigma_0)) \rightarrow 0 \text{ at the lower bound, so derivative can be put} \\
 & \quad \text{inside the integral} \\
 &+ \partial_{m'^2}^2 \int_{(m'+m_{q'})^2}^{\infty} d\sigma \Delta B_0(\sigma, m'^2, m_{q'}^2) \frac{\sigma_0}{\sigma} D_0(\dots, \sigma_0) \rightarrow \text{integrate over } \sigma \text{ gives } B_0(0, m'^2, m_{q'}^2) \text{ (dispersion relation)}
 \end{aligned}$$

$$\begin{aligned}
 I_{\text{plan}} &= \int_0^1 dx \int_0^{1-x} dy \partial_{m'^2}^2 \int_{(m'+m_{q'})^2}^{\infty} d\sigma \Delta B_0(s, m'^2, m_{q'}^2) D_0(p_1^2, p_2^2, k_2'^2, k_1'^2, s, t, m_{V_1}^2, m_{f'}^2, m_{V_2}^2, \sigma) \\
 &= \int_0^1 dx \int_0^{1-x} dy \int_{(m'+m_{q'})^2}^{\infty} d\sigma \partial_{m'^2}^2 \Delta B_0(s, m'^2, m_{q'}^2) (D_0(\dots, \sigma) - \frac{\sigma_0}{\sigma} D_0(\dots, \sigma_0)) \\
 &+ \int_0^1 dx \int_0^{1-x} dy \sigma_0 D_0(\dots, \sigma_0) \partial_{m'^2}^2 B_0(0, m'^2, m_{q'}^2)
 \end{aligned}$$

2. Evaluation Method – planar diagram

If the numerator is not equal to 1, integrating over q_2 gets B_1, B_{00}, B_{11} functions. They have same dispersion relation as B_0 .

For example, num = $p_1 \cdot q_2$

num = $p_1 \cdot q_2, (p_1 \cdot q_2)(k_1 \cdot q_2) \dots \neq 1$

$$\begin{aligned} \int d^D q_2 \frac{p_1 \cdot q_2}{(q_2^2 - m_{q'}^2)(q_2 + q_1 + k')^2 - m'^2} &= p_{1\mu} \int d^D q_2 \frac{q_2^\mu}{(q_2^2 - m_{q'}^2)(q_2 + q_1 + k')^2 - m'^2} \\ &= p_{1\mu} B_\mu((q_1 + k')^2, m'^2, m_{q'}^2) \\ &= \underbrace{p_{1\mu}(p_1 + k')_\mu}_{p_1 \cdot (p_1 + k')} B_1((q_1 + k')^2, m'^2, m_{q'}^2) \Rightarrow \frac{p_1 \cdot (p_1 + k')}{\sigma - (q_1 + k')^2} \int d\sigma \Delta B_1 \end{aligned}$$

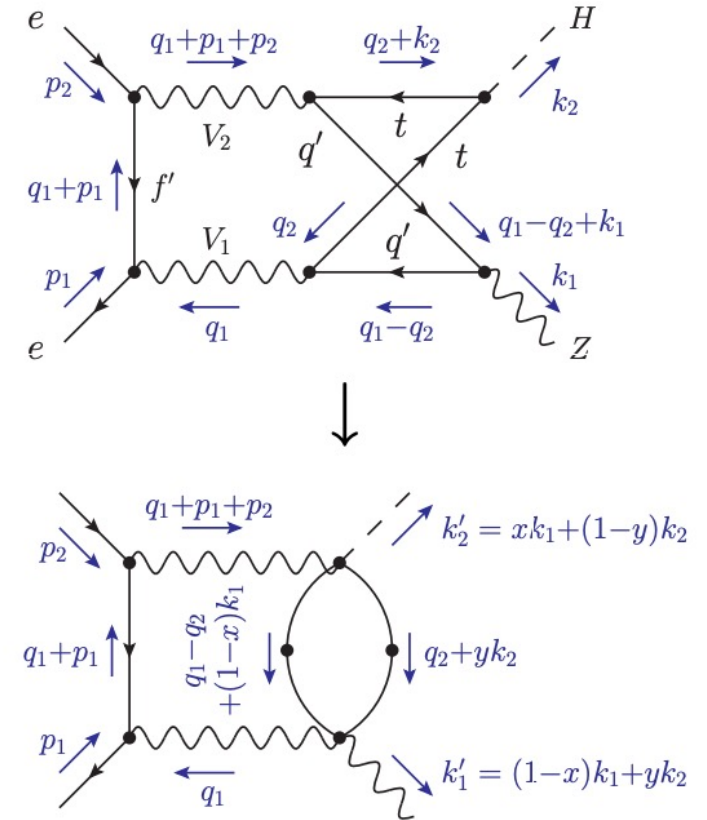
similarly,

$$\begin{aligned} \int d^D q_2 \frac{q_2^\mu q_2^\nu}{(q_2^2 - m_{q'}^2)(q_2 + q_1 + k')^2 - m'^2} &\Rightarrow B_{00}, B_{11} \Rightarrow \int d\sigma \Delta B_{00}, \int d\sigma \Delta B_{11} \\ \int d^D q_2 \frac{q_2^\mu q_2^\nu, q_2^\rho}{(q_2^2 - m_{q'}^2)(q_2 + q_1 + k')^2 - m'^2} &\Rightarrow B_{001}, B_{111} \Rightarrow \int d\sigma \Delta B_{001}, \int d\sigma \Delta B_{111} \end{aligned}$$

2. Evaluation Method – non-planar diagram

Similarly, use Feynman parametrization to simplify the denominators including q_2 and integrating loop momentum q_2 gives B0 function

$$\begin{aligned}
 I_{NP} &= \int d_{q_1}^D d_{q_2}^D \frac{1}{(q_1^2 - m_{V_1}^2)((q_1 + p_1)^2 - m_{f'}^2)((q_1 + p_1 + p_2)^2 - m_{V_2}^2)} \\
 &\quad \frac{1}{\underbrace{((q_1 - q_2)^2 - m_{q'}^2)((q_1 - q_2 + k_1)^2 - m_{q'}^2)}_{\int_0^1 dx \partial_{m_1'^2} \frac{1}{(q_1 - q_2 + (1-x)k_1)^2 - m_1'^2}} \underbrace{(q_2^2 - m_t^2)((q_2 + k_2)^2 - m_t^2)}_{\int_0^1 dy \partial_{m_2'^2} \frac{1}{(q_2 + yk_2)^2 - m_2'^2}}} \\
 &= \int_0^1 dx \int_0^1 dy \partial_{m_1'^2} \partial_{m_2'^2} \int d_{q_1}^D \frac{1}{B_0((q_1 + (1-x)k_1 + yk_2)^2, m_1'^2, m_2'^2)} \\
 &\quad \frac{1}{(q_1^2 - m_{V_1}^2)((q_1 + p_1)^2 - m_{f'}^2)((q_1 + p_1 + p_2)^2 - m_{V_2}^2)}
 \end{aligned}$$



2. Evaluation Method – non-planar diagram

For non-planar double box including $\gamma\gamma, \gamma Z, ZZ$, use the same dispersion relation. Put the derivative inside the integral by subtracting $\frac{\sigma_0}{\sigma} D_0$ and add it back

$$I_{NP(\gamma\gamma, \gamma Z, ZZ)} = \int_0^1 dx \int_0^1 dy \int_{(m'_1+m'_2)^2}^{\infty} d\sigma \partial_{m'_1{}^2} \partial_{m'_2{}^2} \Delta B_0(\sigma, m'_1{}^2, m'_2{}^2) (D_0(\dots, \sigma) - \frac{\sigma_0}{\sigma} D_0(\dots, \sigma_0)) \\ + \int_0^1 dx \int_0^1 dy \sigma_0 D_0(\dots, \sigma_0) \partial_{m'_1{}^2} \partial_{m'_2{}^2} B_0(0, m'_1{}^2, m'_2{}^2)$$

2. Evaluation Method – non-planar diagram

For non-planar double-box including WW:

$$m_1'^2 = m_b^2 - x(1-x)m_Z^2 < 0$$

Branch cut changes, we use a new dispersion relation.

$$\begin{aligned} B_0(p^2, m_1'^2, m_2'^2) &= \frac{1}{2\pi i} \oint_C d\sigma \frac{B_0(\sigma, m_1'^2, m_2'^2)}{\sigma - p^2 - i\epsilon} \\ &= \frac{1}{2\pi i} \int_{-\infty}^{\infty} d\sigma \frac{B_0(\sigma, m_1'^2, m_2'^2)}{\sigma - p^2 - i\epsilon} \end{aligned}$$

$$I_{NP-WW} = \frac{-1}{2\pi i} \int_0^1 dx \int_0^1 dy \int_{-\infty}^{\infty} d\sigma \partial_{m_1'^2} \partial_{m_2'^2} B_0(\sigma, m_1'^2, m_2'^2) D_0(\dots, \sigma - i\epsilon)$$

